

# Aerosol Physics

Presented by

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# Aerosol Physics

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- Agglomeration of aerosols
  - Several mechanisms cause collisions and sticking to produce larger particles
    - Brownian diffusion (random relative motions)
    - Differential gravitational settling (“sweep up”)
    - Turbulent agglomerating by shear and inertial forces
- Hygroscopic models discussed in another presentation

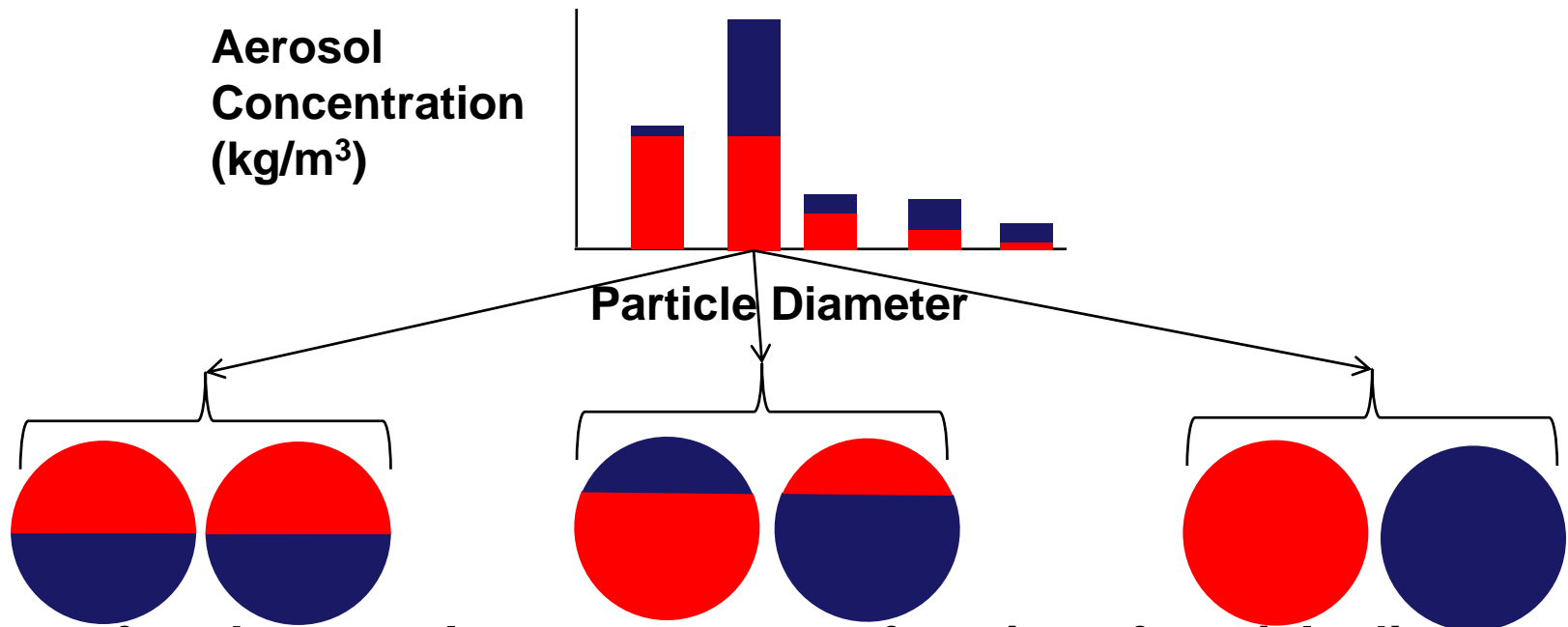
# MAEROS (1)

## Multicomponent AEROSol model

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- Calculates time history of aerosol particle size distribution and CHEMICAL COMPOSITION
  - Calculates changes in masses of each component (material) in each section as a function of time. Prior to this development, material composition of aerosol was unavailable and all particles were assumed to be of the same chemical composition regardless of particle size.
  - Currently limited to requiring that all aerosol components (materials), have the same material density.
  - Solves multi-sectional, multi-component formulation of dynamic equations for deposition and agglomeration.

# Basic Conceptual MAEROS Model (2)



Mass of each aerosol component as a function of particle diameter is used to determine health effects, but that is not a unique representation.

## Basic Approximations

- The total mass of a particle determines how the particle deposits, agglomerates, and grows.
- (Currently) All component material densities are the same.

# MAEROS (3)

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- *Sections* are particle size bins based on particle mass.
- Default is 10 sections between 0.1  $\mu\text{m}$  and 50.0  $\mu\text{m}$  in geometric diameter
  - Diameter boundaries: 0.100, 0.186, 0.347, 0.645, 1.20, 2.24, 4.16, 7.75, 14.4, 26.9, 50.0  $\mu\text{m}$
  - Can change number of sections, limits set through user input
    - To simplify analysis, agglomeration of two particles can't produce mass beyond next-larger section (particle size bin)
    - Requires diameter ratio  $> 2^{1/3} = 1.26$
    - For 0.1 to 50  $\mu\text{m}$  diameter, maximum of 26 sections ( $2^{n/3} < 50/0.1$ ),  $n = 26$ .

# MAEROS (4)

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- *Components* are materials
  - Each component has an independent size distribution
  - Conventional to take all densities as nominal  $1000 \text{ kg/m}^3$ 
    - Particles are rarely single spheres, so aerodynamic diameter is often used instead
      - Aerodynamic diameter ( $d_a$ ) is the diameter of a sphere with a material density of  $1000 \text{ kg/m}^3$  with the same settling velocity as the particle
      - Dynamic shape factor ( $\chi$ ) and agglomeration shape factor ( $\gamma$ ) are included to compensate for nonspherical effects
      - $d_a = d_e (\rho/1000)^{0.5}$ ,  $d_e =$  volume equivalent diameter

# Aerosol Factors: What to Use

- Chi - Aerosol dynamic shape factor (1.0)
- Gamma - agglomeration shape factor (1.0)
- FSLIP – particle slip coefficient (1.257)
- Stick – particle sticking coefficient (1.0)

Shapes	$\chi$
Sphere	1.00
Cube	1.08
4 sphere cluster	1.17
Sand	1.57
Talc	2.04

W. C. Hinds, Aerosol Technology, 1982.

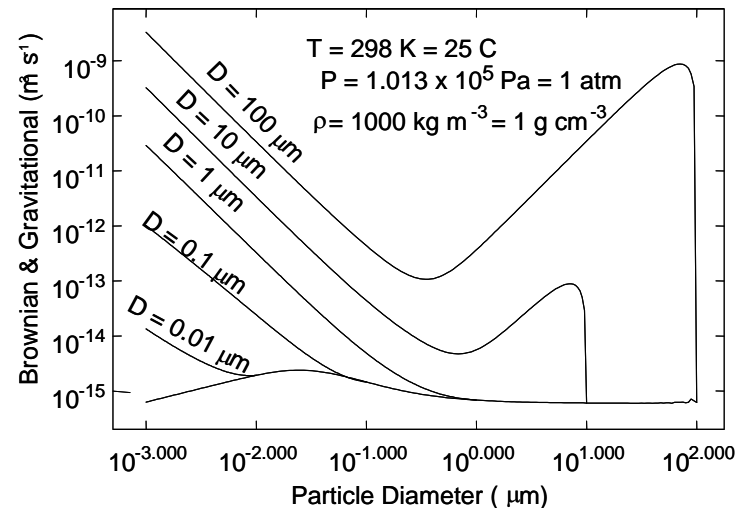
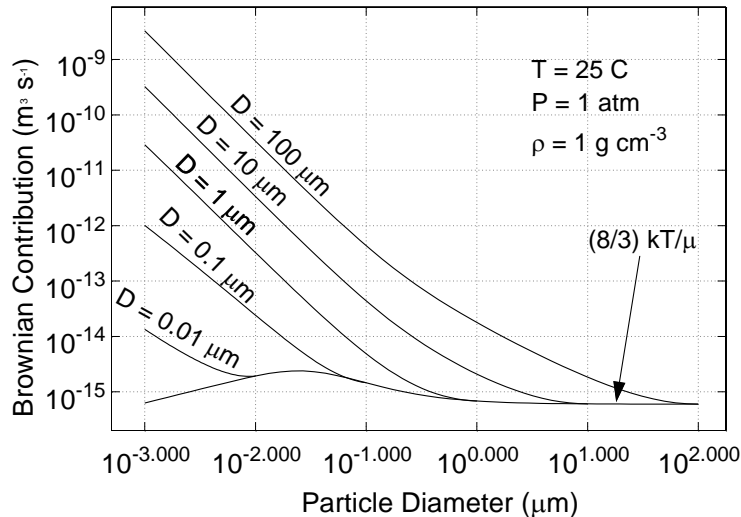
Brownian:	$\beta_B \propto \gamma \chi^{-1} f(d_i, d_j)$ Stick
Gravitational:	$\beta_{grav} \propto \varepsilon_g \gamma^2 \chi^{-1} (d_i + d_j)^2 (d_i^2 - d_j^2)$ Stick
Turbulent, Shear:	$\beta_{T1} \propto \gamma^3 \varepsilon^{1/2} (d_i + d_j)^3$ Stick
Turbulent, Inertial:	$\beta_{T2} \propto \gamma^2 \chi^{-1} \varepsilon^{3/4} (d_i + d_j)^2 (d_i^2 - d_j^2)$ Stick

***RN1\_MS00 chi gamma FSLIP STICK***

**Recommendation: use default unless data available.**

# Agglomeration

- Agglomeration becomes more significant for more concentrated aerosols
  - Particles collide, stick, and become larger particles;  
Rate  $\sim \beta N(D_i) N(D_j)$  where  $N$  is the number density ( $\text{m}^{-3}$ )
  - Brownian mechanism dominates for small particles, differential gravitational for large ones





# Composition of Individual Particles

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- MAEROS tells you only the mass of each material in particles in each size bin
  - It *does not* tell you the composition (or distribution of compositions) of any particle
- Deposition and agglomeration depend only on mass, diameter, and shape factors
  - Assume that the densities of the materials are the same and the shape factors depend at most on particle size
  - Then, independent of composition
    - All particles in each section deposit at same rate
      - If fraction  $x$  in section  $\ell$  is component  $n$ , then fraction  $x$  of deposition from this section will be component  $n$
    - *On average*, particle collisions will involve the same masses of each component
      - Section-to-section transfers will carry same mass of each component from section to section

# Note on MAEROS Coefficients

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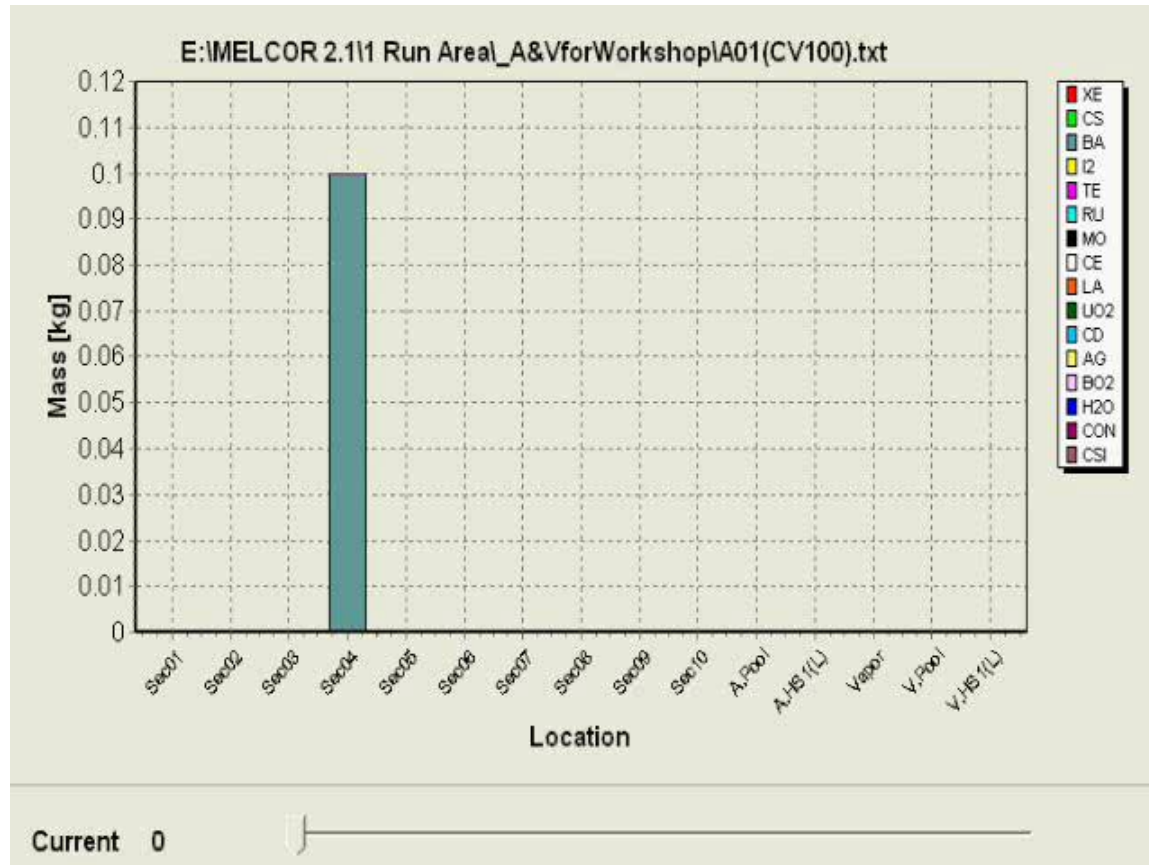
- Coefficients used by MAEROS are not typically calculated during transient
  - Require integrals over sections for deposition, double integrals for agglomeration
    - Calculations are relatively time-consuming
  - Values pre-calculated at corners of a finite  $(P,T)$  domain
    - Values interpolated for each volume at appropriate  $(P,T)$ 
      - Recent versions of MELCOR use bilinear interpolation in  $P^a$  and  $T^b$ ,
    - Properties of *air* used in pre-calculation
      - Should be accurate in normal containment calculations
      - May be inaccurate in other cases
- Can be re-calculated every time step (RN1\_Turb)

# Simple Agglomeration Calculations

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- Single material, nominal density =  $1000 \text{ kg/m}^3$ , tiny surface to effectively eliminate deposition
- Three cases with single  $d_p \sim 1 \mu\text{m}$  or  $\sim 10 \mu\text{m}$ 
  - Case 1:  $d_p = 0.880 \mu\text{m}$ ,  $\rho = 1000 \text{ kg/m}^3$ ,  $10^{-10} \text{ m}^2$  surface
  - Case 2:  $d_p = 10.57 \mu\text{m}$ ,  $\rho = 1000 \text{ kg/m}^3$ ,  $10^{-10} \text{ m}^2$  surface
  - Case 3:  $d_p = 10.57 \mu\text{m}$ ,  $\rho = 1000 \text{ kg/m}^3$ ,  $10^{-10} \text{ m}^2$  surface, settle back to same volume through  $15 \text{ m}^2$  “settling surface”

# Visualization of Results, Case 1



# Visualization of Results, Cases 2 and 3

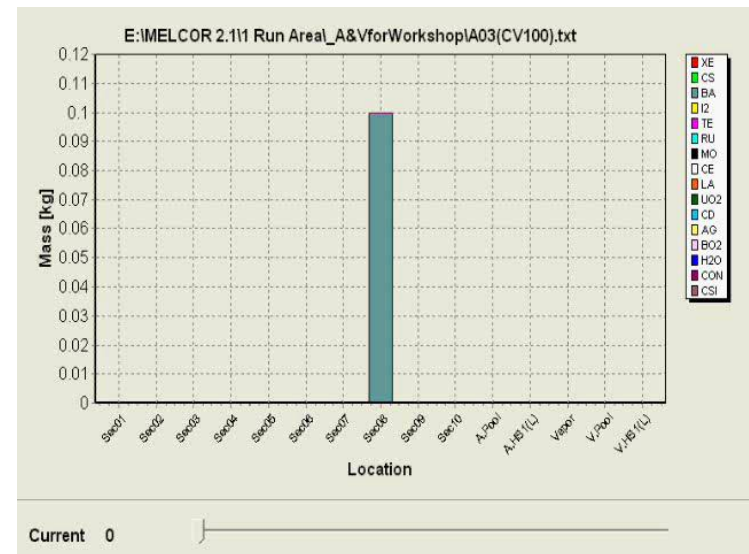
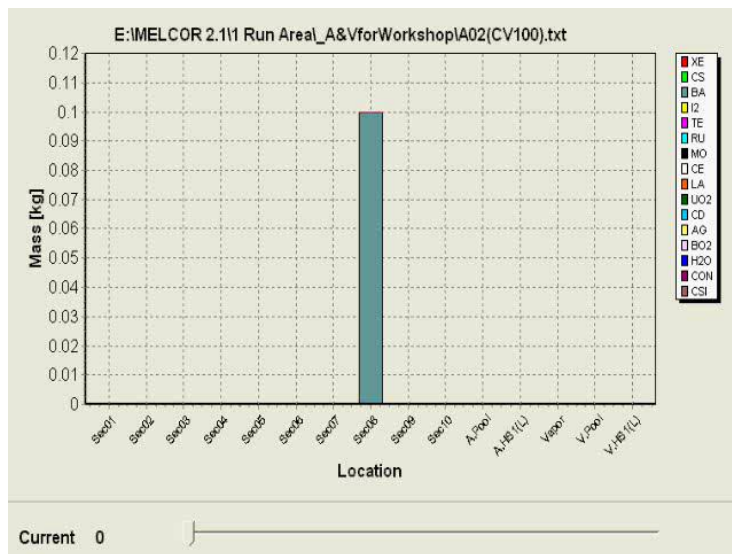
## • Case 2

- Initial  $\sim 10 \mu\text{m}$  (section 8)
- Tiny ( $10^{-10} \text{ m}^2$ ) deposition area
- Rapid growth to section 10 and larger
  - Mass settles to heat structure surface despite tiny area

## • Case 3

- Like Case 2 *but*  $15 \text{ m}^2$  settling area from volume to itself
- All mass stays suspended
  - *Huge* population in section 10 sweeps up all smaller aerosols
  - *Not physical*

**Start**



# Multi-Material Aerosols

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- RN Package and MAEROS each treat more than one material, but treatments differ
  - Main RN database includes distinct size distribution for each RN class (Cs, Ba, UO<sub>2</sub>, ...)
  - MAEROS considers only a limited number of *components*
    - Each contains one or more RN classes
      - Component masses in each section calculated at start of MAEROS advancement as sums of class masses; sub-compositions saved
      - Post-advancement component masses are distributed to RN class distributions using sub-compositions
    - User can define number of components and the classes assigned to each
      - Default is 2, with one component reserved for water and all other classes in the other
      - Recommend at least 3 which (absent further input) will further assign the volatiles (Cs, I<sub>2</sub>, CsI, CsM) to a separate component
      - Can modify these, or add other components to track classes of interest or classes with very different release histories (like CON from ex-vessel core/concrete interactions)

# Two-Material Agglomeration Calculations

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- Ran two versions of a 2 material case
  - Initial 0.1 kg of Ba aerosol,  $d_p=0.880\mu\text{m}$
  - Initial 0.1 kg of UO<sub>2</sub> aerosol,  $d_p=10.57\mu\text{m}$
  - $\rho=1000\text{kg/m}^3$ ,  $10^{-10}\text{ m}^2$  surface
- Case 4: default component assignments
  - Both Ba and UO<sub>2</sub> assigned to component 1
- Case 5: custom component assignments
  - Ba assigned to component 1, UO<sub>2</sub> to component 4

# Visualization of Results, Cases 4 and 5

- Case 4 (same component)

- MAEROS does not maintain distinction

- Aerosol distribution “homogenized” on first advancement

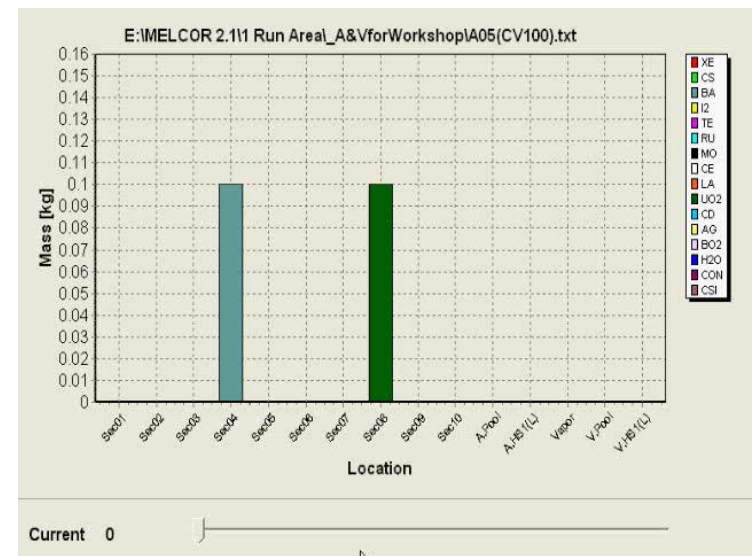
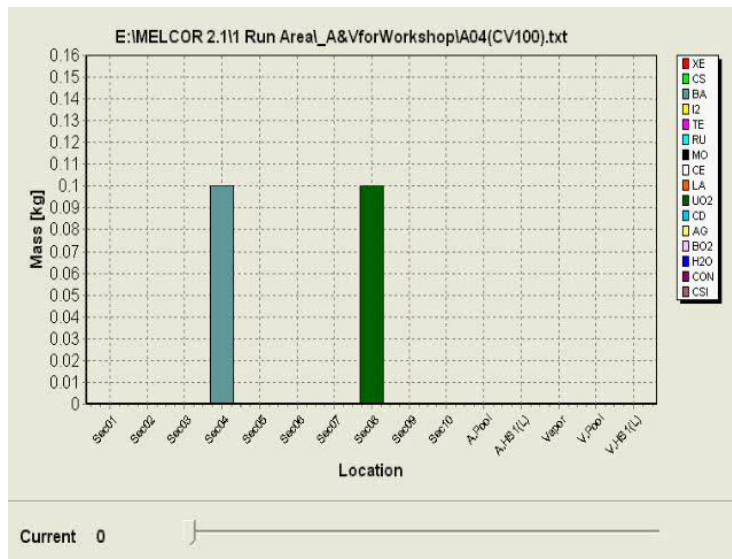
- Puts half UO<sub>2</sub> mass into smaller section, half Ba mass into larger one

- Case 5 (distinct component)

- MAEROS maintains distinction

- Agglomeration of small and large aerosols slowly moves some Ba mass into larger sections

Start





# TRAP MELT

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- Models condensation and evaporation of RN vapors involving aerosols and surfaces (replaces treatment in stand-alone MAEROS)
- Volatile radionuclides (e.g., CsOH, I<sub>2</sub>, CsI, Cs<sub>2</sub>MoO<sub>4</sub>), have finite vapor pressures that increase with temperature
  - Concentration in atmosphere limited by vapor pressure at  $T_{atm}$
  - Mass can be transported to/from condensed phase on aerosol surfaces and/or structural surfaces
    - Aerosols are at atmosphere temperature
    - Structure surfaces may be hotter or colder
    - Rate limits apply

# TRAP MELT Equations

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- Conservation of mass, and rate equations are

$$\frac{dM_a}{dt} + \sum_i \frac{dM_i}{dt} = 0 \quad \frac{dM_i}{dt} = A_i k_i (C_a - C_i^s)$$

–  $M$  is mass,  $C = M/V$  is concentration, subscript  $a$  refers to atmosphere, subscript  $i$  refers to surface, superscript  $s$  is saturation at surface temperature

- Surfaces include aerosols, section by section

- Model evaluates closed-form solution for full MELCOR timestep,  $\Delta t$

$$C_a = M_a / V = \frac{\beta}{\alpha} - \left( \frac{\beta}{\alpha} - C_{a0} \right) e^{-\alpha \Delta t}$$

$$M_i = M_{i0} + A_i k_i \left( \frac{\beta}{\alpha} - C_i^s \right) \Delta t - A_i k_i \left( \frac{\beta}{\alpha} - C_{a0} \right) \left( \frac{1 - e^{-\alpha \Delta t}}{\alpha} \right)$$

$$\alpha = \sum_i A_i k_i / V \quad \frac{\beta}{\alpha} = \frac{\sum_i A_i k_i C_i^s}{\sum_i A_i k_i}$$

– Iteration may be needed if any surface mass falls to zero

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# Condensation Aerosols

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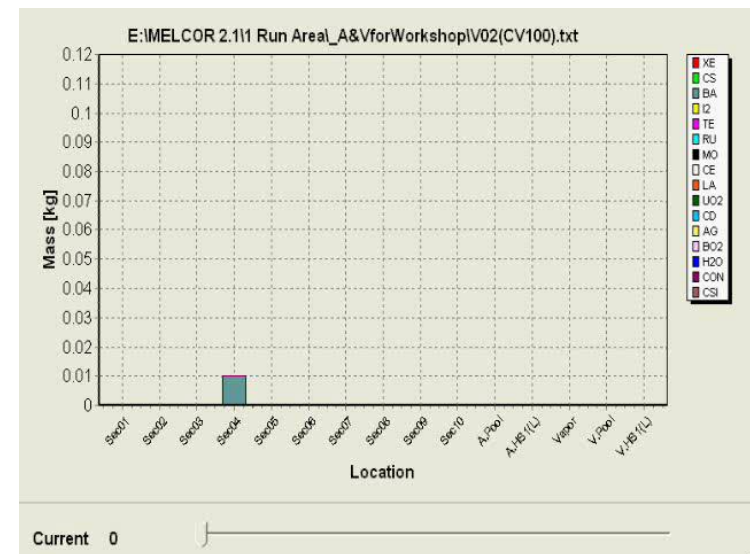
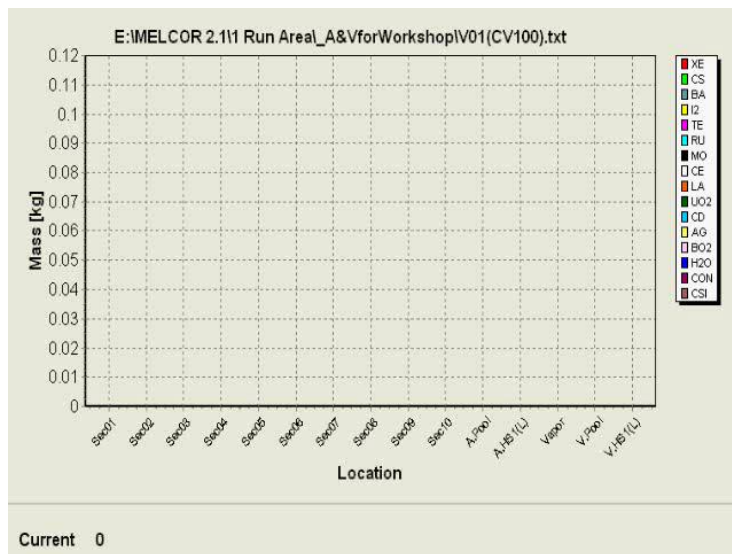
- Ran test cases with the 45 m<sup>3</sup> room and Cs (actually, CsOH) vapor source
  - Temperature raised to 780 K, where mass corresponding to saturation is 0.00685 kg
  - Cs-class vapor mass added at 10<sup>-5</sup> kg/sec
    - Takes 685 s to reach saturation
  - Chemisorption model turned off
  - Two cases
    - Case 1: no initial vapor or aerosol
    - Case 2: no initial vapor, initial 0.01 kg non-volatile (Ba) aerosol ~0.88 μm

# Condensation Aerosol Results

- Case 1 No vapor, no aerosol
  - Cs concentration rises to saturation
  - First aerosols form in smallest section, then agglomerate rapidly
  - Further condensation on existing aerosols

- Case 2 No vapor, little aerosol
  - Same rise to saturation
  - Most early condensation on existing Ba aerosols

Start



# Comments on Condensation Calculations

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- See almost no direct condensation on walls
  - Wall and aerosol areas comparable (within factor of 10)
  - Mass transfer coefficient for wall is *much* smaller
    - Characteristic length in Sherwood number (analog of Nusselt number) is much larger, m vs.  $\mu\text{m}$
- Could construct other cases
  - Smaller aerosol concentrations
  - Multiple walls
    - Different temperatures
    - Initial deposited vapors

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# Questions