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BEL V MODEL DEVELOPMENT AND ASSESSMENT WITH MELCOR 2.2

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REI

<u>Martina Adorni</u>, Albert Malkhasyan

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TABLE OF CONTENTS

- Introduction
- Progress in MELCOR modeling
 - Bel V-developed NPP nodalization
 - Creep failure modeling
 - Feedbacks
- SFP-building study
- Conclusive remarks



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INTRODUCTION

- MELCOR: reference code selected by Bel V for severe accident analysis
- Acquisition of MELCOR code: end 2012
- MELCOR code mainly used in the framework of Bel V R&D program and in support of nuclear safety assessments
- Objectives of the presentation

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- Exchange experience and information about model development and assessment efforts
 - Key messages from model development and open questions
 - Focus on modeling activities, some sample results

Creep rupture modeling

PROGRESS IN MELCOR MODELING

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- PIPE-STR and LM-CREEP CFs can be used to calculate the creep failure of a pipe under pressure-induced stresses
 - Hot leg creep failure MELCOR modeling
 - Problems with the stress function
 - Two-step procedure of calculations
- Focus on the capability of creep failure modeling, no nodalization changes at this stage
- MELCOR input manual contains useful example of modeling

• PIPE-STR: cumulative damage to the pipe, max stress in a thick-walled cylindrical pipe under internal pressure

```
CF_ID Stress 202 PIPE-STR

CF_SAI 1.0 0.0

CF_MSC 0.37 0.46

CF_ARG 2

1 CVH-P('hot leg_C') 1. 0. ! Inner pressure (hot leg)

2 CVH-P('RCS C') 1. 0. ! Outer pressure (containment)
```

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• LM-CREEP: cumulative damage based on the Larson-Miller creep-rupture failure model

```
CF_ID 'Pipe Creep' 203 LM-CREEP
CF_SAI 1.0 0.0
CF_MSC SS-316 ! default data of 316 Stainless steel
CF_ARG 2
1 CF-VALU(Stress) 1. 0. ! Stress
2 HS-TEMP('hl pipe hor_3', 2) 1. 0. ! Temp, node 2
```

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• Failure is assumed to occur when LM-CREEP(t) = 1

```
CF_ID 'Pipe Creep=1' 204 L-GT
CF_LIV FALSE
CF_ARG 2
1 CF-VALU('Pipe Creep') 1.0
2 CF-CONST 1.0
```



 Trip function used to operate valves (open/close)

CF_ID	'Pipe Creep_1'	205 TRIP	
CF_SAI	1.0	0.0	0.0
CF_ULB	DEFAULT	0.0	0.0
CF_ARG	1		
	1 CF-VALU('Pipe Creep=1')		

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12

- Upon creep failure of the hot leg nozzle, a large hole opens that rapidly depressurizes the RCS
 - FLs & CFs modeling like a large break loss-of-coolant accident
- Alternate failure locations could include
 - pressurizer surge line
 - steam generator tubes
- The most vulnerable location can be calculated



- Problem encountered by modeling as explained in the previous slides
 - @Time ~ hot leg creep failure prediction
 - Calculation terminated by: CF_CREEP error: Negative or zero value for Stress

14

- Two-step calculation procedure
 - RUN 1: Activation of creep CFs, without LB-LOCA like features → no rapid depressurization of the RCS at HL failure

Id of time of HL creep failure

 – RUN 2: Disabling of creep CFs, with LB-LOCA like features operating at time id above → rapid depressurization of the RCS resulting from HL failure

Run with creep failure induced depressurization

• Are there better ways to model it?

The IRSN's DENOPI research program, in which Bel V collaborates, is devoted to spent fuel pool loss-ofcooling and loss-of-coolant accidents (French National Research Agency (ANR) contract reference: ANR 11 - RSNR 006)

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Bel V contribution to the IRSN's DENOPI project

STUDY OF THE AERAULICS OF THE SFP-BUILDING BY MEANS OF MELCOR CODE

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• Objective

- Analysis of the SFP building aeraulic by means of MELCOR code during accident situations
 - Base calculations of the Kondo et al.* *(current presentation)*
 - Comparisons with the results of ASTEC calculations (*to be confirmed*) and IRSN's DENOPI project experimental results (*when available*)
- Phenomena of interest
 - SFP building atmosphere transient behavior
 - Wall condensation
 - SFP free surface evaporation
 - Impact of: opening to the environment (doors, leaks), surface/volume ratio of the building, spent fuel power



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- MELCOR version 1.8.6.4073
- SBO accident scenario
 - No power for cooling spent fuel
 - No conditioning of the air
- BWR reactor building
 - SFP located within the reactor building, but outside of the primary containment
- 72h transient calculations

* Kondo M. et al., An evaluation model to predict steam concentration in a BWR reactor building, Nuclear Science and Technology, 2015 Vol. 52, No.11, pp 1369-1382.

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- Base input deck created starting from
 - Tills J. et al., Application of the MELCOR Code to Design Basis PWR Large Dry Containment Analysis, SAND2009-2858
- Initial and Boundary conditions from Kondo et al. (2015)
- Simulation domain
 - Operation floor, floor wall, building atmosphere and environment
 - SFP time dependent boundary conditions: evaporation rate and enthalpy







Temperature of building atmosphere (left) and vapor concentration in the building (right)

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SFP condensation rate (left) and temperature distribution in the building wall (right)

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FUTURE PLANS

- The activity proceeds as scheduled
 - SFP-building analysis in support of the interpretation of the IRSN's DENOPI project experimental results
- Next steps

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- Conversion of the developed input decks to MELCOR 2.2 version
- Extension of the simulation to the pool modeling
- Sensitivity analyses
- Study of other cases: SFP-LOCA?



Bel V model development and assessment with MELCOR 2.2

CONCLUSIVE REMARKS

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CONCLUSIVE REMARKS

- Exchange experience and information about model development and assessment efforts
 - Bel V is progressing in MELCOR modeling by extending the developed plant input deck with additional modeling capabilities (HL creep failure)
 - Bel V contributes to MELCOR assessment (IRSN's DENOPI project)
- Possible future interest
 - Activity calculations (BONUS): how to use it?
 - Retrieving isotopes composition from MELCOR classes

24

QUESTIONS?

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THANKS FOR YOUR ATTENTION!

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