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MELCOR modeling of FP scrubbing in experiments and in integral accident scenarios

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Outline

- Scrubbing modeling with MELCOR/SPARC for experiments
 - POSEIDON experiments, for general SPARC behavior testing (older TEPCO-TOSHIBA-HITACHI experiments, for boiling conditions)
 - thermal-hydraulic behavior by MELCOR in experiments
 - aerosol retention with default/non-default SPARC settings
- Scrubbing modeling with MELCOR for integral "Fukushima-like" scenarios and FP behavior
 - thermalhydraulics
 - WW Mark-I scrubbing related phenomena for Cs and iodine compounds
 - with the same default/non-default MELCOR/SPARC settings
- Conclusions and outlook



SPARC and MELCOR/SPARC model and POSEIDON test series

- SPARC (MELCOR/SPARC) --a relatively complex code written for aerosol retention calculations in WW water of a BWR (iodine vapors included)
 - what it is in MELCOR now is -to our knowledge- the same as original SPARC
- as all currently used scrubbing models, SPARC is rather old -yet, its validation is not great
- our aim was to use SPARC for scrubbing experiments having conditions prototypical to severe accidents and then in the same way for an integral BWR accident based on Fukushima U3; stand-alone BUSCA code used as well for comparison
- PSI POSEIDON test series chosen as first
 - very well documented
 - prototypic (high) flow rates of gases used in
 POSEIDON as well as other relevant conditions



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Experimental parameters in POSEIDON tests and calculated DFs

Test	Gas Flow Rate (kg/h)	Steam Mass Fraction	Inlet Pressure (bar)	Gas Temp. (ºC)	Pool Temp. (ºC)	Pool Height (m)	Inlet Aerosol Flow Rate (g/s)	Outlet Steam Mass Fraction	Outlet AMMD (µm)	Outlet GSD	DF exp	calc. BUSCA	calc. DF (MELCOR / SPARC defaults)	calc. DF (non- default "sparger" option)
PA06	142.5	0.553	1.45	243.0	86.9	1.0	0.0118	0.518	0.36	1.64	7.3 ±1.4	5.5	1.2	12
PA07	142.5	0.553	1.42	267.7	86.3	0.3	0.0119	0.506	0.36	1.5	6.6 ±2.3	2.1	~1	~1.8
PA08	145.1	0.563	1.63	212.9	86.8	4.0	0.0096	0.525	0.28	1.34	21.4 ±6.7	183	~2	~240
PA11	137.9	0.043	1.46	256.1	75.3	2.0	0.0152	0.237	0.24	1.6	5.4 ±1.4	-	1.05	14
PA12	124.9	0.0	1.36	237.7	71.8	1.0	0.0161	0.249	0.3	1.55	3.4 ±0.6	2.8	~1	~5.5
PA15	94.3	0.719	1.30	305.2	85.4	1.0	0.0091	0.475	0.31	1.59	4.9 ±1.0	-	~1.4	~13
PA17*	91.8	0.747	1.30	310.8	88.0	1.0	0.0571	0.539	0.46	1.62	12.3 ±6.2	12	1.7	40
PA15 PA17*	94.3 91.8	0.719	1.30 1.30	305.2 310.8	85.4 88.0	1.0 1.0	0.0091	0.475 0.539	0.31 0.46	1.59 1.62	4.9 ±1.0 12.3 ±6.2	- 12	~1.4	~13 40

* inlet AMMD =0.54 µm in PA17, 0.3 µm in all other tests

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0.08

0.06

0.04

0

0

5

10

gas flow rate (kg/s) 70

typical results of POSEIDON simulations thermalhydraulics in PA08

- simple model used, similar to Sandia **MELCOR** test problems
- PA08: 4m of water, 86°C, inlet steam mass fraction 0.56, gas flow rate ~40g/s, 212°C, inlet aerosol concentration ~0.2g/m3, inlet AMMD=0.3µm
- thermalhydraulics very well captured by **MELCOR for all POSEIDON tests**





Decontamination Factors in POSEIDON simulations by MELCOR/SPARC

- trends in calculated DFs the same in all POSEIDON tests: the same effect of submergence, steam content, particle size
- by far the most important sensitivity in calculations :
 - default MELCOR/SPARC options versus non-default "quencher" (multihole) vent option
- large differences in predicted DF values whereas the thermohydraulics was calculated to be the same between the 2 runs; this same picture seen in calculations of all POSEIDON tests
- differences lie in description of the initial bubble formation for various vent types (original EPRI correlations)
- for all other calculated tests than PA08, which is of highest submergence, the agreement with experiment for DF values (with non-default SPARC settings) far better than in PA08





BWR integral source-term calculations with MELCOR/SPARC

- differences seen in simulations of experiments may have significant impact on integral source term predictions for severe accidents at BWRs (e.g., with relevant systems at FU2 versus those at FU3)
 - DF~2 versus DF~200 (as in PA08 with high submergence) represents efficiency of 50% versus 99.5% of the aerosol mass scrubbed
- try to check it -with Cs and I- for "Fukushima-like" BWR SBO scenarios: prolonged operation of relevant core cooling systems => "Fukushima-like"



- our Fukushima-like sequence based on detailed FU3 simulations by PSI(*)
- at about 40h into the accident, things starting to "go definitively wrong" :
 - RPV water level below BAF
 - first hydrogen
 - beginning of FP release

(*) L.Fernandez, J.Birchley, Annals of Nuclear Energy, 83 (2015) 193–215



Comparison of the same BWR sequences with different MELCOR/SPARC settings

- calculated Fukushima-like scenarios with active containment venting operation (*NUTHOS-11 paper) defined such as to allow for the FP environmental release -and Cs and I isotopes in particular- only via WetWell water (Suppression Chamber) and then through ventilation lines
 - starting to deviate from FU3 case at about these 40h
- no head flange DryWell leakage, no other containment failures
- enables to compare more easily the FP retention in WetWell for different MELCOR/SPARC settings in an integral scenario
- again, like for experiments, calculated thermalhydraulics very similar between the 2 cases
 - R01: defaults in MELCOR/SPARC

– R02: non-default MELCOR/SPARC "sparger/quencher" vent











what would happen if also vapors are scrubbed? (directions taken from an old Sandia CSARP presentation)



effect is huge, as one would expect,

but not a single word is written about this model in the code manuals!



Conclusions and outlook

- presented work consists of
 - aerosol scrubbing modeling by MELCOR/SPARC for POSEIDON experiments
 - FP transport modeling in an integral severe accident (BWR Mark-I, "Fukushima-like") with focus on Cs (I) behavior and its retention/scrubbing in WW
- MELCOR/SPARC calculates reasonably the thermalhydraulics in POSEIDON experiments (including steam condensation); aerosol retention calculations, on the other hand, were very sensitive to changes in default SPARC input options
 - proper use of different EPRI correlations in different areas of interest should be examined
- BWR "Fukushima-like" sequence and FP retention in WW
 - predicted aerosol DFs in WW sensitive the same way as for the experiments
 - FP releases from RPV to WW are discrete events, at least in this type of a scenario -other factors than just DFs can play a role in retention (timing, ...)
 - to understand the retention of Cs (or FPs in general) and its behavior one needs to study
 every given accident sequence in detail
 here MELCOR is quite helpful
 - calculations also confirmed again that FP speciation is crucial (e.g., CsOH versus Cs2MoO4 in terms of their volatility)
 - we need to check MELCOR/SPARC treatment of FP vapors other than those of iodine
- work continues, first with looking at boiling conditions for aerosol scrubbing (TEPCO-TOSHIBA-HITACHI tests) and then with some newer Japanese scrubbing tests



Wir schaffen Wissen – heute für morgen





MELCOR nodalization





WW water temperature





consists of four tasks:

- (1) analyses of an extended duration BWR sequence
 - integral scenario (up to approximately 6 days) with source term evaluations
 - generic Mark-I BWR "Fukushima-like" sequence
- (2) FP transport with special focus on Cs and iodine behavior in the integral BWR scenarios
- (3) pool scrubbing models tested in experiments and in the integral BWR scenarios
 - WW Mark-I scrubbing related phenomena
- (4) iodine radiochemistry modeling relevant to iodine containment behavior at accidents
 - small scale PSI test recalculations with dedicated tools (PSIodine, IODE part of ASTEC code(?), ...)

WORK STARTED THIS YEAR with

- pool scrubbing modeling
 - for POSEIDON test series (and TEPCO-TOSHIBA-HITACHI experiments for boiling conditions -not yet finished)
 - and for corresponding WW scrubbing modeling in a "Fukushima-like" BWR scenario
- Cs and iodine transport modeling in the same integral scenario