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# Conversion of SFP input deck from MELCOR 1.8.6 to 2.1 and back

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- Introduction
- Modelling
- Conversion
- Results
- Conclusions



Goal of the work was to check the SNAP convertion routines with a relatively simple SFP inpt deck

A MELCOR 1.8.6 input deck was prepared for the Fukushima unit 4 spent fuel pool

The results of the converted MELCOR 2.1 deck were compared with the results of the original deck

The results of the back converted MELCOR 1.8.6 deck also were compared with the original results



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Slow Loss of coolant accident until pool is completly dried out

Remaining pool water heats up during drainage

After start of uncovery fuel heats up and cladding starts to oxidize

Buoancy driven gas flow starts after water level reaches lower end of fuel racks

PSI breakaway model is activated (in steam and air)

Radio nuclide release and MCCI is activated

Cavity will be activated after failure of the steel liner at melting temperature





Fuel Assembly Geometry









Two phases were planned during the project:

- Hot neighbour configuration
- Cold neighbour configuration



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**Conversion MELCOR 1.8.6 to MELCOR 2.1** 

# **Conversion of the input deck with SNAP**

1. Problem was setting of not used hydraulic diameters to 0.0 (needs manual correction)



Failure of MELGEN, but production of restart file MELCOR fails with: restart file not found!!!



**Conversion MELCOR 1.8.6 to MELCOR 2.1** 

# **MELCOR 1.8.6 (YV 3084 PSI)**

*	DHYCL	DHYOS	DHYPD	DHYCNC	DHYCNB	DHYSS	DHYNS	DHYPB
COR10204	0.09652	0.09652	0.09652	0.09652	0.09652	0.09652	0.09652	0.09652
*		DHYRK						
COR10204	C	0.09652						

# **MELCOR 2.1 (6342)**

COR_EDR	24 ! n	ia	ir	dhycl	dhypd	dhycnc	dhycnb	dhyss	dhyns	dhypb
	2	2	1	0.09652	0.09652	0.0	0.0	0.09652	0.09652	0.09652
COR_RDR	24 ! n	ia	ir	dhyrk						
	2	2	1	0.09652						



**Conversion MELCOR 1.8.6 to MELCOR 2.1** 

# **Conversion of the input deck with SNAP**

2. Problem was reversing the command to store contour data for cavity shape (1 -> exclude)

# **MELCOR 1.8.6**

CAV01Z1 SHAPEPLOT 1

# MELCOR 2.1

CAV\_U 4 !n keyword value[1] value[2] 4 SHAPEPLOT EXCLUDE



# **Problem with MELCOR 2.1:**

MELCOR 2.1 fails at restart with PSI breakaway model activated after oxidation has started (breakaway conditions could not be identified)



#### **Conversion MELCOR 2.1 to MELCOR 1.8.6**

### MELCOR 2.1

COR_EDR	24 ! n	ia	ir	dhycl	dhypd	dhycnc	dhycnb	dhyss	dhyns	dhypb
	2	2	1	0.09652	0.09652	0.01	0.01	0.09652	0.09652	0.09652
COR_RDR	24 ! n	ia	ir	dhyrk						
	2	2	1	0.09652						

### **MELCOR 1.8.6**

\*
dhycl
dhyfm
dhypd
dhycnc
dhycnb
dhyss
dhyns
dhypb

COR10204
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## no problem for MELCOR 1.8.6 here, but...

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#### **Conversion MELCOR 2.1 to MELCOR 1.8.6**

'IN' TRANSFER PROCESS FROM COR PACKAGE TO TP PKG \* \* NMSIN NTHRM TPIN10100 6 9 **'OUT' TRANSFER PROCESS FROM TP PACKAGE TO CAV PKG** NMSOT NPOTOI IOTMTX TPOT10100 5 101 **UIN.101** TPM1010000 5 6 **TRANSFER PROCESS INPUT - RADIONUCLIDE MASS** NMSIN NTHRM **TPIN60100** 16 1 NMSOT NPOTOI IOTMTX **TPOT60100** DEF.1 16 601

#### **Problem with TP**

*n: ITP_1 * TPIN00100 *	nmsin 6	nthrm 9	
*n: ITP_2 * TPIN50100 *	nmsin 16	nthrm 1	
*n: OTP_1 * TPOT10100 *n: OTP_2	nmsot <mark>0</mark>	npotoi 1	outmtx UIN.1*
* TPOT60100 *	nmsot <mark>0</mark>	npotoi 501	outmtx DEF.1

MELCOR 1.8.6 original

#### MELCOR 2.1

**!\*\*\*\*\*\*** Input Transfer Components ! size TP IN 2 In nametpin type direct ip2edf nmsin nthrm 1 'ITP\_1' COR 2 'ITP\_2' RNCOR **!\*\*\*\*\*\* Output Transfer Components** ! size TP\_OUT 2 !n nametpot npotoi outmtx nmsot 'OTP\_1' 'ITP\_1' 'MTX\_101' 1 2 'OTP 2' 'ITP 2'

MELCOR 1.8.6 back converted



# Problem again was reversing the command to store contour data for cavity shape (include -> 0.)

# MELCOR 2.1

CAV\_U 4 !n keyword value[1] value[2] 4 SHAPEPLOT INCLUDE

# **MELCOR 1.8.6**

CAV01U3 SHAPEPLOT 0.



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Identical results until beginning of fuel uncovery. numerical instable behavior of the code leads to slightly different calculation.





The results of the converted input decks start to differ more significantly after begin of relocation.

The peak cladding temperature (above) shows differences after the first peak and also at the last cladding relocation.

The hydrogen production in the core (below) stops at different levels and the later hydrogen production after fuel relocation can be explained by oxidation of non-relocated rack materials (steel).



100

0

0

2

1

3

4

Time (d)

5

6

8

7



The oxide thickness of the cladding is a very useful variable and is used since several years. Surprisingly it was notified that it is not available in 2.1.

It is also not mentioned in the user guide of 1.8.6.

Recommendation: Include the variable in 2.1 version.

The ejected mass is almost identical except of the timing.



Time (d)

A Problem with 2.1 is a larger instability of the program during MCCI. It was not possible to drive the code for the further calculation of the accident sequence.

The melt temperatures (above) are differing strongly between 2.1 and 1.8.6.

Also the horizontal concrete ablation is strongly different between MELCOR 1.8.6 and MELCOR 2.1.



#### MELCOR 2.1 failed during the MCCI calculation with following error message:

<Diagnostic Message> Time= 9.3320E+06 Dt= 1.2000E+00 Cycle= 3957380 (COR) VIEW FACTOR ERROR IN CORVF SUM OF VIEW FACTORS EXCEEDS UNITY FOR SURFACE PRT.DBR IN CORE CELL 303 FURTHER MESSAGES SUPPRESSED

<Diagnostic Message> Time= 9.3442E+06 Dt= 8.3435E-10 Cycle= 3968860 (CVH) Error in equilibrium thermo routine CVTWGE Called from CVTNQE for Volume Building

MELDIA\_v2-0 and MELOUT\_v2-0 filesize increased over 85 GB each before run was stopped manually.



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# The code conversion with SNAP is working with some problems (TH diameters, MCCI contour data, TP).

# The code calculates in rather good agreement at the beginning of the transient. Diversivities are growing with time as usual.

Attention! MELCOR 2.1 produces restart file even if MELGEN fails.



# Wir schaffen Wissen – heute für morgen



