

Application of MELCOR 1.8.2 (fusion version) and MELCOR 2.1 on the DEMO Helium Cooled Pebble Bed blanket concept.

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Outline

1. Introduction - Motivation.
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3. PHTS modellization for Stationary runs.
4. PHTS modellization for In-Vessel LOCA scenarios.
5. Conclusions.
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Introduction - Motivation



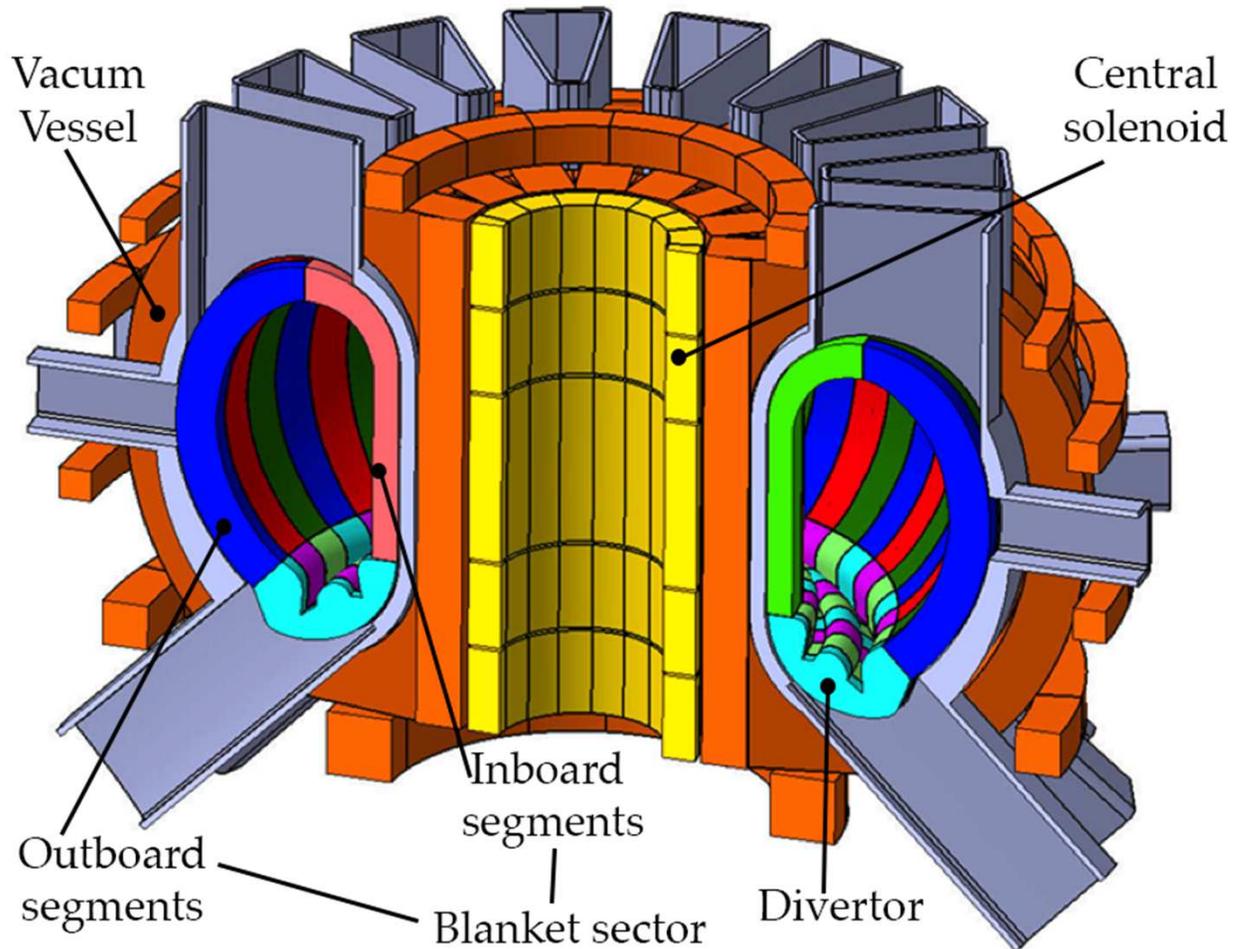
- Several incidental/accidental conditions can hamper the safety of a fusion reactor, and the Loss of Coolant Accident (LOCA) of the blanket Primary Heat Transfer System (PHTS) is one of the most challenging [1].
- To date, one of the main codes employed for incidental conditions analyses in fusion installations is MELCOR 1.8.x. Although, this version is quite old, and newer version were released (MELCOR 2.1.6342).
- The aim of this work is to stress the positive and negative aspects of M 1.8.2 and M 2.1 through a “version-to-version” comparison employing the same nodalisation.

DEMO & HCPB blanket concept (1/3)

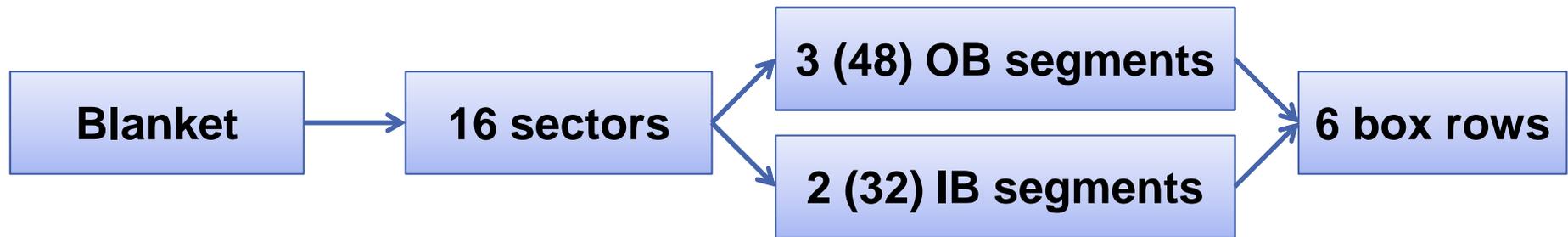
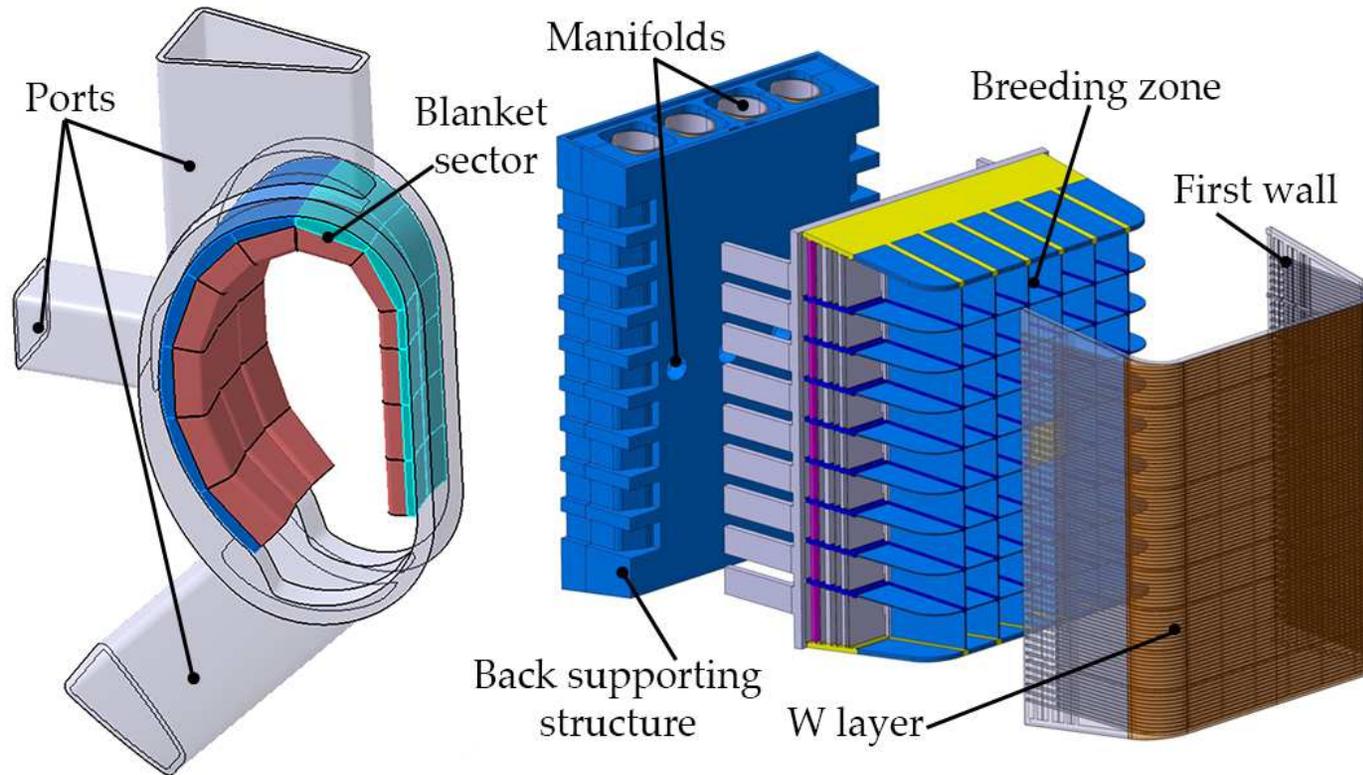
- DEMO represents the prosecution of the scientific and technological challenge of ITER, and it should demonstrate the suitability of the fusion power as a sustainable energy power source.
- To date, several different DEMO concepts exist basing on the various “blanket concept” proposed:
 - HCPB – Helium Cooled Pebble Bed
 - WCLL – Water Cooled Lithium Lead

DEMO & HCPB blanket concept (2/3)

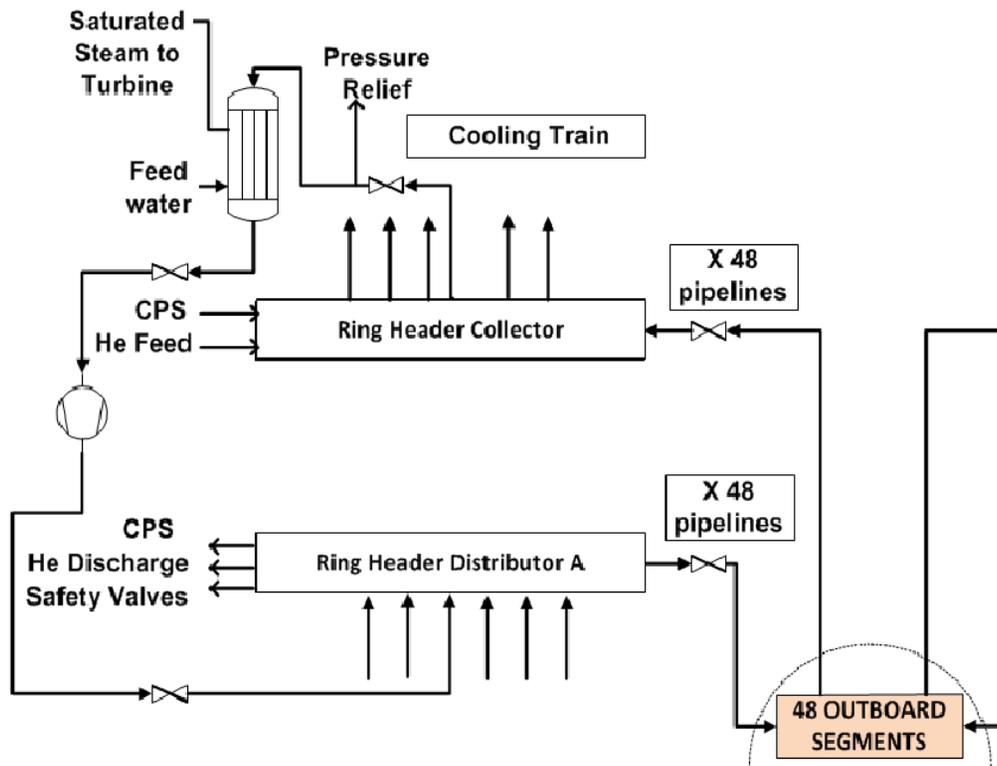
- DEMO is a tokamak machine as ITER;



DEMO & HCPB blanket concept (3/3)



PHTS description: Reference design



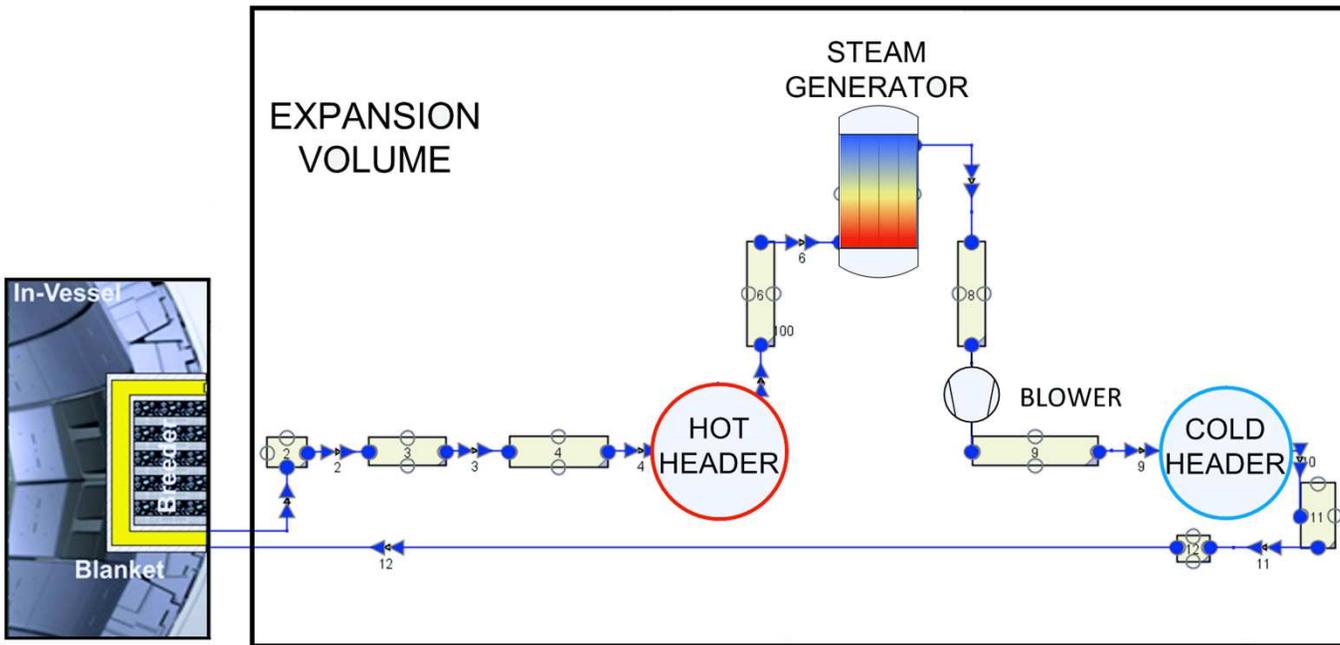
- Two independent coolant loops for the Out-Board (OB) segments and two for the In-Board (IB) ones. [2]

- He as coolant at 8.0 MPa in the temperature range of 300 – 500 °C. He inventory ~7000 kg each OB coolant loop. [3]

- Each OB loop removes 910.5 MW. [3]

- 6 Cooling trains (CTs) with one helicoidal steam generator each (5 operational and 1 spare). [2]

PHTS modellization: stationary run



- 13 CV (12–PHTS, 1-EV).
- 12 Flow Junction (FJs).
- 2 HSs (blanket and SG).

Characteristics	MELCOR
EV Volume [m ³]	70000.0
Heat transfer area [m ²]	15000.0
Blanket HS temp. [K]	773.15
SG HS temp. [K]	573.15
Total mass flow [kg/s]	875.5

Characteristics	MELCOR
EV Temperature [K]	313.35
Blanket temp. [K]	773.15
SG temp. [K]	573.15
Total pressure drop [MPa]	0.37
Heat flow [W/m ²]	60700.0

Stationary run results (1/2)

Parameter	Reference	1.8.2	2.1	Difference [%]
Blanket Total Pressure [MPa]	-	8.19	8.2	0.1 %
SG Total pressure [MPa]	-	7.82	7.83	0.1 %
Pressure drops [MPa]	0.37	0.37	0.37	0.0 %
Mass Flow rate [kg/s]	875.5	872.8	872.3	< 0.04 %
He mass [kg]	~ 6620.0	6795.4	6795.4	3.0 %
Blanket CV Temp. [K]	773.15	771.39	773.39	~ 0.2 %
Blanket HS Temp. [K]	773.15	773.43	781.61	< 1.1 %
SG CV Temp. [K]	573.15	573.83	573.82	~ 0.1 %
SG HS Temp. [K]	573.15	570.3	570.52	< 0.5 %
HTC Blanket [W/m ² K]	-	29686.8	7384.7	75.0 %
HTC SG [W/m ² K]	-	17221.8	18421.1	7.0 %

- The results of the stationary run are quite similar, but great differences exist on the inner heat transfer coefficients of the two HSs.

Stationary run results (2/2)

- Differences on the HTC → Due to the different temperature equilibrium among CV and HS.

$$q'' = HTC(T_{HS} - T_{CV})$$

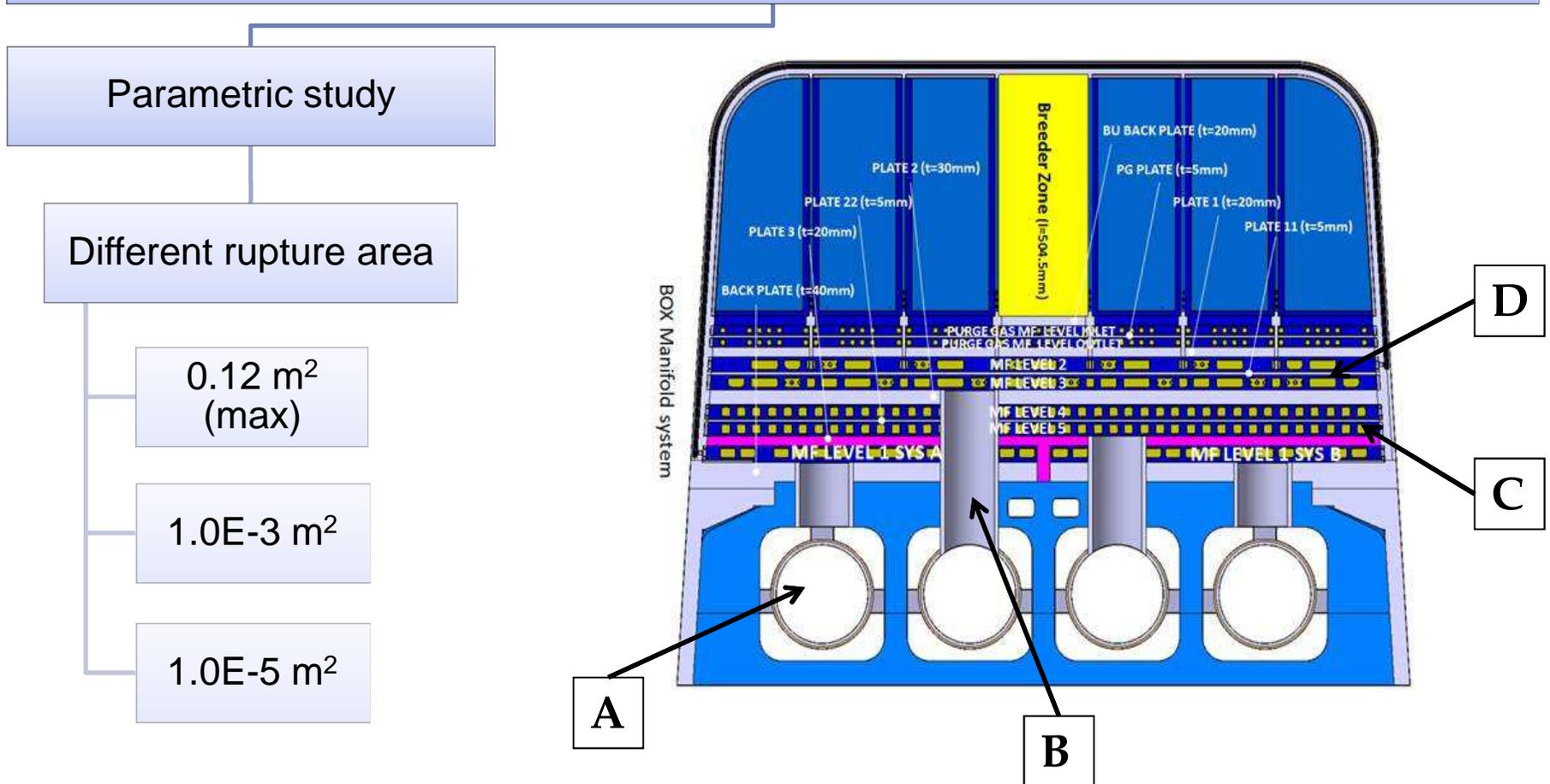
M 1.8.2 → To remove 60700.0 W/m² with a ΔT of 2.04 K an HTC of 29754.9 W/m²K is needed.

M 2.1 → To remove 60700.0 W/m² with a ΔT of 8.22 K an HTC of 7384.7 W/m²K is needed.

- No differences changing the default SC from 2.1 to 1.86.
- One difference exists: CPFPL and CPFAL (critical pool fractions) values.
 - In 1.8.2 set both to 0.0;
 - In 2.1 set >0.0 due to numerical error if set to 0.0
- Although, the stationary runs provide exhaustive results. Further analyses with complex nodalisations are required.

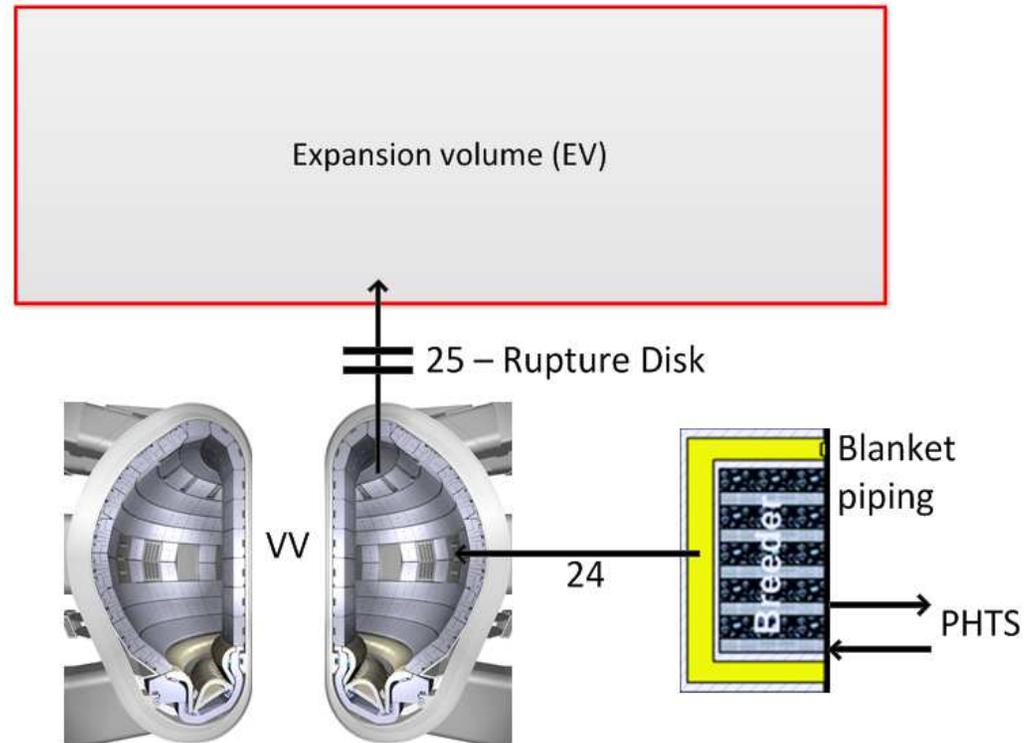
In-Vessel LOCA: Approach

Helium release inside the Vacuum Vessel (VV), and opening of a rupture disk connecting the VV and the Expansion Volume (EV) once reached the imposed set-point.



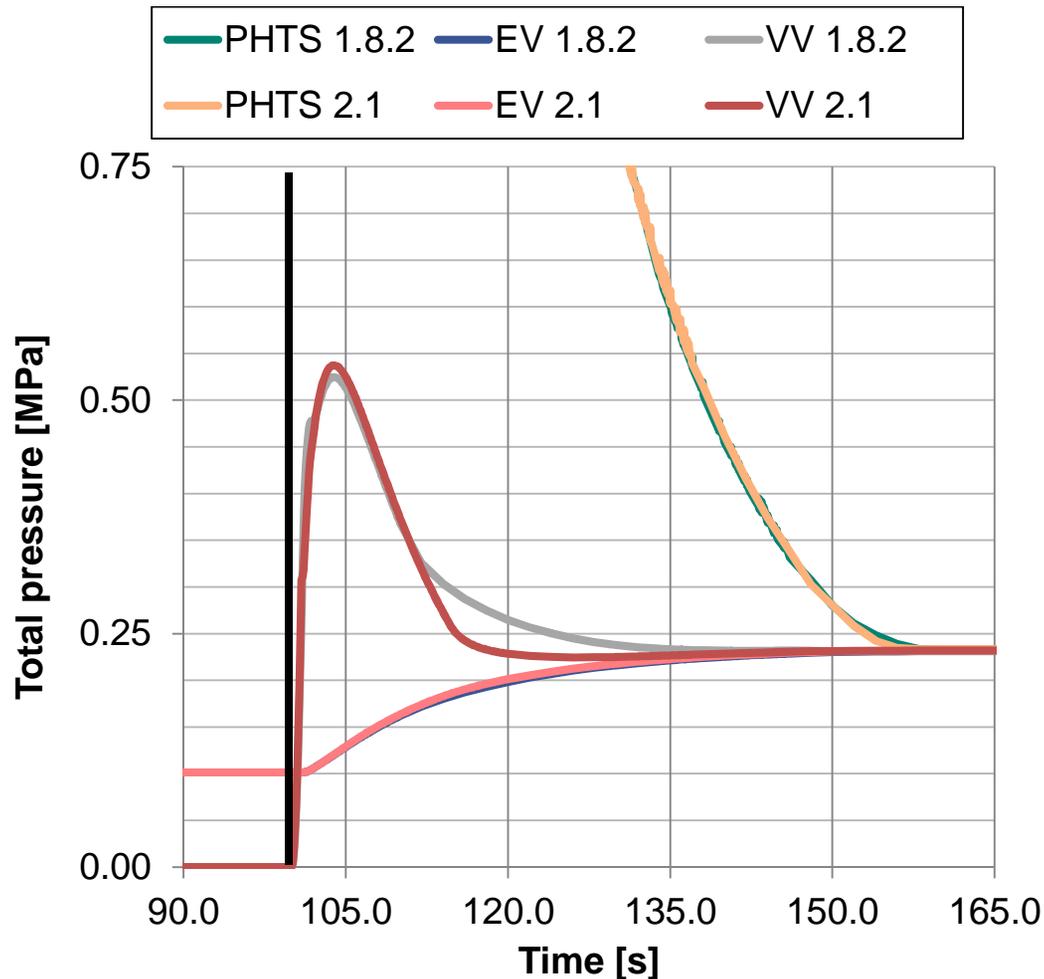
In-Vessel LOCA: modellisation

Parameter	MELCOR
EV Volume [m ³]	70000.0
EV temp. [K]	313.35
VV Pressure [Pa]	210.0
VV Volume [m ³]	1860.0
VV internal Temp. [K]	473.15
W dust mass [kg]	10.0
T mass [kg]	0.2
R. D. area [m ²]	1.0
R. D. set point [MPa]	0.15



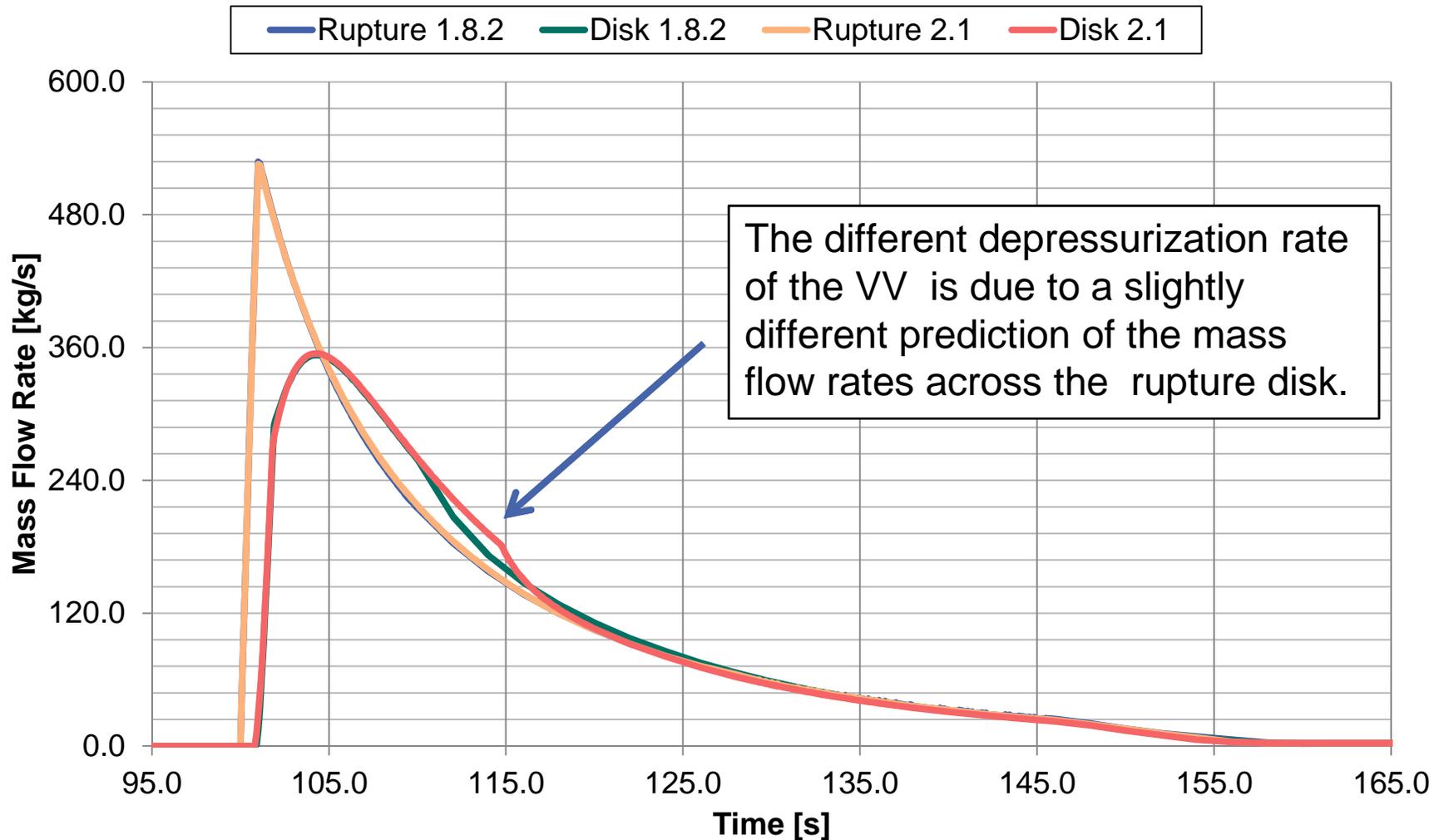
- PHTS as in stationary run.
- Rupture → Valve connecting PHTS and VV.
- VV as a single volume.
- Rupture disk connecting VV and EV.

In-Vessel LOCA: 0.12 m² (1/7)

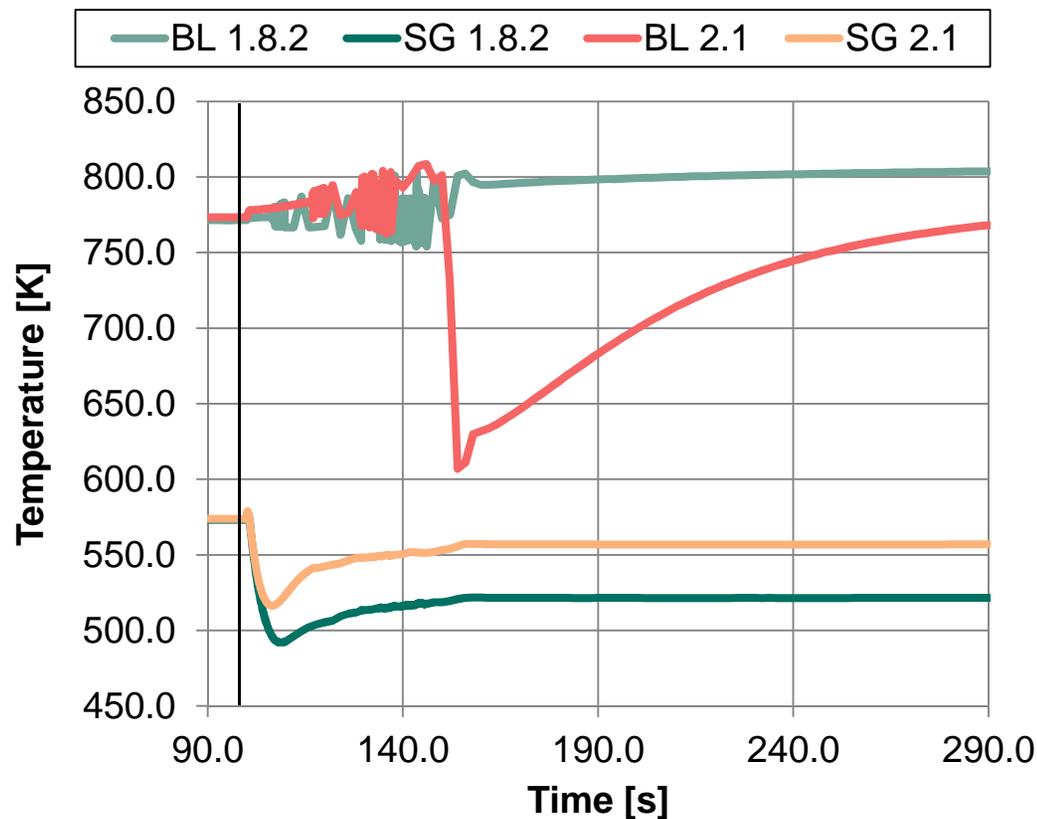


- Similar PHTS depressurization, but numerical instabilities in M 2.1.
- Similar EV depressurization.
- VV depressurization rate different, especially from 114.0 s to 135.0 s.
- The helium ingress inside the VV could cause the W dust mobilisation.

In-Vessel LOCA: 0.12 m² (2/7)

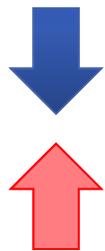


In-Vessel LOCA: 0.12 m² (3/7)



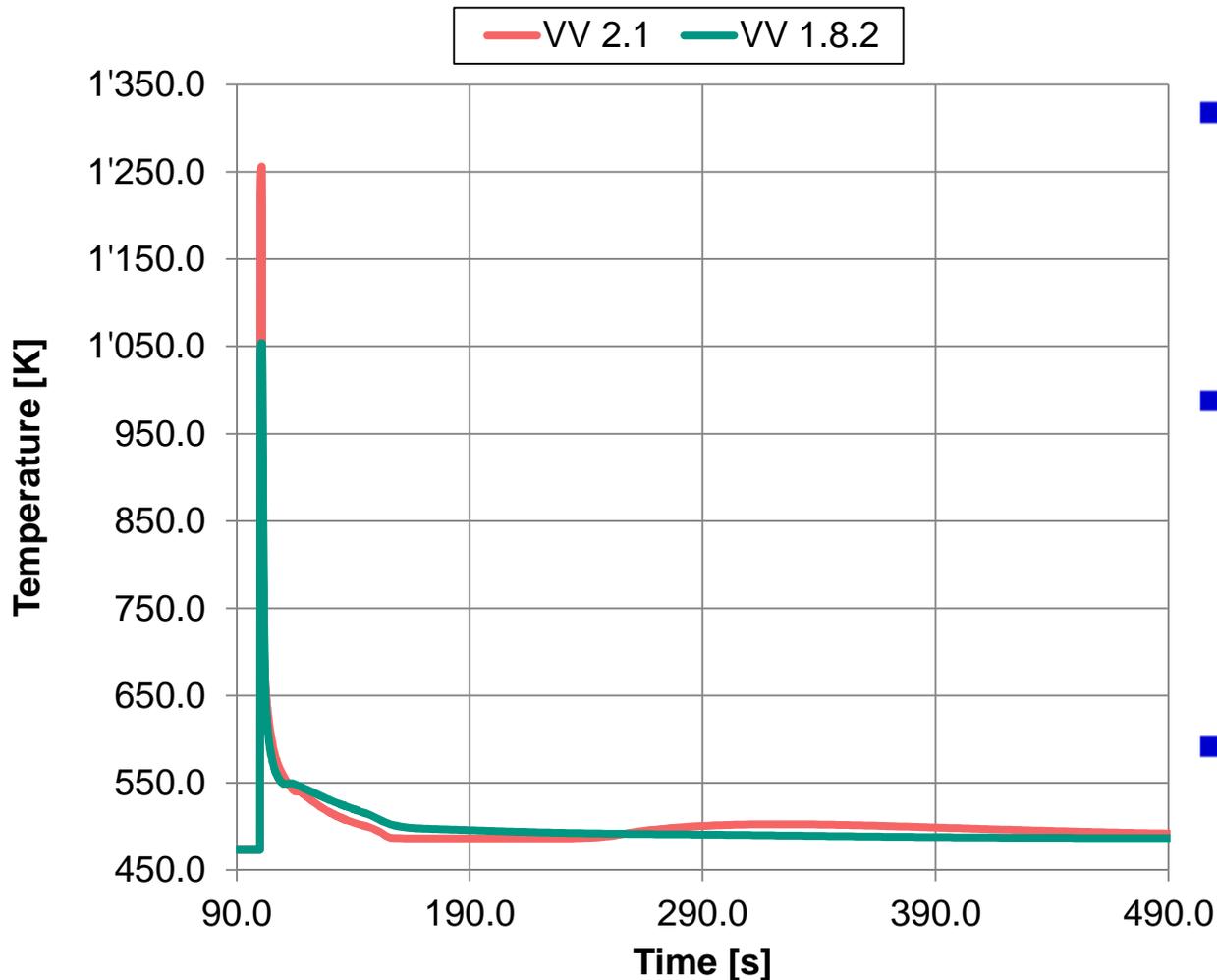
- Two phenomena influence the temperature trends.

- Helium expansion
- Unbalanced blanket-SG power.



- Blanket M 2.1 → temperature decrease when the VV and EV reach the same pressure.
- SG → Same trend, but different temperature decrease magnitude (~25 K).

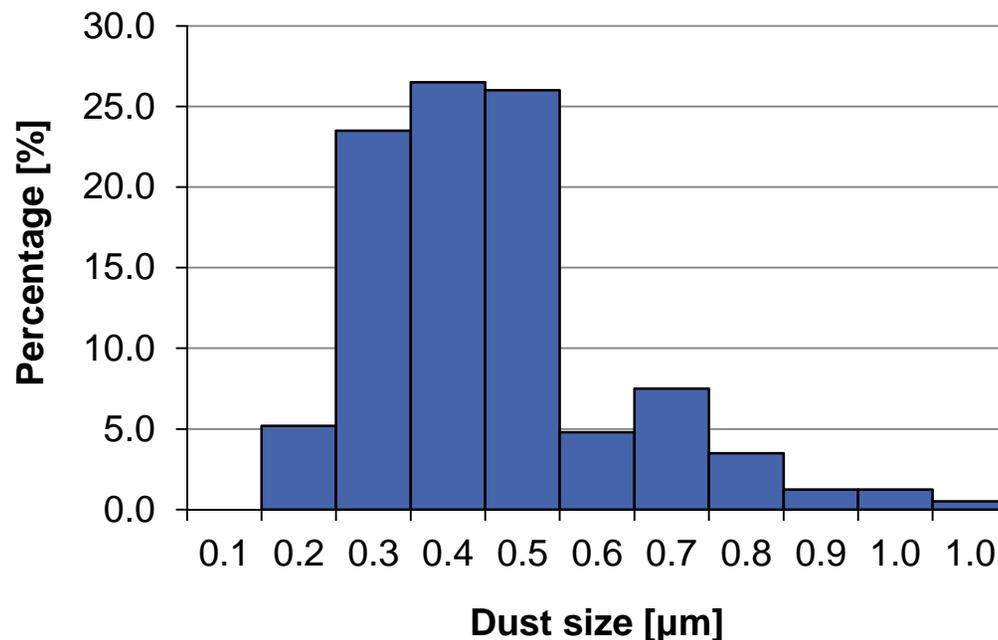
In-Vessel LOCA: 0.12 m² (4/7)



- Max VV temperature:
 - 1255 K – M 2.1
 - 1050 K – M 1.8.2
- Different temperature trends after 110.0 s
 - 150.0 s → M2.1 <15 K
 - 330.0 s → M2.1 >12 K
- No apparent causes for this behaviour (max. pressurization identical).

In-Vessel LOCA: 0.12 m² (5/7)

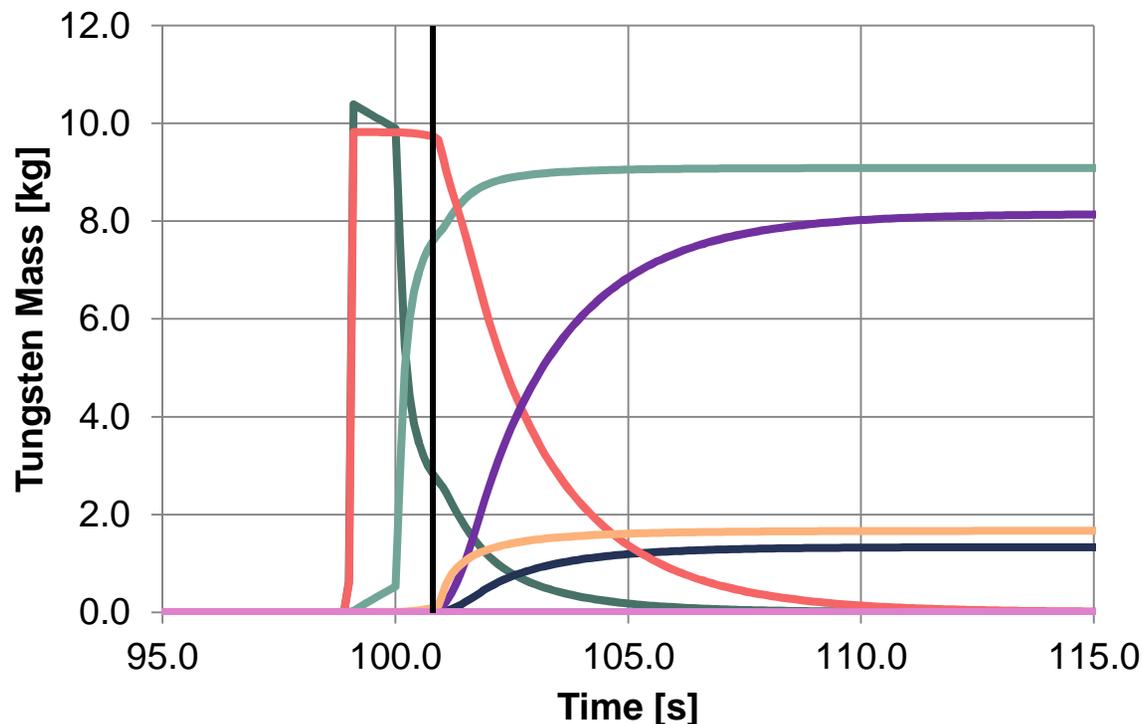
- The fast pressurization of the VV can lead to the W dust resuspension.
- W dust data taken from STARDUST experiment [4].
- M lacks of a resuspension model.



- Two cases investigate:
 - W injected 1 s before the rupture event.
 - W injected during the rupture event.

In-Vessel LOCA: 0.12 m² (6/7)

— VV atm 1.8.2 — EV atm 1.8.2 — VV dep 1.8.2 — EV dep 1.8.2
— VV atm 2.1 — EV atm 2.1 — VV dep 2.1 — EV dep 2.1



- M 1.8.2. → Injected mass overestimated (~200g).
- M 1.8.2 → W mass mainly deposited on VV.
- M2.1 → W mass mainly in EV atmosphere.
- M 2.1 results similar to ASTEC ones.
- Further investigation needed.

Conclusions

- Version-to-version comparison among M 1.8.2 (fusion version) and M 2.1.6342 employing the same nodalisation.
- Stationary run: Different blanket HTC value, but reliable and satisfactory results for both versions.
- In-Vessel run: Minor differences, except for the atmospheric temperatures and the W dust behaviour.
- In the future the introduction of fusion specific models of the 1.8.6 version inside the 2.1 version could be an interesting evolution.

Acknowledgments

- The work with MELCOR 1.8.2 has been performed at Karlsruhe Institute of Technology (KIT) at Karlsruhe (D).
- The work with MELCOR 2.1 has been performed at University of Pisa (UNIFI) at Pisa (I).

Thank you for your attention

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References

1. D. N. Dongiovanni, T. Pinna, and D. Carloni, "*RAMI Analysis for DEMO HCPB blanket concept cooling system*", Proceedings of Symposium of Fusion Technology 2014 (SOFT2014), San Sebastian, Spain, September 29-October 3, 2014.
2. M. D. Donne, "Conceptual Design of the Cooling System for a DEMO Fusion Reactor with Helium Cooled Solid Breeder Blanket and Calculation of the Transient Temperature Behavior in Accidents," Karlsruhe, 1992.
3. D. Carloni and S. Kecskes, "Helium Cooled Blanket Design Development," Karlsruhe, 2012.
4. M. T. Porfiri, N. Forgione, S. Paci and A. Rufoloni, "Dust mobilization experiments in the context of the fusion plants - STARDUST facility," in *Seventh International Symposium on Fusion Nuclear Technology - ISFNT-7 Part B*, 2006.