UPM Research with MELCOR 2.x. PWR-W Applications

EMUG, Brugg Switzerland

April 2019

Kevin Fernández-Cosials, César Queral, Gonzalo Jiménez.

Kevin.fcosials@upm.es



Index

- 1. A Little bit of history.
- 2. UPM Models (PWR-W, AP1000)
- 3. Research on In-Vessel Retention with portable equipment after LBLOCA
- 4. Research on Instrumentation survival
- 5. Conclusions
- 6. References



MELCOR history in the UPM

- UPM-CSN (Spanish Nuclear Safety Council) agreement to collaborate in CSARP (July 2017)
- The translation of Trillo NPP from MELCOR 1.8.5 to MELCOR 2.1 has been performed as part of the agreement between CSN and UPM.
- Previous works with MELCOR 1.8.3:
 - A PWR-W model was developed in the UPM and used for European report project.
- Currently UPM is working with different NPPs models (PWR-W, BWR, PWR-Siemens, AP1000) in several projects.



- PWR-Siemens (Trillo NPP)
 - Translation of the model from MELCOR 1.8.5 to 2.1
 - A set of sequences were used to verify the model





April, 2019

- PWR-W main features
 - Primary System
 - Secondary System up to Turbine admison Valves
 - RWST
 - Accumulators
 - HPSI, LPSI and Recirculation.



Based on: F. Martin-Fuertes *et al.*, "Analysis of three severe accident sequences (AB, SGTR and V) in a 3 loop W-PWR 900 MWe NPP with the MELCOR code," *European Commission*, vol. EUR 16054, 1994



- PWR-W Containment
 - More than 40 CV
 - Connected two-way
 - Containment Spray included





April, 2019

- PWR-W Vessel and core
 - 28 Heat Structures
 - 35 CV
 - 6 Rings 13 Levels





April, 2019

- PWR-W Control
 - Safety Injection System Control Modeled
 - PZR Control
 - Pumps performance
 - SCRAM













April, 2019

Study of <u>FLEX Strategies</u> with the MELCOR code:

- Simulation of a Recirculation Failure after LBLOCA
- Comparison of Different Time Failures
- Comparison with ASTEC
- Study with RN package included
- Simulation of using portable equipment after recirculation Failure to inject into RCS.



LBLOCA with recirculation failure

- Injection with Portable Equipment into RCS
- Option B is selected and simulated with MELCOR 2.2





IYNCWiN18 Bariloche, Argentina



Correct Behavior of the Primary System and Containment pressure after LBLOCA



April, 2019





April, 2019





April, 2019





April, 2019

• Comparison with ASTEC (KWU) MBLOCA

- Cladding Melting (~3600 s vs ~3300 s after recirc Loss)
- Relocation in Lower Plenum (~ 4600 s vs ~ 5200 s after recirc Loss)
- Vessel Failure (~ 9000 s vs ~ 11600 s after recirc Loss)



Ref: Investigation of SAM measures during selected MBLOCA sequences along with Station Blackout in a generic Konvoi PWR using ASTECV2.0. Ignacio García Gomez-Toraño et al. Annals of Nuclear Energy Volume 105, July 2017, Pages 226-239

April, 2019

• Behavior of Core Temperature along different FLEX INJECTIONS

| | | Recirculation failure since recriculation begins | | | | | | | | | | | |
|------------|----------|---|--------|--------|---------|---------|---------|---------|---------|---------|--|--|--|
| | | 0 min | 10 min | 70 min | 130 min | 190 min | 250 min | 310 min | 370 min | 430 min | | | |
| | | | | | | | | | | | | | |
| | 30 min | | | | | | | | | | | | |
| | 60 min | | | | | | | | | | | | |
| FLEX | 90 min | Calculation of the different Reponses against a | | | | | | | |) | | | |
| Invection | 120 min | injection of water in a degraded care with pertable | | | | | | | | | | | |
| time since | 150 min | injection of water in a degraded core with portable | | | | | | | | le | | | |
| failure | 180 min | equipment. (Also using different equipment) | | | | | | | | | | | |
| | 210 min | | | | | | | | | | | | |
| | 240 min | | | | | | | | | | | | |
| | >270 min | | | | | | | | | | | | |



April, 2019

• Behavior of Core Temperature along different FLEX INJECTIONS





European Melcor Users Group, Switzerland





April. 2019

• Behavior of Core Temperature along different FLEX Injections

| Safe State | | | | |
|--------------------------|--|--|--|--|
| PCT > 1477 K | | | | |
| Fuel Melting | | | | |
| Corium Relocation | | | | |
| Vessel Failure | | | | |

| G = 20 kg/s | | Recirculation failure since recriculation begins | | | | | | | | | |
|--|----------|--|--------|--------|---------|---------|---------|---------|---------|---------|--|
| | | 0 min | 10 min | 70 min | 130 min | 190 min | 250 min | 310 min | 370 min | 430 min | |
| FLEX Inyection time since failure | 30 min | SS | SS | SS | SS | SS | SS | SS | SS | SS | |
| | 60 min | FM | FM | SS | SS | SS | SS | SS | SS | SS | |
| | 90 min | CR | CR | FM | FM | FM | CD | SS | SS | SS | |
| | 120 min | CR | CR | FM | FM | FM | FM | FM | CD | CD | |
| | 150 min | CR | CR | CR | FM | FM | FM | FM | FM | FM | |
| | 180 min | CR | CR | CR | CR | CR | CR | FM | FM | FM | |
| | 210 min | VF | CR | CR | CR | CR | CR | CR | CR | CR | |
| | 240 min | VF | VF | VF | CR | CR | CR | CR | CR | CR | |
| | >270 min | VF | VF | VF | VF | VF | VF | VF | VF | VF | |



European Melcor Users Group, Switzerland

• Behavior of Core Temperature along different FLEX Injections.

| G = 20 kg/s | | | Recirculation failure since recriculation begins | | | | | | | |
|--|----------|-------|--|--------|---------|---------|---------|---------|---------|---------|
| | | 0 min | 10 min | 70 min | 130 min | 190 min | 250 min | 310 min | 370 min | 430 min |
| FLEX Inyection time since failure | 30 min | SS | SS | SS | SS | SS | SS | SS | SS | SS |
| | 60 min | FM | FM | SS | SS | SS | SS | SS | ss | SS |
| | 90 min | CR | CR | FM | FM | FM | CD | SS | SS | SS |
| | 120 min | CR | CR | FM | FM | FM | FM | FM | CD | CD |
| | 150 min | CR | CR | CR | FM | FM | FM | FM | FM | FM |
| | 180 min | CR | CR | CR | CR | CR | CR | FM | FM | FM |
| | 210 min | VF | CR | CR | CR | CR | CR | CR | CR | CR |
| | 240 min | VF | VF | VF | CR | CR | CR | CR | (CR) | CR |
| | >270 min | VF | VF | VF | VF | VF | VF | VF | VF | VF |



Behavior of Core Temperature along different FLEX Injections:

- After 270 min without injection, it is not posible to avoid vessel Failure
- If more than 25 tons of corium are relocated in the Lower Plenum, vessel failure is very likely (same conclusion as ASTEC).
- It is better to inject in the RCS as soon as possible, more than delaying the failure of the recirculation.



Behavior of Core Temperature along different FLEX Injections.

- Enveloping Strategy to overcome lack of convergence
- Inference of accident progression if too small DT.
- MELCOR 2.2 used (more stable)
- DT max study provided 0.01 sec as the most stable
- Lack of convergence (small DT) cannot be esily predicted, sometimes causing Failure in apparently non-problematic scenarios.
- Reflooding of the hot core decreases the DT up to 1E-06 during the process.
- No problem detected in cases without Hot core reflooding.



Study of <u>Instrumentation Survival</u> with the MELCOR code:

- LBLOCA with Recirculation Failure (SBO) is simulated.
- Instrumentation Survival during a Severe Accident
- Use of a subdivided containment to localize each instrument and obtain "local conditions"
- Developing a strategy for instrumentation Reading based on survivability.



Study of Instrumentation Survival with the MELCOR code:

- Containment subdivided in several Rooms to provide a higher resolution on Temperature.
- Other studies have similar objectives and outcomes



Ref: J. L. Rempe, D. L. Knudson, and R. J. Lutz, "Scoping Study Investigating PWR Instrumentation during a Severe Accident Scenario," 2015



April, 2019

Study of Instrumentation Survival with the MELCOR code:

- Definition of different Damage Conditions of the Instrumentation
- Dose not taken into account in the present study (future research lines)

| Damage Condition 0 | Normal Operating Conditions |
|--------------------|---|
| Damage Condition 1 | Anomalous operating conditions I. The operating conditions are challenging or above the design, but useful measurements in tendency and values are still obtained. |
| Damage Condition 2 | Anomalous operating conditions II. The limit is greatly surpassed, and measurements on value are no longer valid. The information on tendency and order of magnitude is still useful. |
| Damage Condition 3 | Damage Operating Conditions. The instrument measurements are only reliable in terms of tendencies, not values or orders of magnitude. |
| Damage Condition 4 | Destruction Conditions . The measurements lack of any value and they should not be used at all. |



Study of Instrumentation Survival with the MELCOR code:

- LBLOCA with SBO at 5200 sec
- Different temperatures for different locations and containment compartments





April, 2019

Study of Instrumentation Survival with the MELCOR code:

- Damage condition Evolution of the different instrumentation systems.
- Actions within the SAMGs make use of this instrumentation but no regard on which is the most reliable instrument.





April, 2019





Time [s]

PWR-W MELCOR Conclusions

- 1. PWR-W MELCOR Model used in the UPM is allowing the study of different accidents.
- 2. A SA scenario involving Portable equipment is simulated adequately with MELCOR 2.2
- 3. An enveloping strategy and careful choosing of parameters is used to determine the damage condition of the core and vessel and retain numerical stability.
- 4. A detailed containment and RCS nodalization allows to obtain "local" conditions of the instrumentation, which permits the study of the instrumentation survivability.



PWR-W MELCOR Main References

- 1. J. L. Rempe, D. L. Knudson, and R. J. Lutz, "Scoping Study Investigating PWR Instrumentation during a Severe Accident Scenario," 2015
- 2. Investigation of SAM measures during selected MBLOCA sequences along with Station Blackout in a generic Konvoi PWR using ASTECV2.0. Ignacio García Gomez-Toraño et al. Annals of Nuclear Energy Volume 105, July 2017, Pages 226-239
- 3. D. J. Hanson, W. C. Arcieri, and L. W. Ward, "Assessing information needs and instrument availability for a pressurized water reactor during severe accidents," *Nuclear Engineering and Design*, vol. 148, no. 2–3, pp. 233–252, Jul. 1994
- F. Martin-Fuertes *et al.*, "Analysis of three severe accident sequences (AB, SGTR and V) in a 3 loop W-PWR 900 MWe NPP with the MELCOR code," *European Commission*, vol. EUR 16054, 1994
- 5. J. L. Rempe and D. L. Knudson, "TMI-2 A Case Study for PWR Instrumentation Performance During a Severe Accident. INL/EXT-13-28043," 2013
- 6. N. Chikhi, J. Fleurot, Revisiting the QUENCH-11 integral reflood test with a new thermal– hydraulic model: Existence of a minimum injection rate Ann. Nucl. Energy, 49 (2012), pp. 12-22



Thank you very much for your attention



April, 2019