

Cross-walk study between MELCOR, ASTEC and MAAP: LB LOCA scenario and encountered modeling issues for the MELCOR 2.2.21402

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12th – 14th April 2023

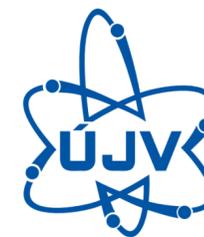
JSI, Ljubljana, Slovenia

14th Meeting of the European MELCOR and MACCS User Group (EMUG)



OVERVIEW

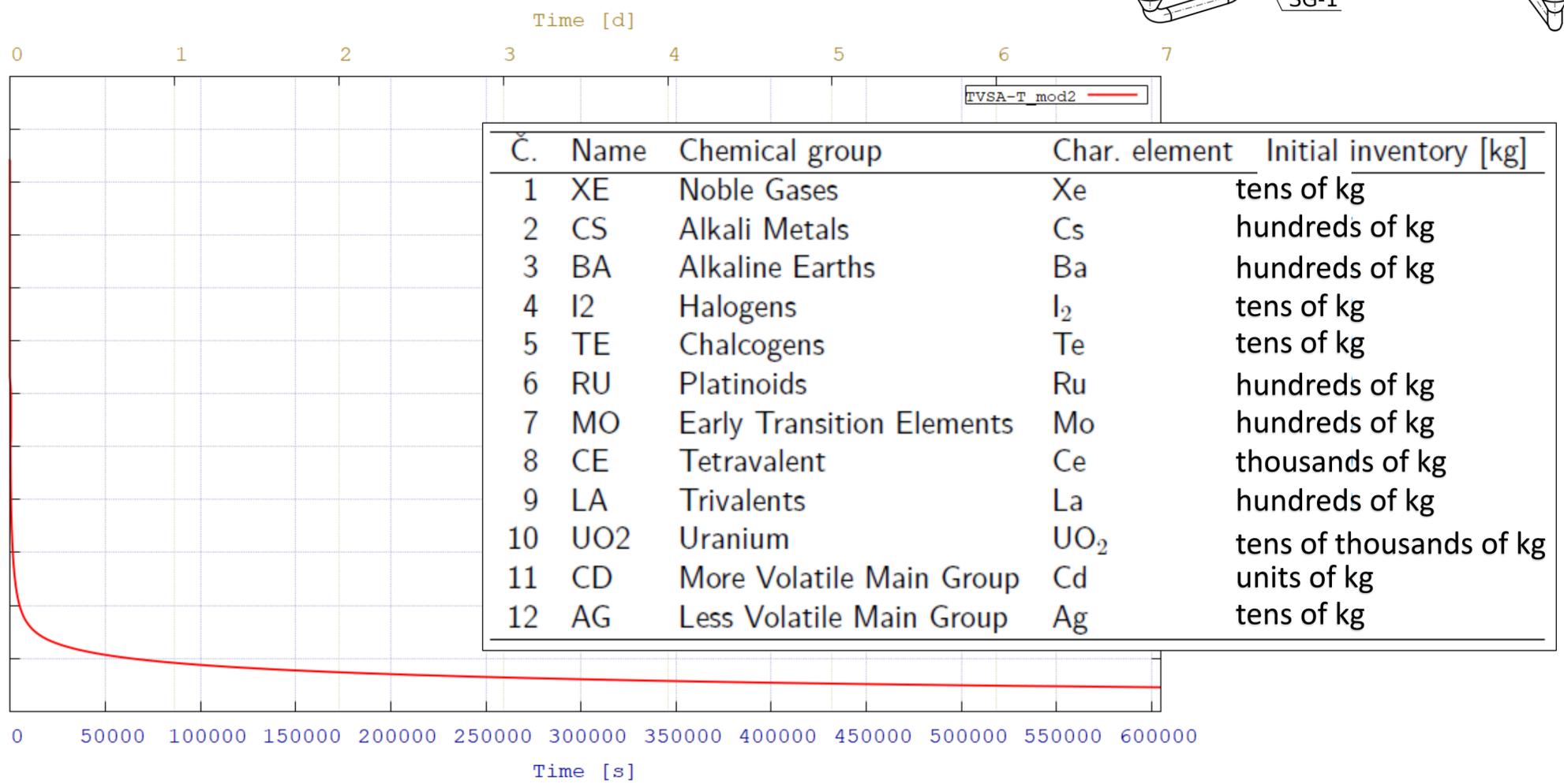
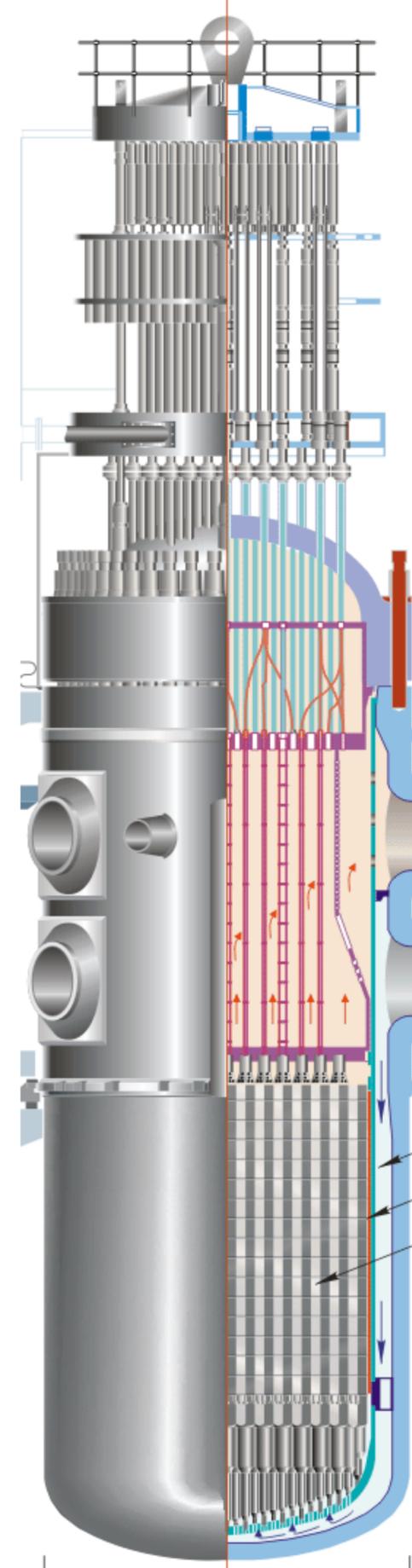
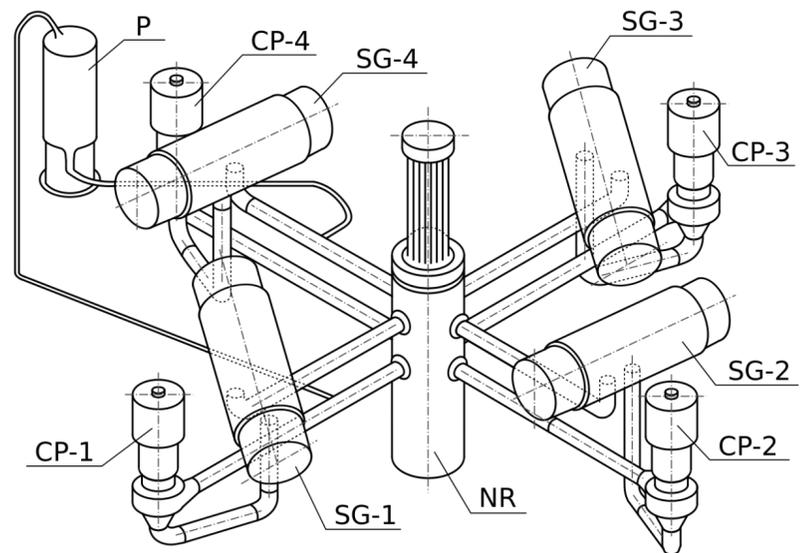
1. New input model of the VVER-1000 core
 - FAs: TVSA-T mod1 => mod2
 - Substantially enhanced oxidation
2. Benchmark analysis of LB LOCA scenario for VVER-1000
 - ASTEC/MELCOR/MAAP
 - Discrepancies in the LP molten mass
3. Encountered MELCOR issues (21402)
 - Unfailed LH even if completely molten
 - SPR package: spray is ON, but no heat/mass transfer



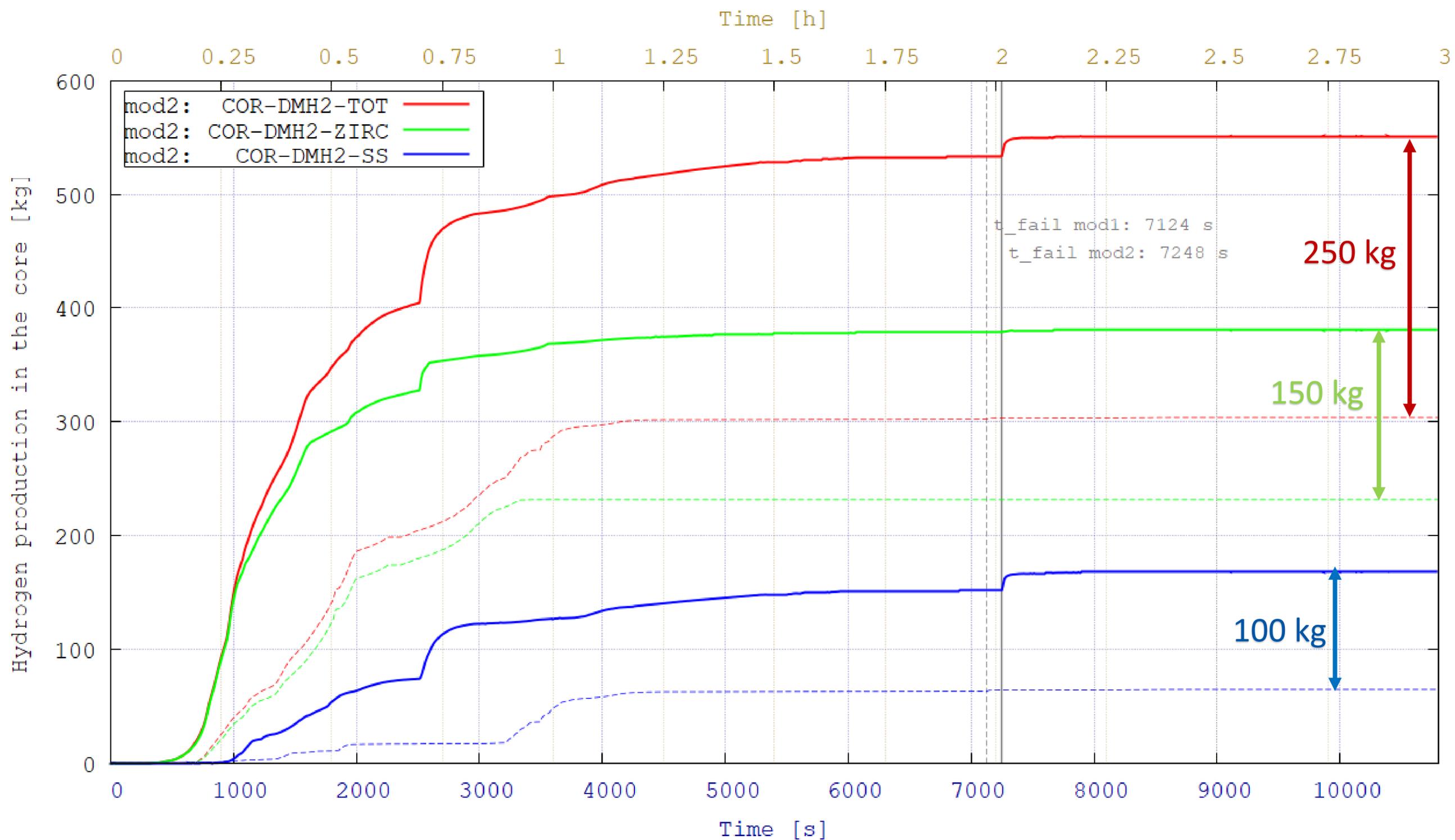
New input model of the VVER-1000 core

VVER-1000/320 (TEMELIN NPP)

- New FAs (TVEL TVSA-T mod2) modeled (8 => 15 SGs)
- Realistic decay power & FP inventory calculated
- SCALE/TRITON sequence used



TVSA-T MOD1 VS. MOD2: HYDROGEN PRODUCTION



TVSA-T MOD1 VS. MOD2: SURFACE AREA ETC.

- 8 vs. 15 SGs

- SA of all SGs in the core: 1269 vs. 2141 m²

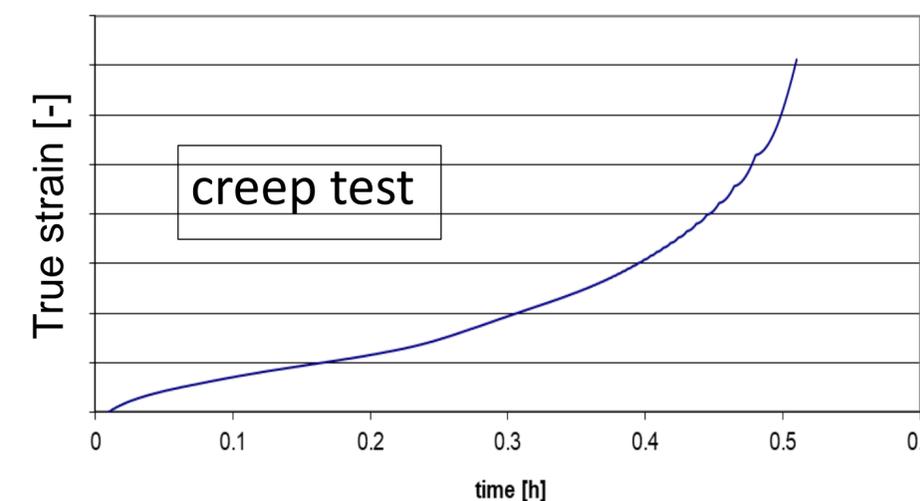
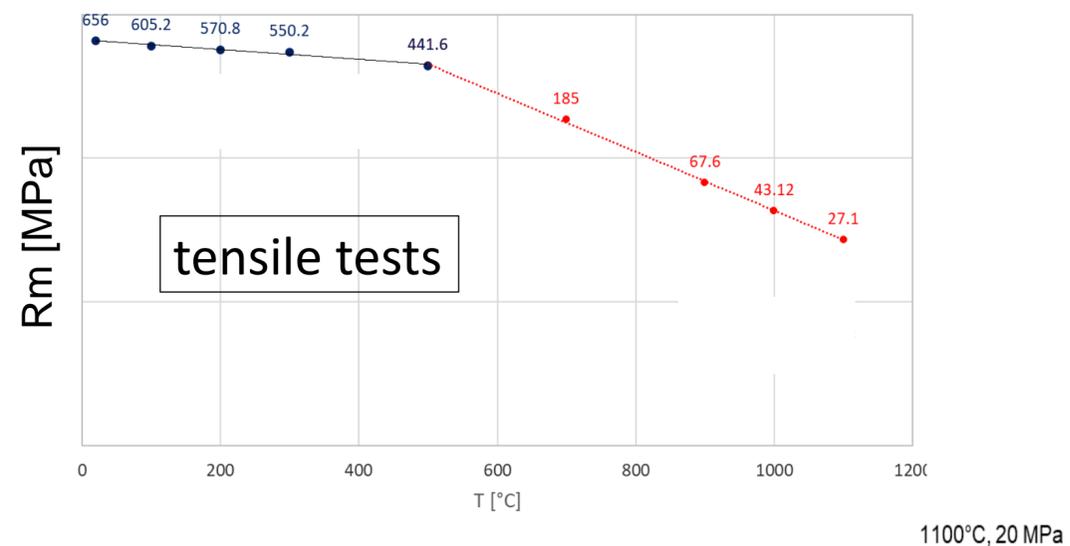
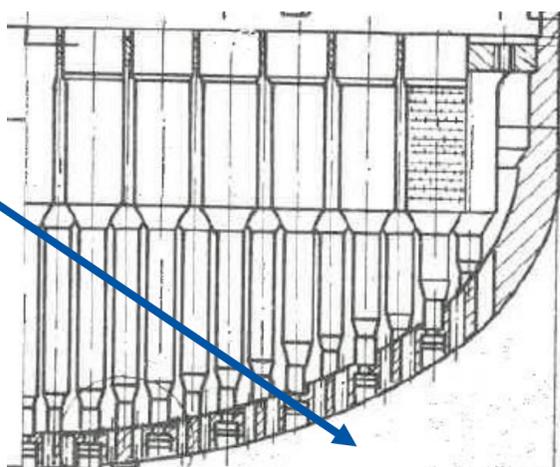
piece	SA_unit [m ²]	# units in FA	SA_FA [m ²]	ratio
cladding	0.1066	312	33.26	2.53
SG	0.9733	13.5	13.14	

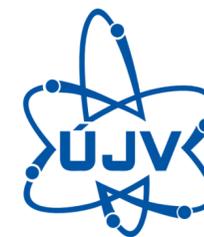
- Accelerated degradation of steel SS-component supporting capabilities

- Updated failure & collapse temperatures (lowered): investigation of σ_{UTS} and creep properties
- PD more prone to oxidation than MP?

- PD retention within the perforated core barrel LH

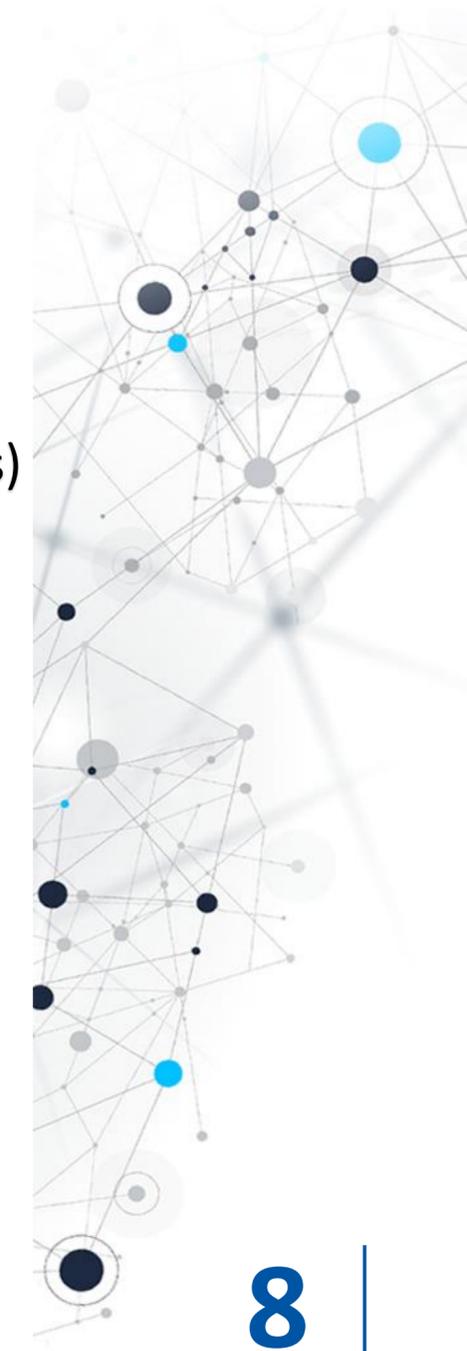
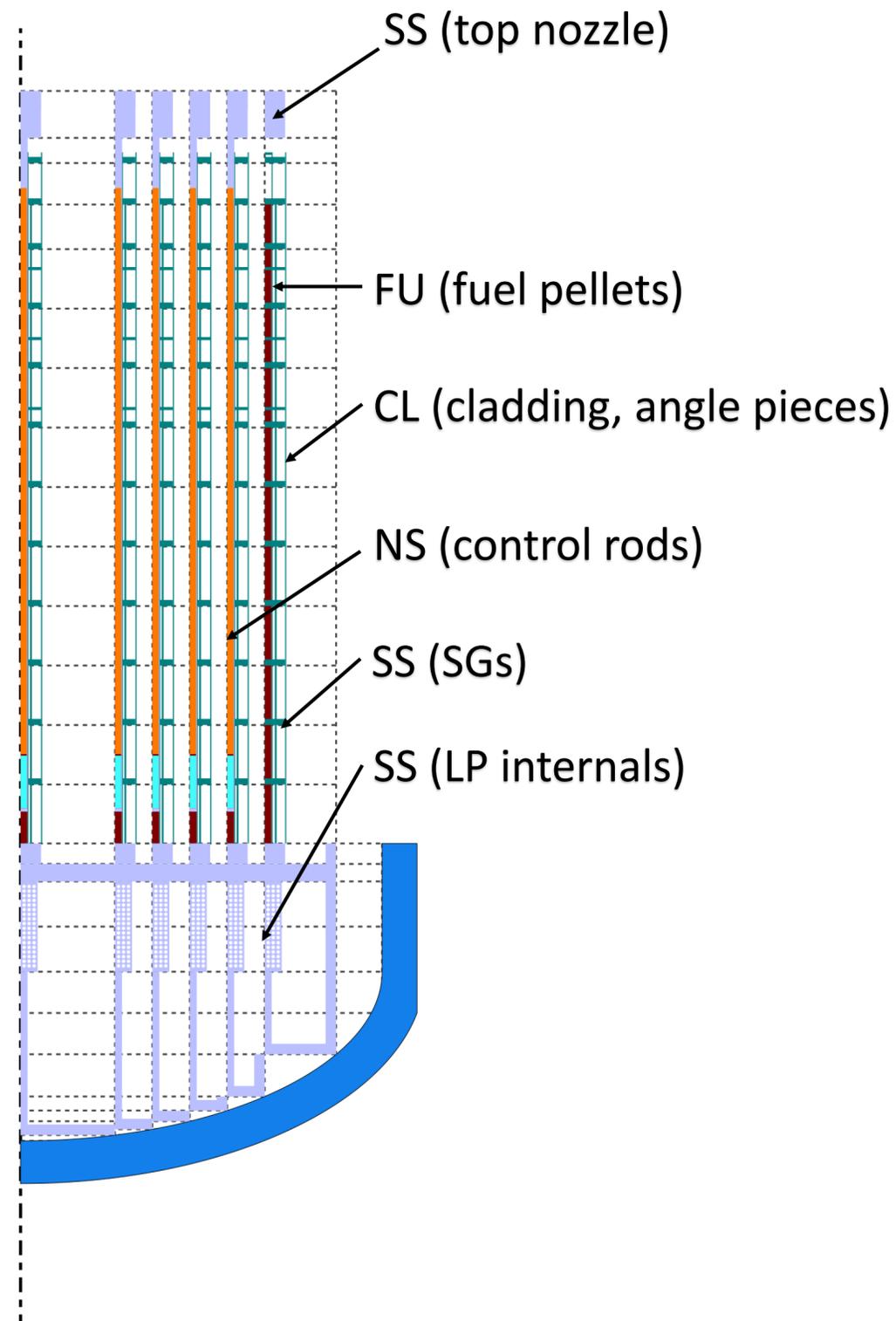
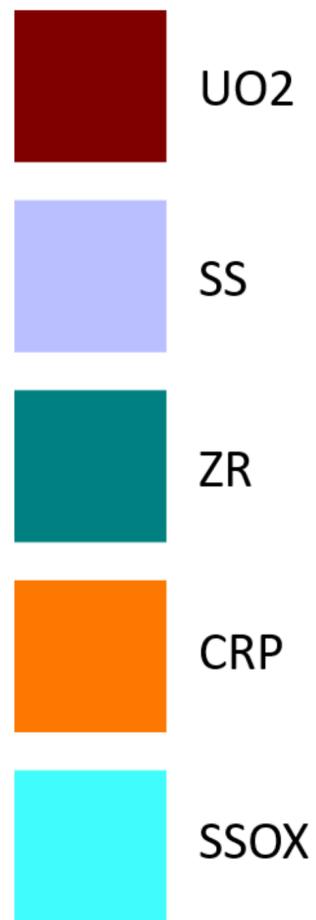
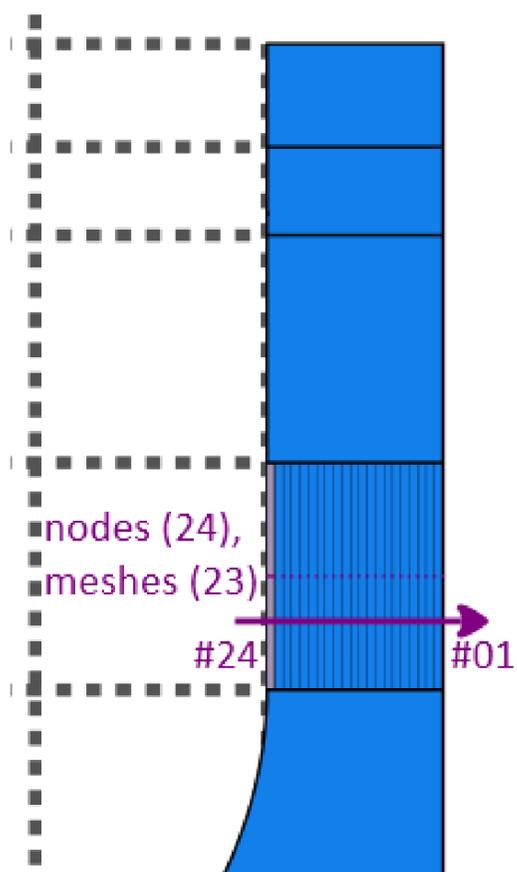
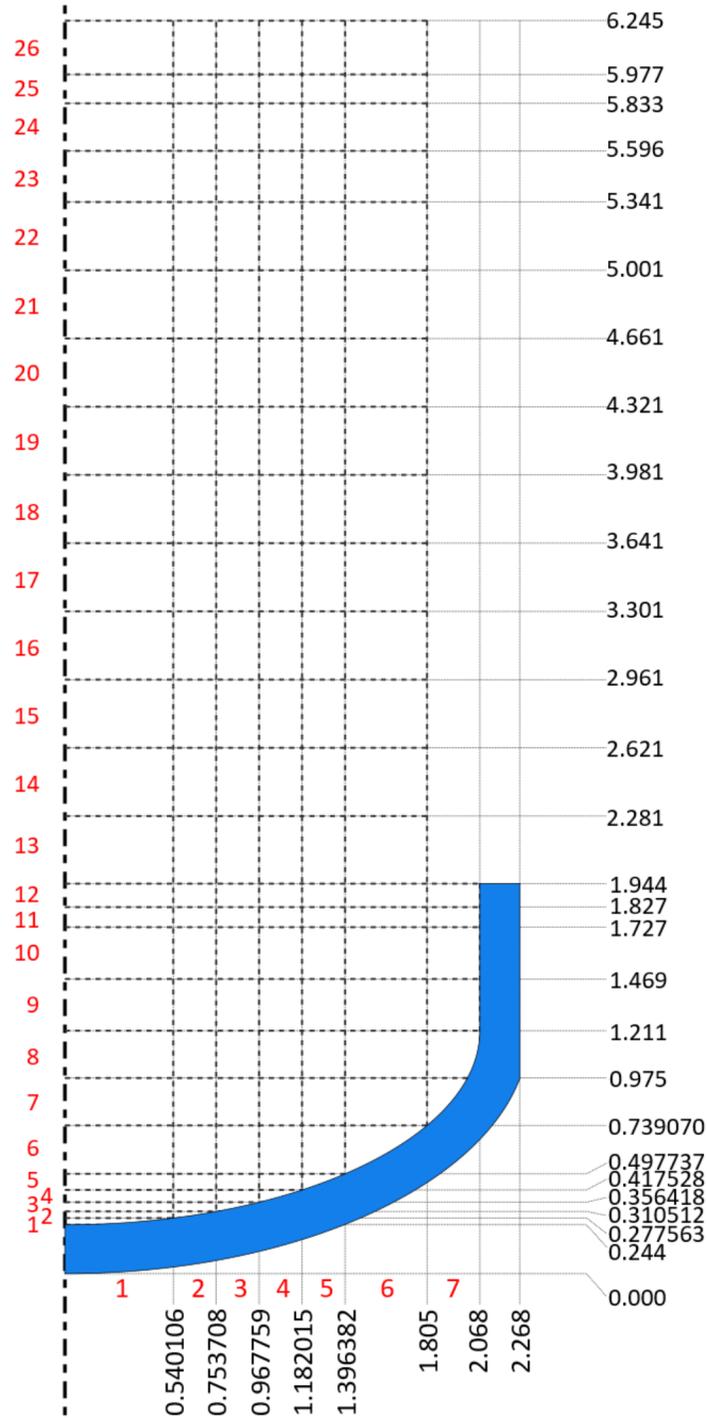
- Experimental investigation
- Water access into the gap barrel \Leftrightarrow RPV
- => prolonged oxidation



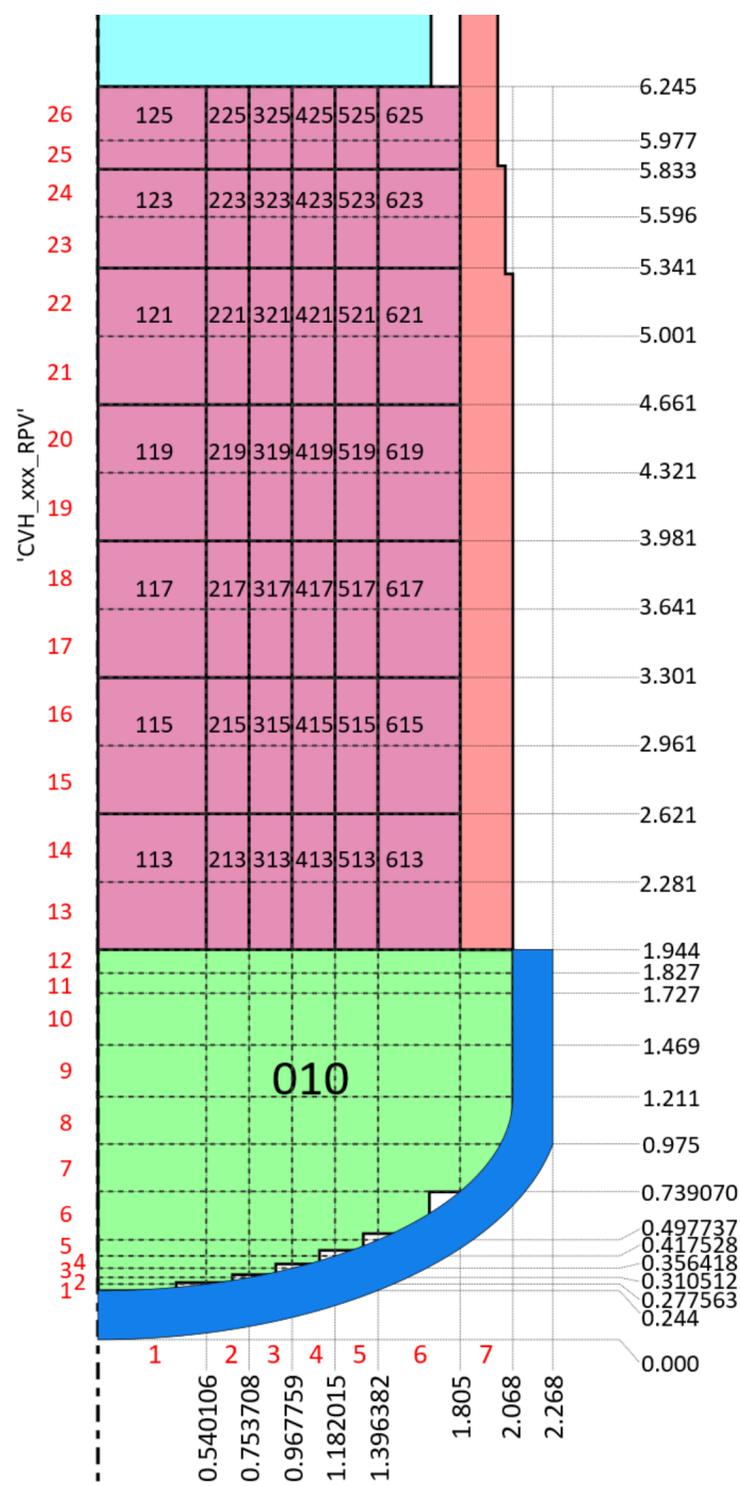


Benchmark analysis of LB LOCA scenario for VVER-1000

MELCOR NODALIZATION: COR

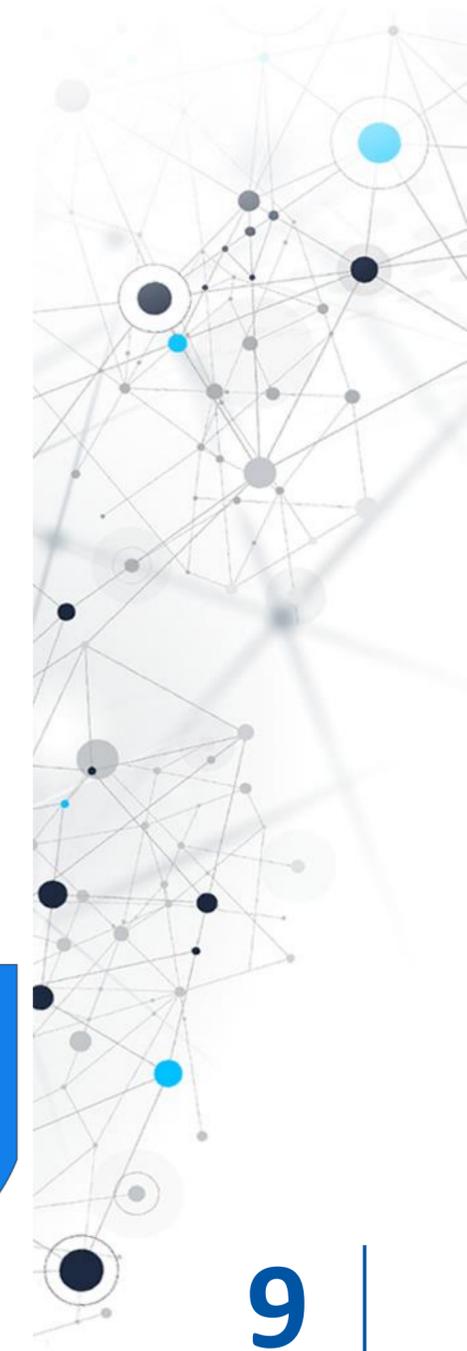
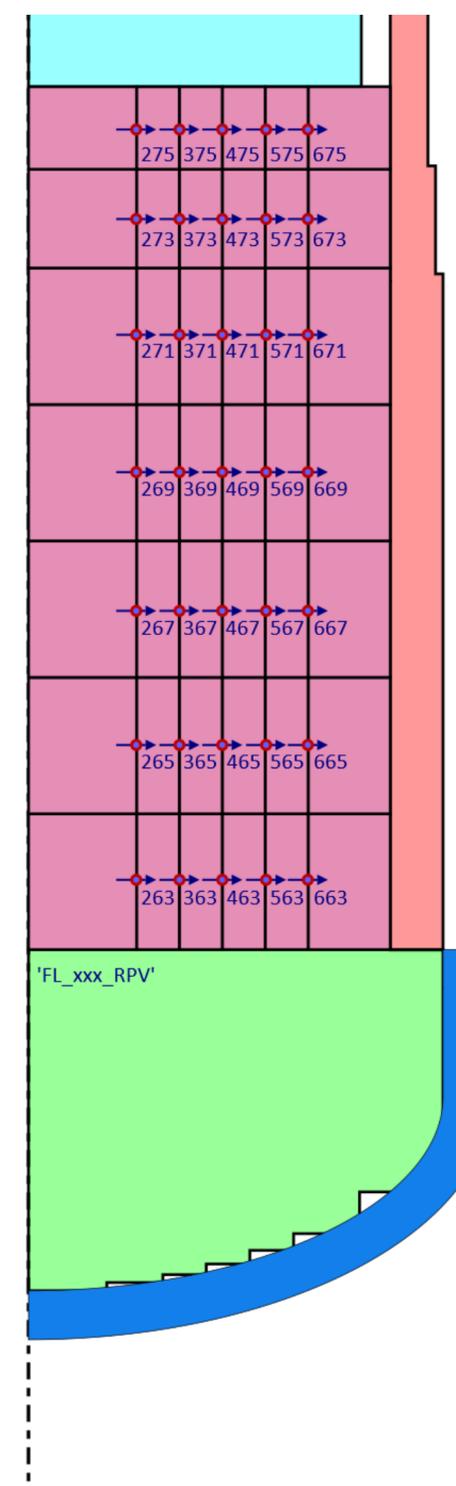
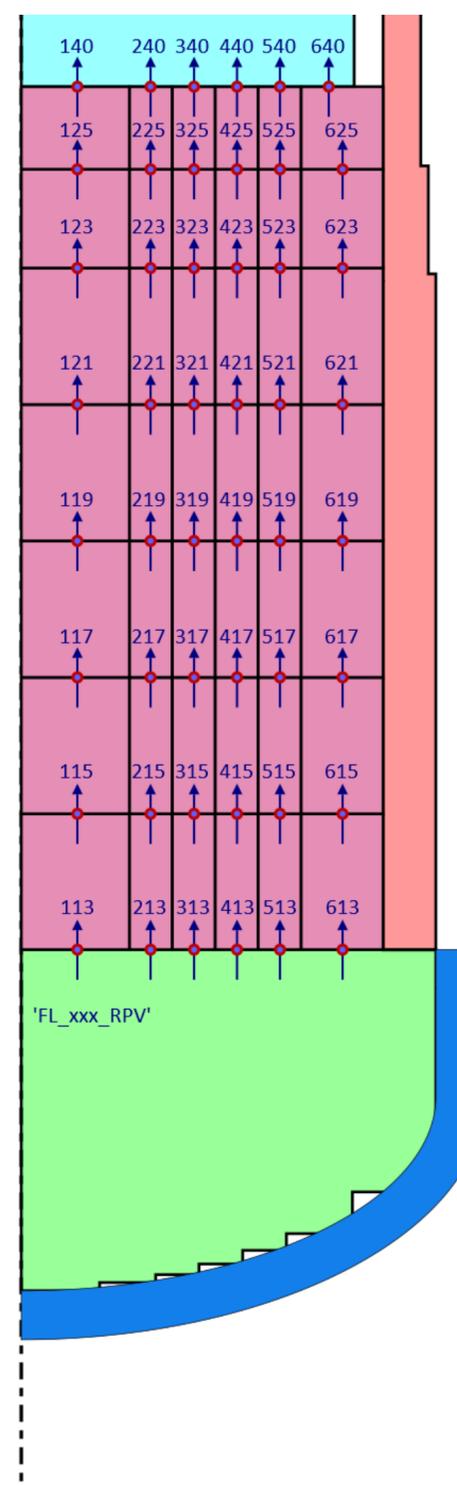


MELCOR NODALIZATION: CV, FL

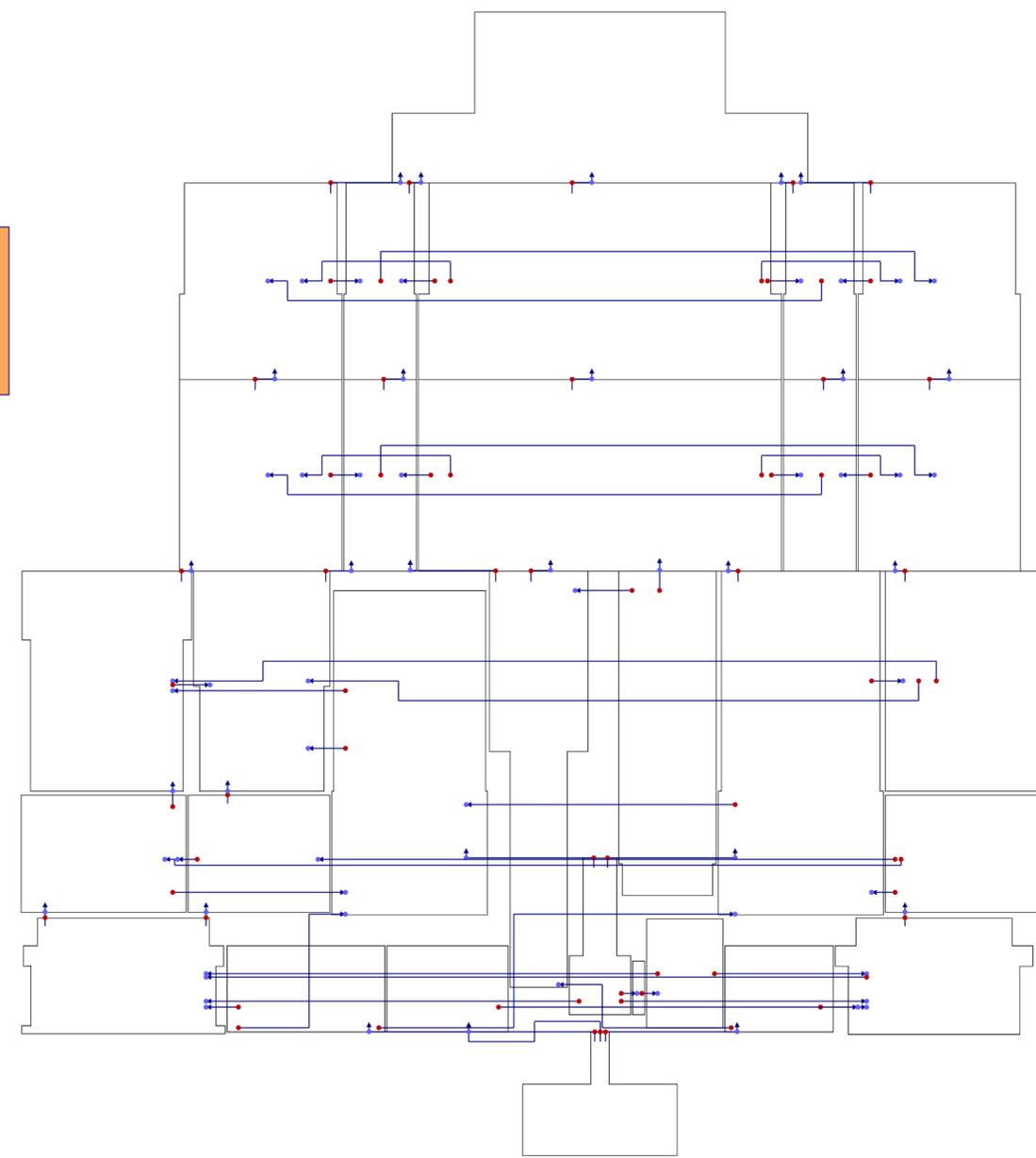
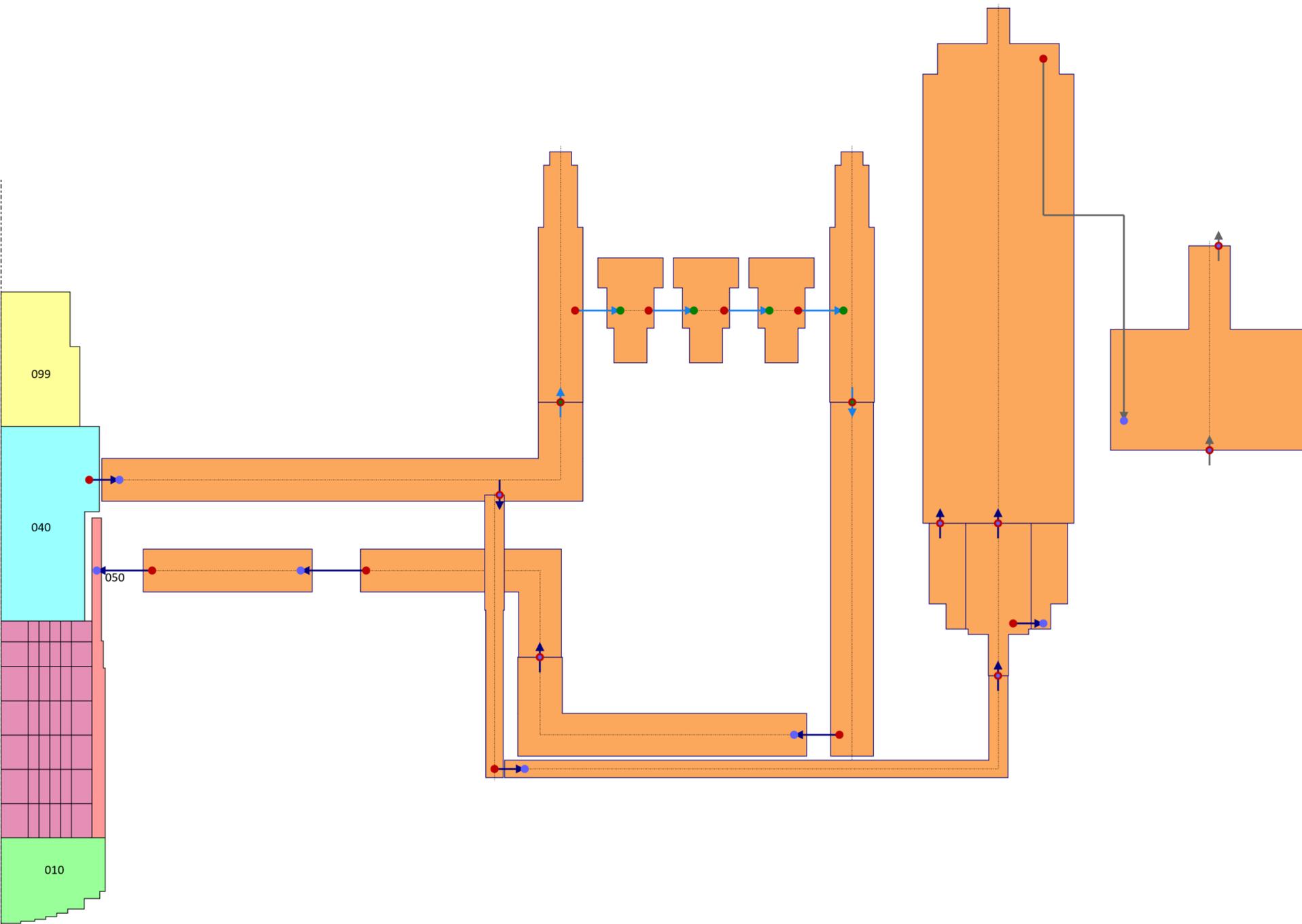


2 COR cells per 1 CV

A. I. #/r. r. #	1	2	3	4	5	6	7
26	40	40	40	40	40	40	50
25	125	225	325	425	525	625	50
24	125	225	325	425	525	625	50
23	123	223	323	423	523	623	50
22	123	223	323	423	523	623	50
21	121	221	321	421	521	621	50
20	121	221	321	421	521	621	50
19	119	219	319	419	519	619	50
18	119	219	319	419	519	619	50
17	117	217	317	417	517	617	50
16	117	217	317	417	517	617	50
15	115	215	315	415	515	615	50
14	115	215	315	415	515	615	50
13	113	213	313	413	513	613	50
12	113	213	313	413	513	613	50
11	10	10	10	10	10	10	10
10	10	10	10	10	10	10	10
9	10	10	10	10	10	10	10
8	10	10	10	10	10	10	10
7	10	10	10	10	10	10	10
6	10	10	10	10	10	10	'NULL'
5	10	10	10	10	10	'NULL'	'NULL'
4	10	10	10	10	'NULL'	'NULL'	'NULL'
3	10	10	10	'NULL'	'NULL'	'NULL'	'NULL'
2	10	10	'NULL'	'NULL'	'NULL'	'NULL'	'NULL'
1	10	'NULL'	'NULL'	'NULL'	'NULL'	'NULL'	'NULL'



MELCOR NODALIZATION: PC, CTMT



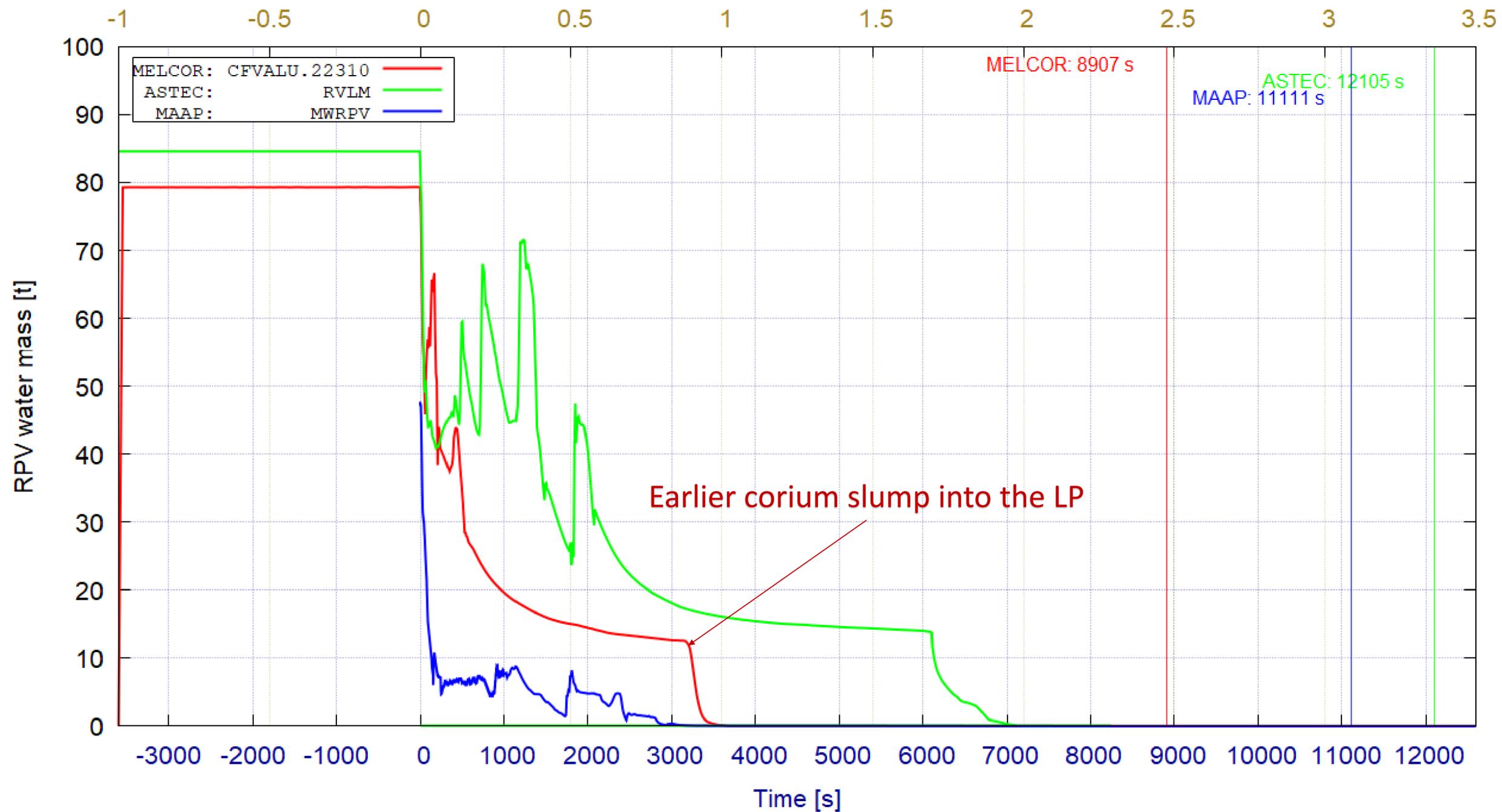
SCENARIO DEFINITION, CODES USED

- LB LOCA (equivalent $\varnothing 200$ mm) @ CL of 4th loop (single, with connected PRZ)
- SBO => no active systems
- Without IVMR => RPV failure
- Codes used:
 - *MELCOR 2.2.21402*
 - *ASTEC V3.1*
 - *MAAP 5.03-VVER*
- Results:
 - Red- MELCOR: $t_{\text{RPV-failure}} = 8907$ s (2.47 h)
 - Green-ASTEC: $t_{\text{RPV-failure}} = 12105$ s (3.36 h)
 - Blue- MAAP: $t_{\text{RPV-failure}} = 11111$ s (3.09 h)

RPV WATER INVENTORY

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAP

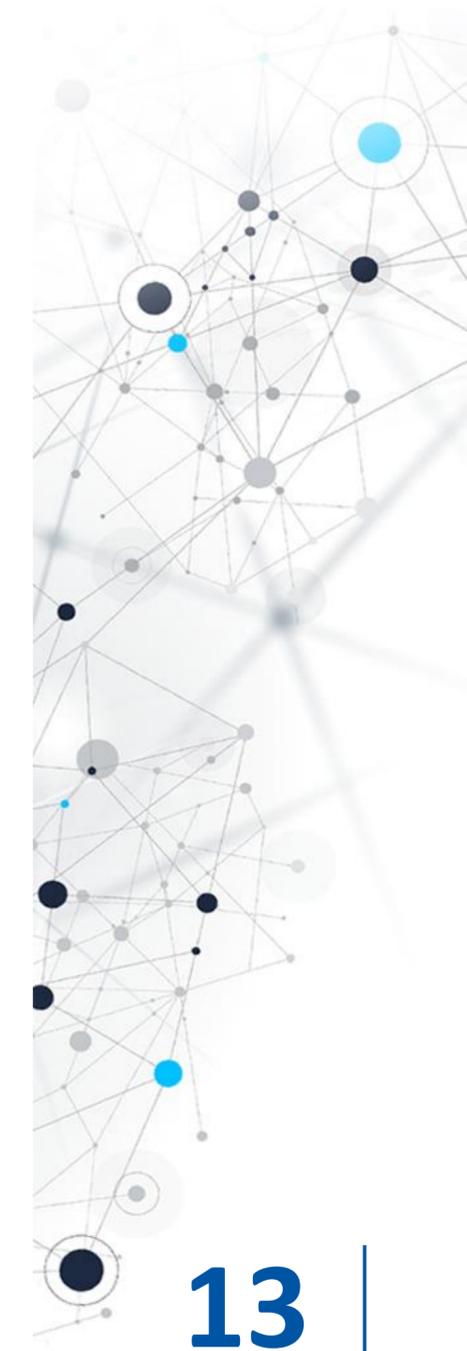
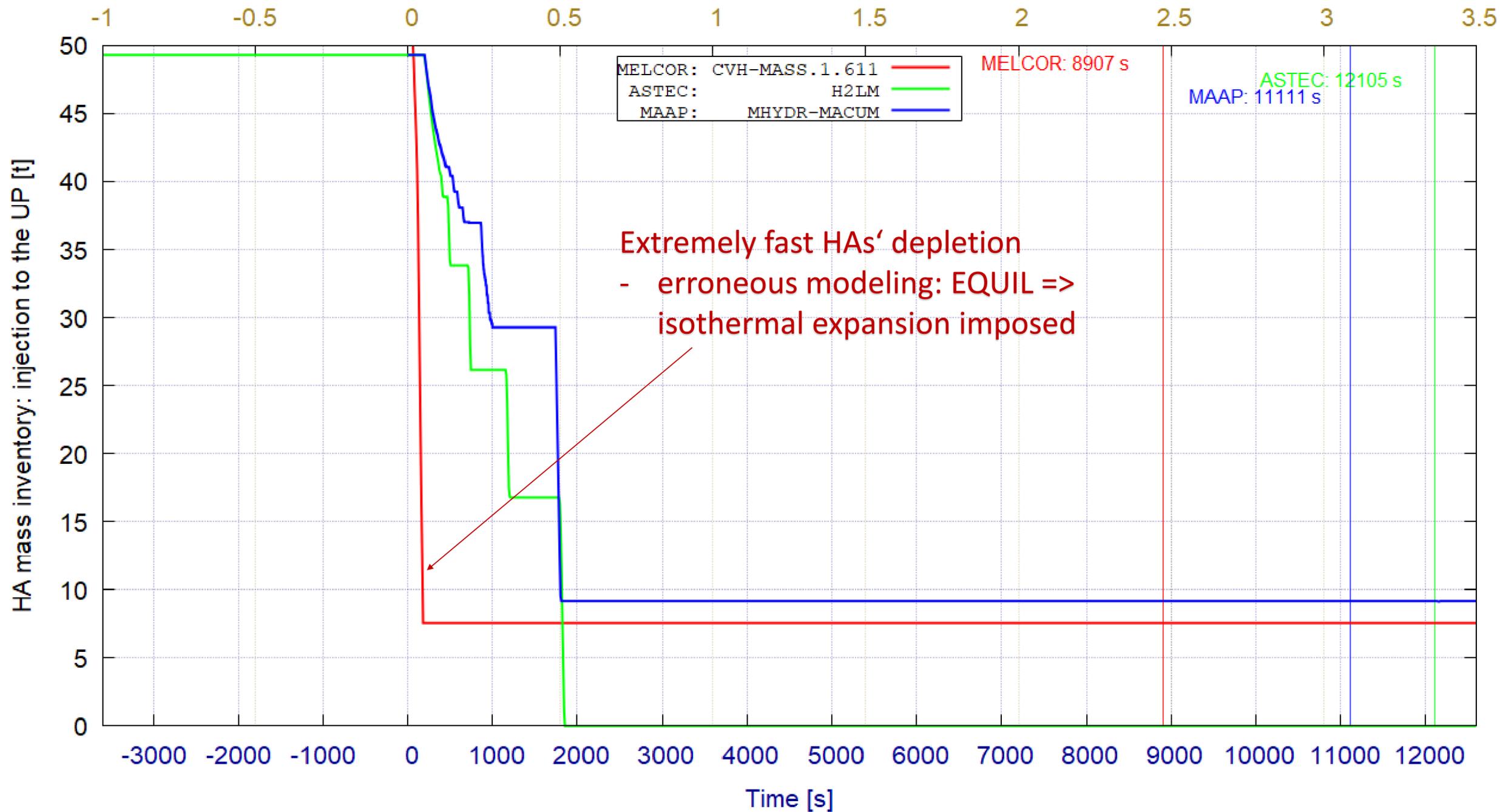
Time [h]



HA INJECTION

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAAP

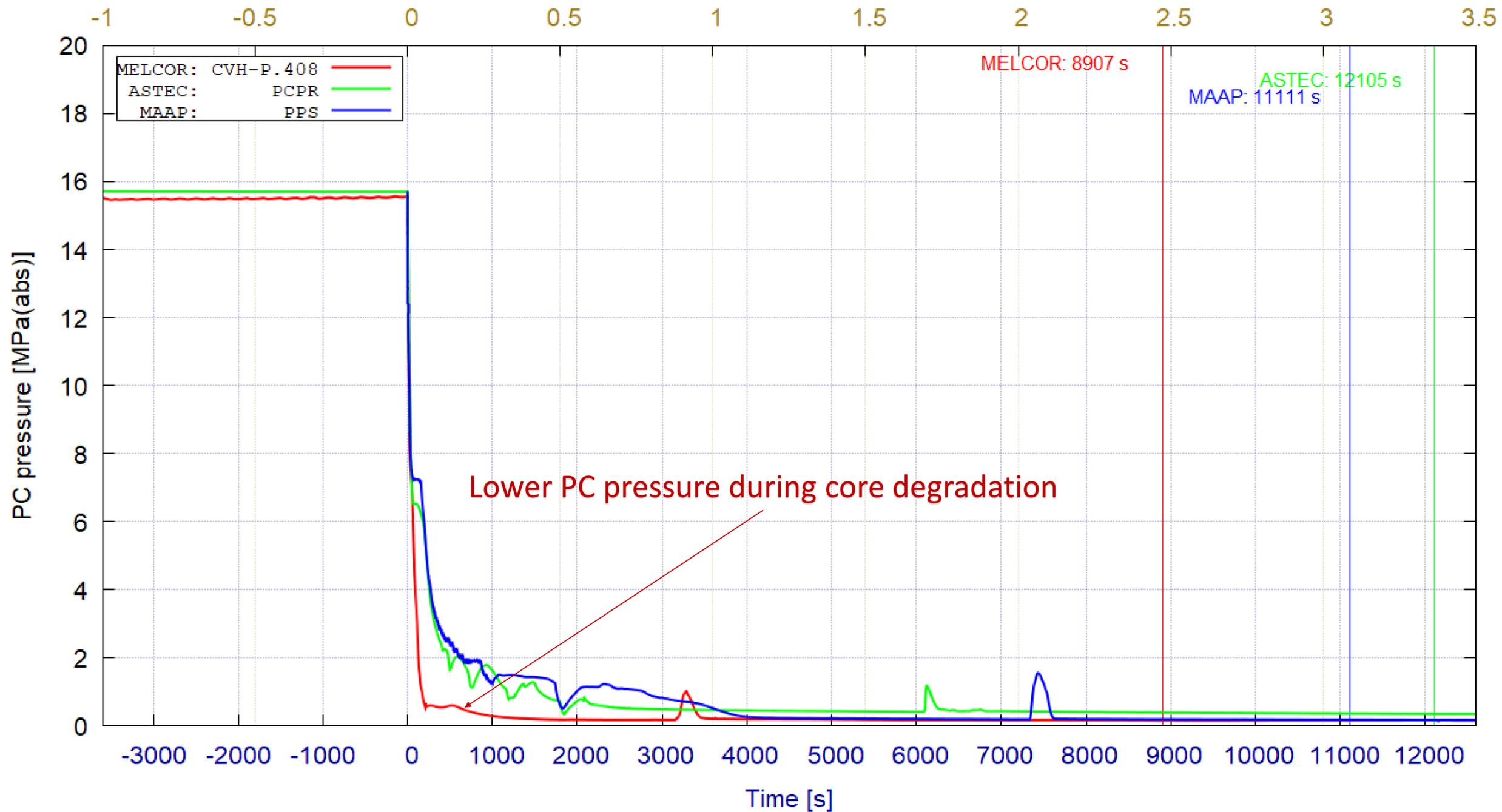
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PRIMARY PRESSURE

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAA

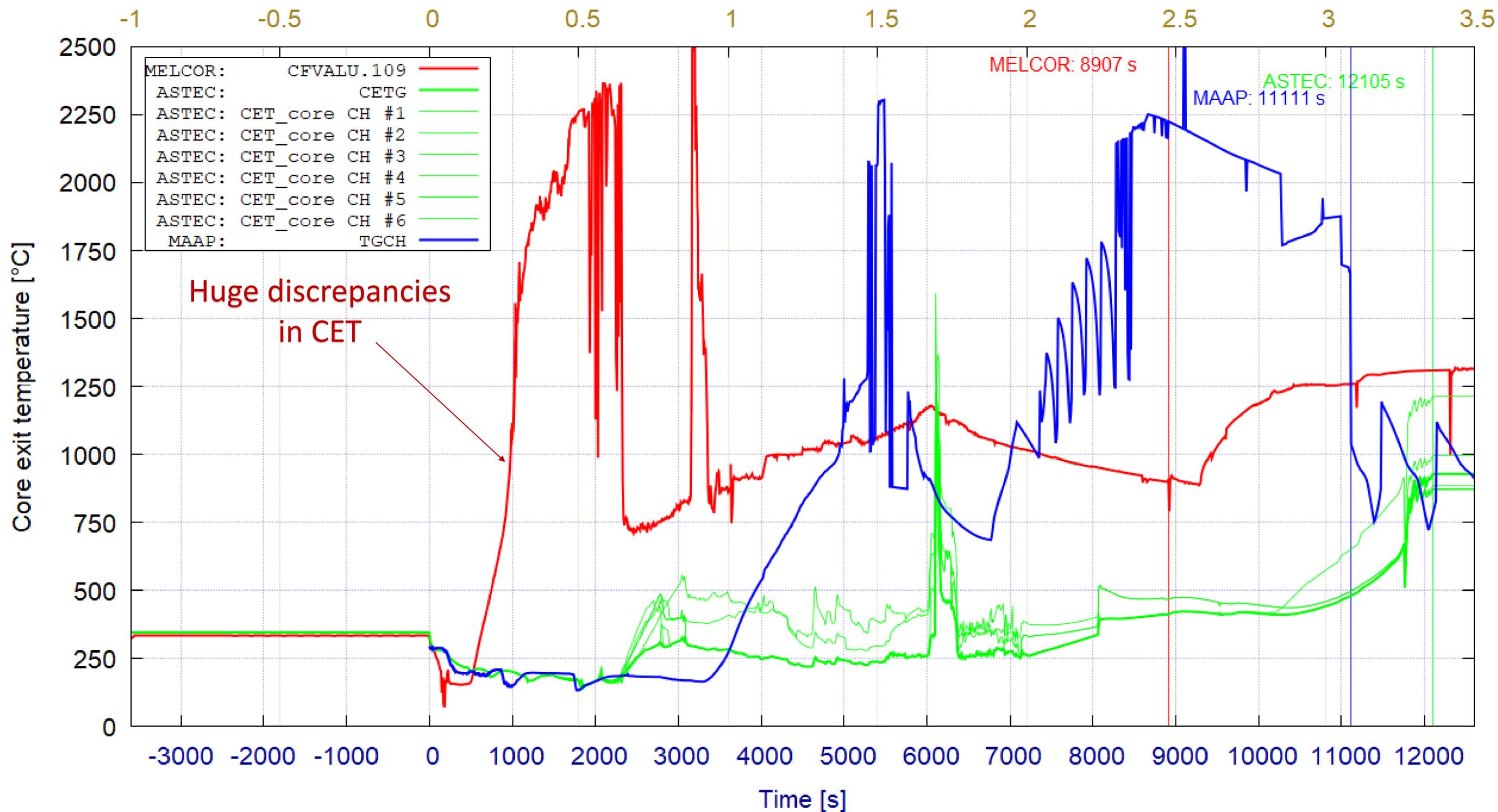
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CORE EXIT TEMPERATURE

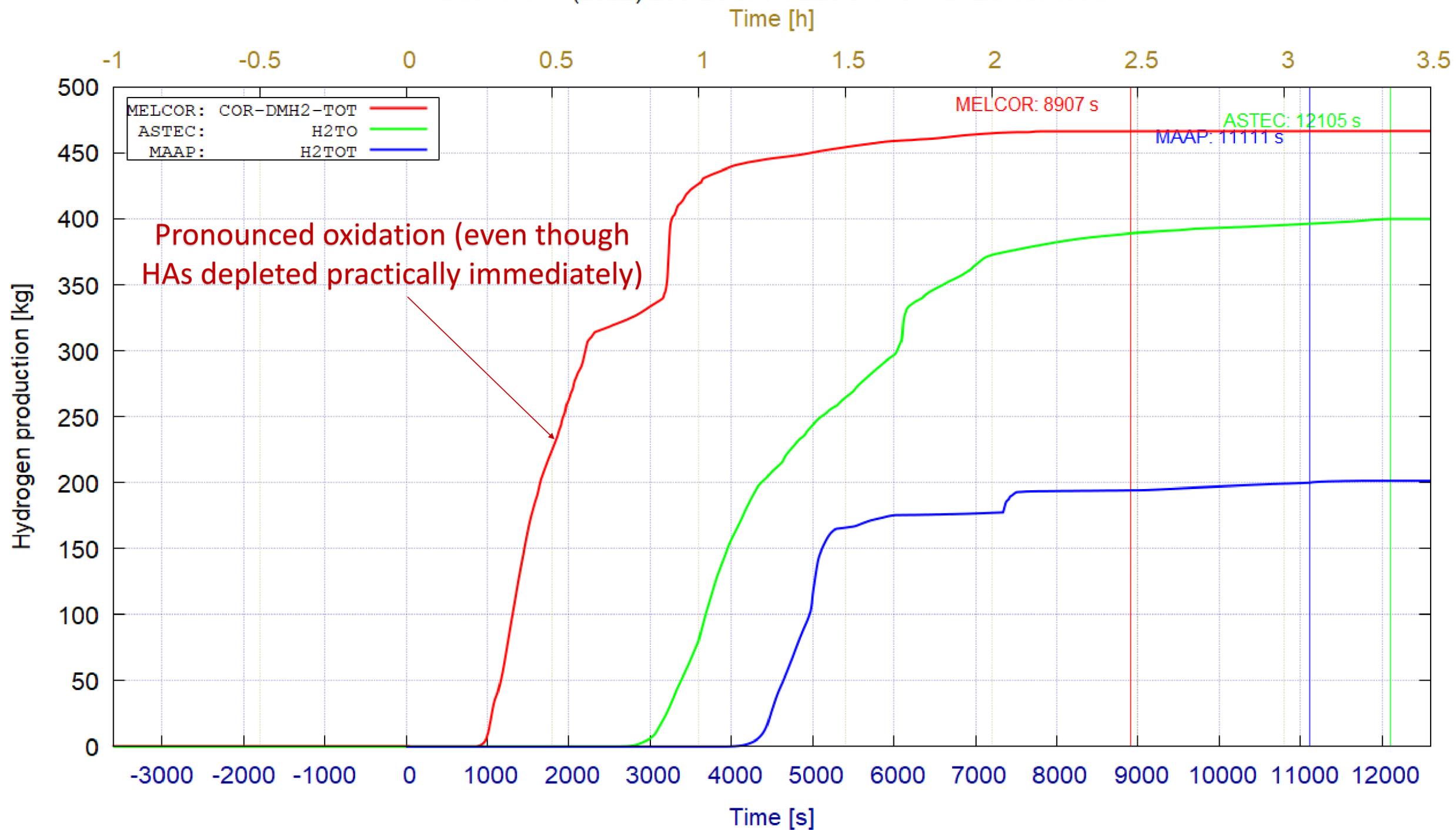
Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAAP

Time [h]



H2 PRODUCTION

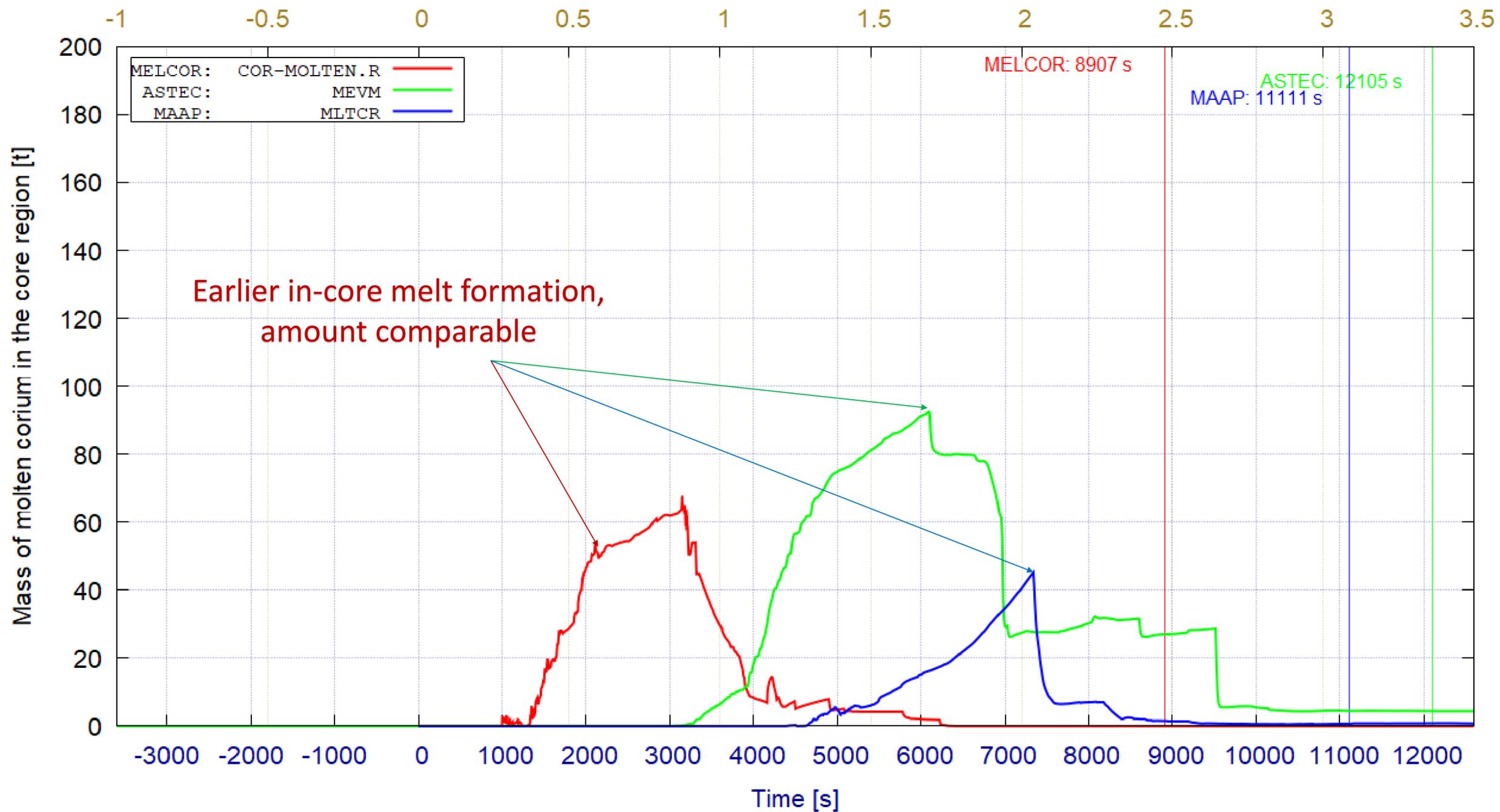
Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAAP



MOLTEN MASS IN THE CORE

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAP

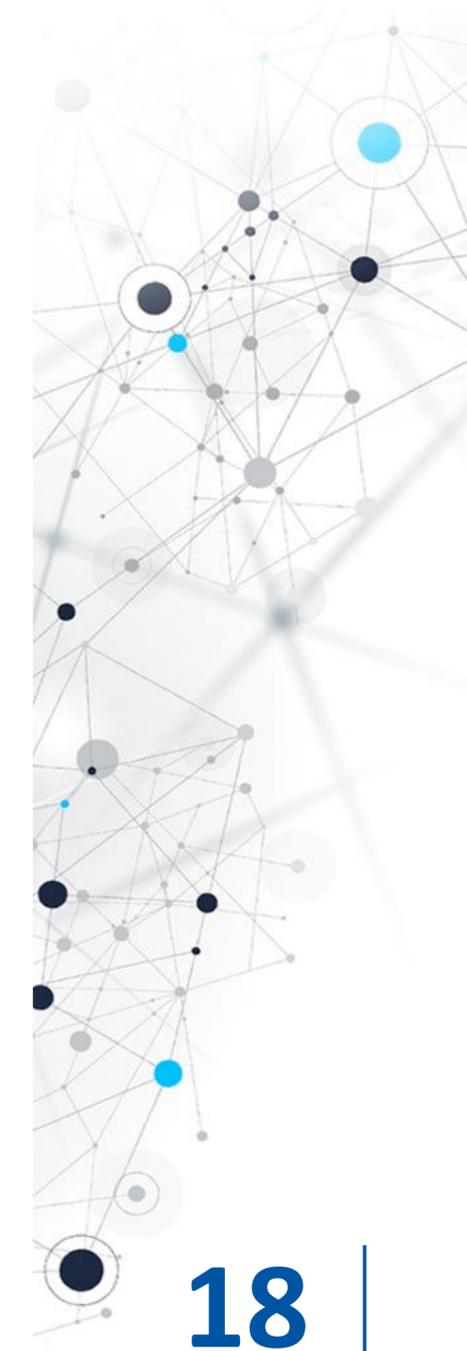
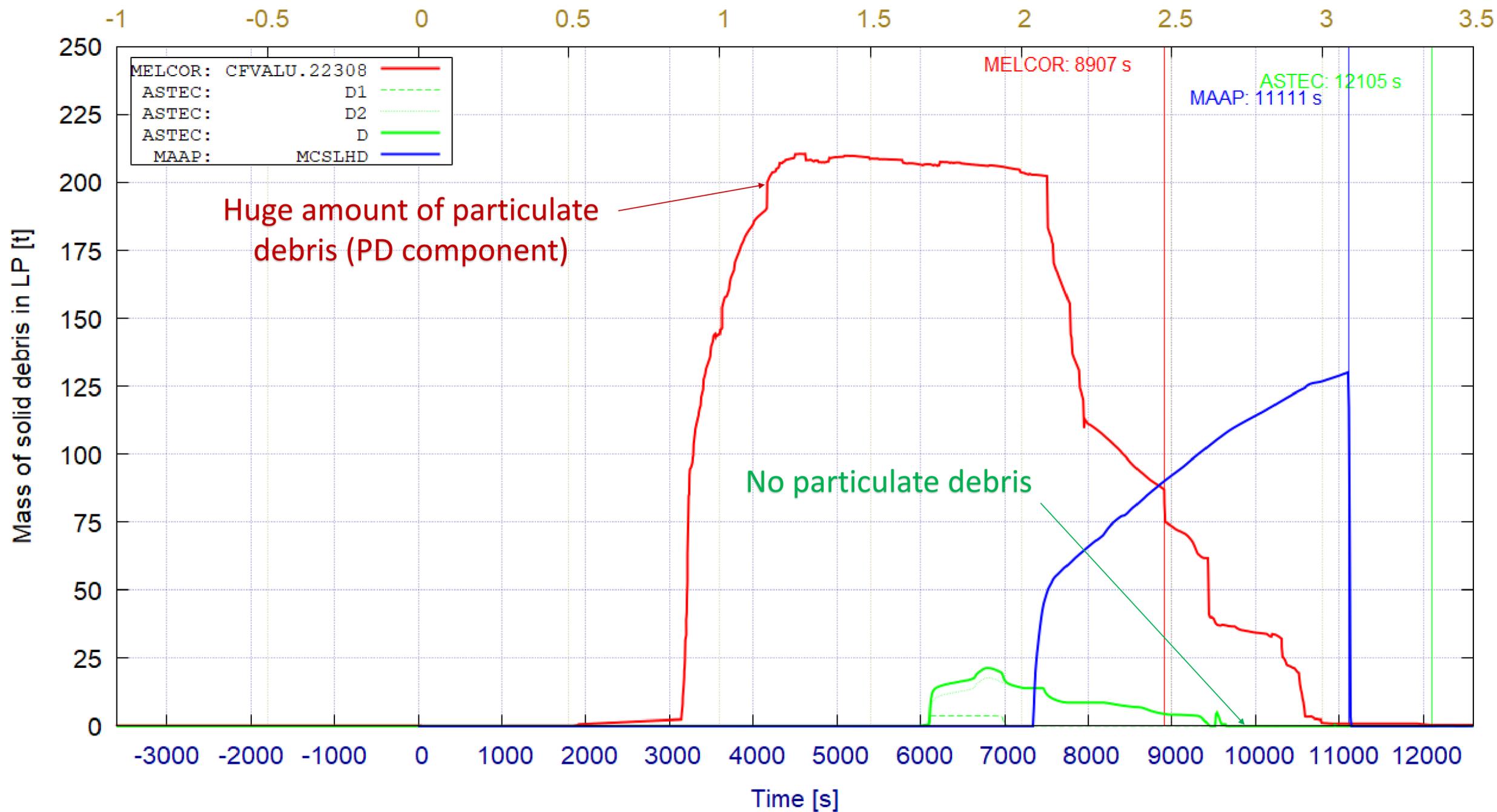
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SOLID DEBRIS IN LP

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAP

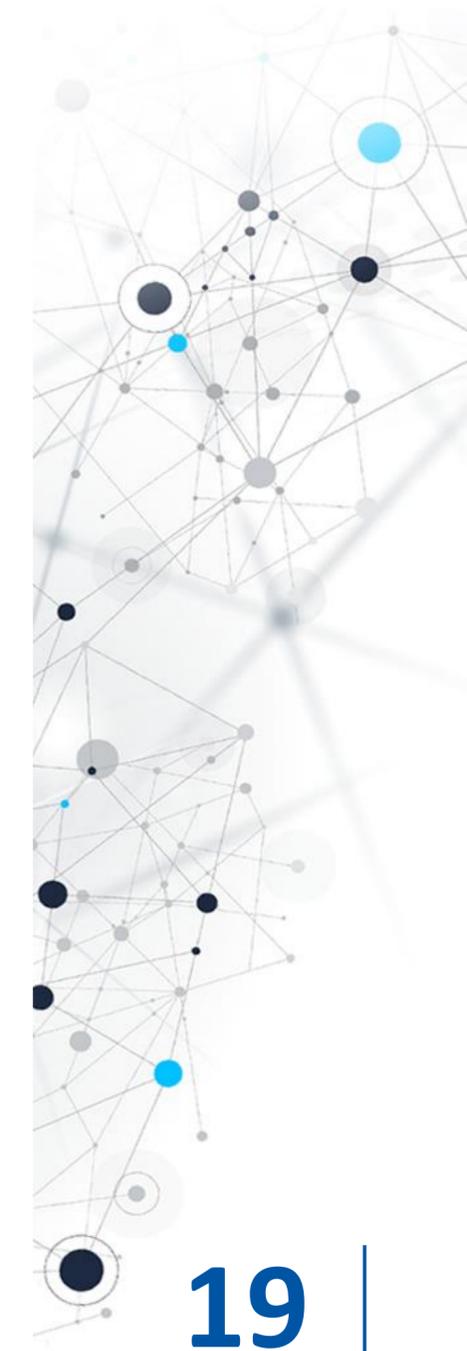
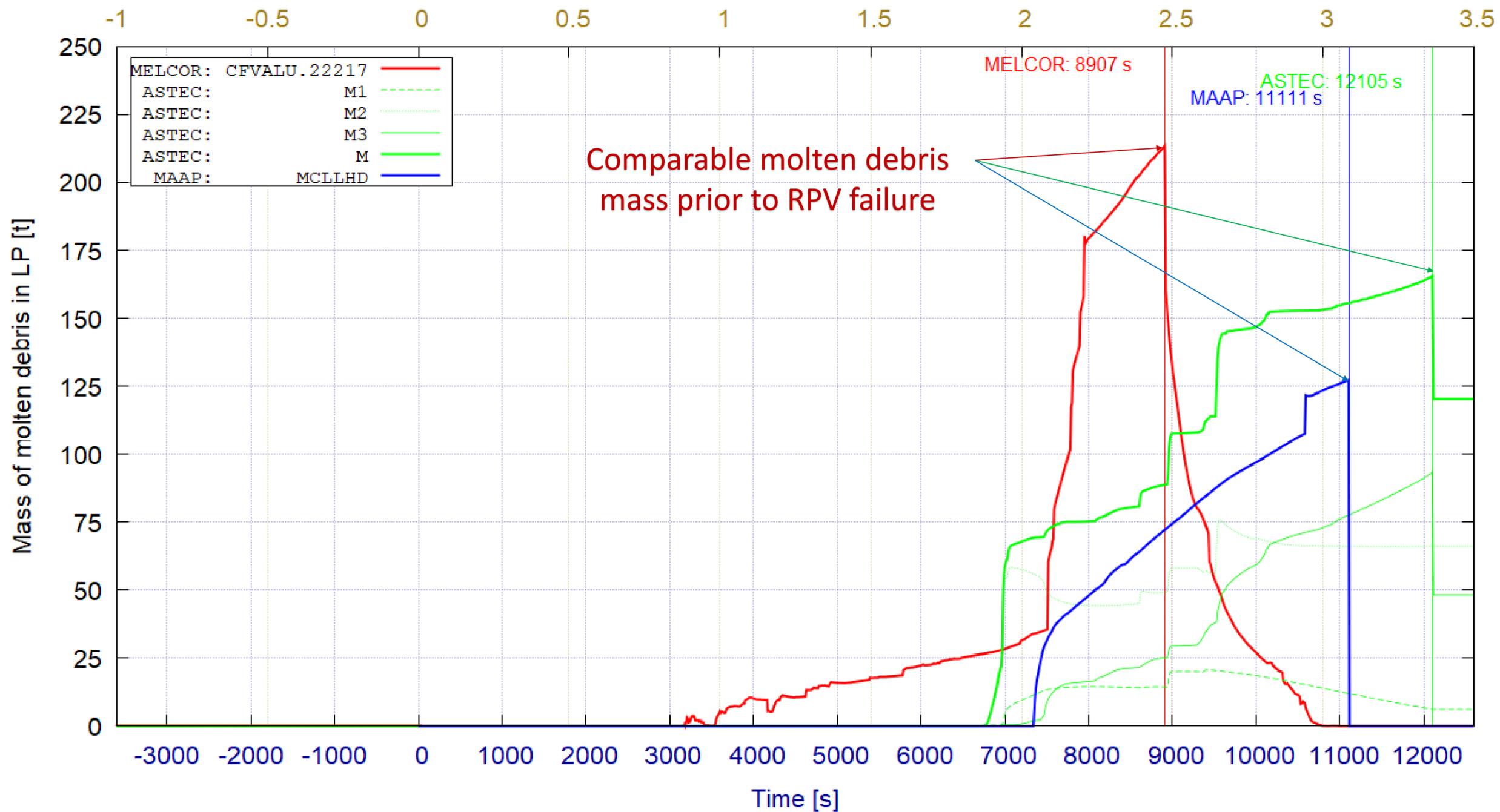
Time [h]



MOLTEN DEBRIS IN LP

Temelin NPP (2022) 200-LOCA: MELCOR vs. ASTEC vs. MAAP

Time [h]



STATE OF CORIUM AT TIME OF LH FAILURE

- „Liquidity“ of corium influences its spread-ability after RPV failure

Code	$t_{RPV-fail}$ [h]	Solid debris [t]	"Molten" pool [t]	Total corium [t]	Solid/"Molten" fraction [%]
MELCOR	2.47	88	213	301	29.2
ASTEC	3.36	0	164	164	0.0
MAAP	3.09	128	127	255	50.2

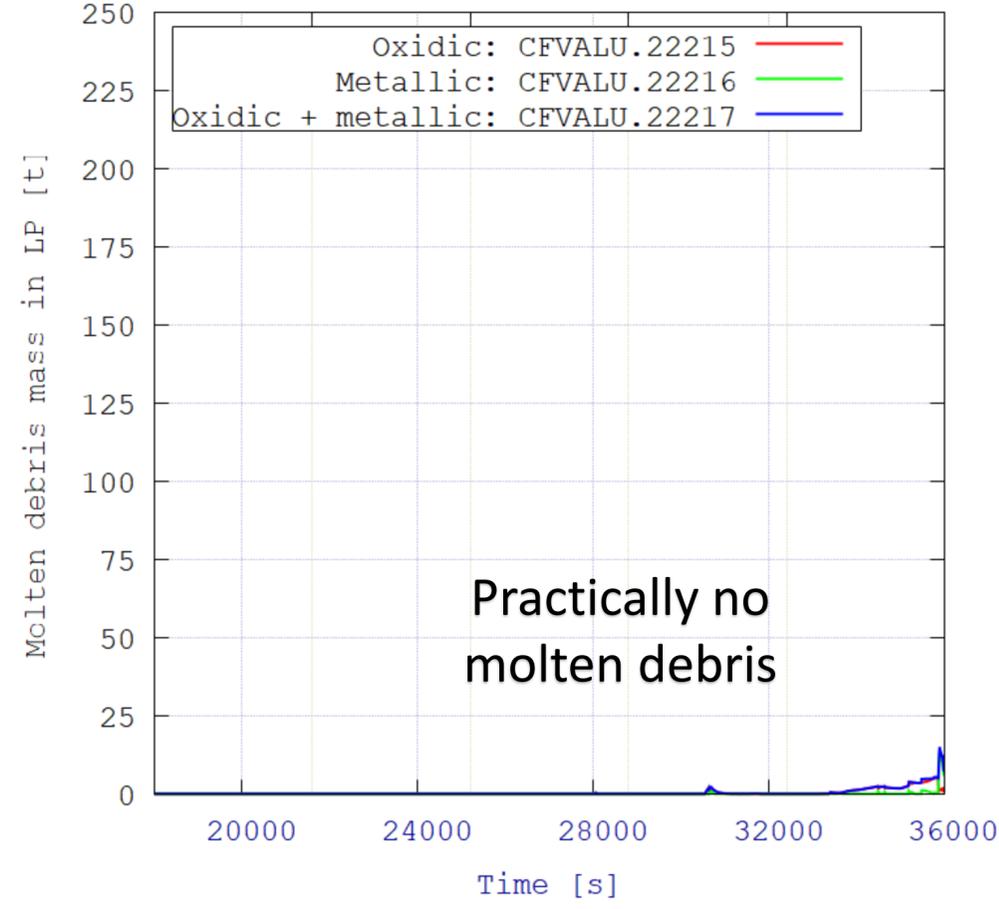
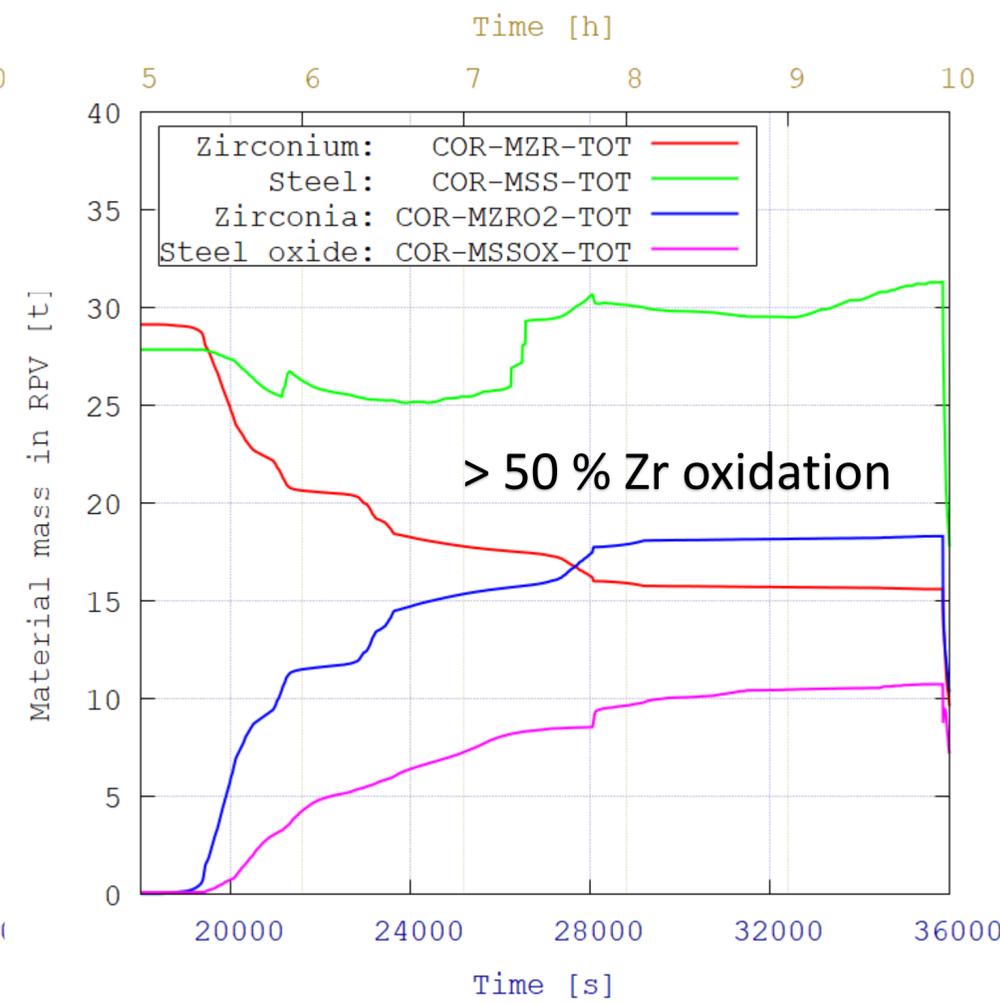
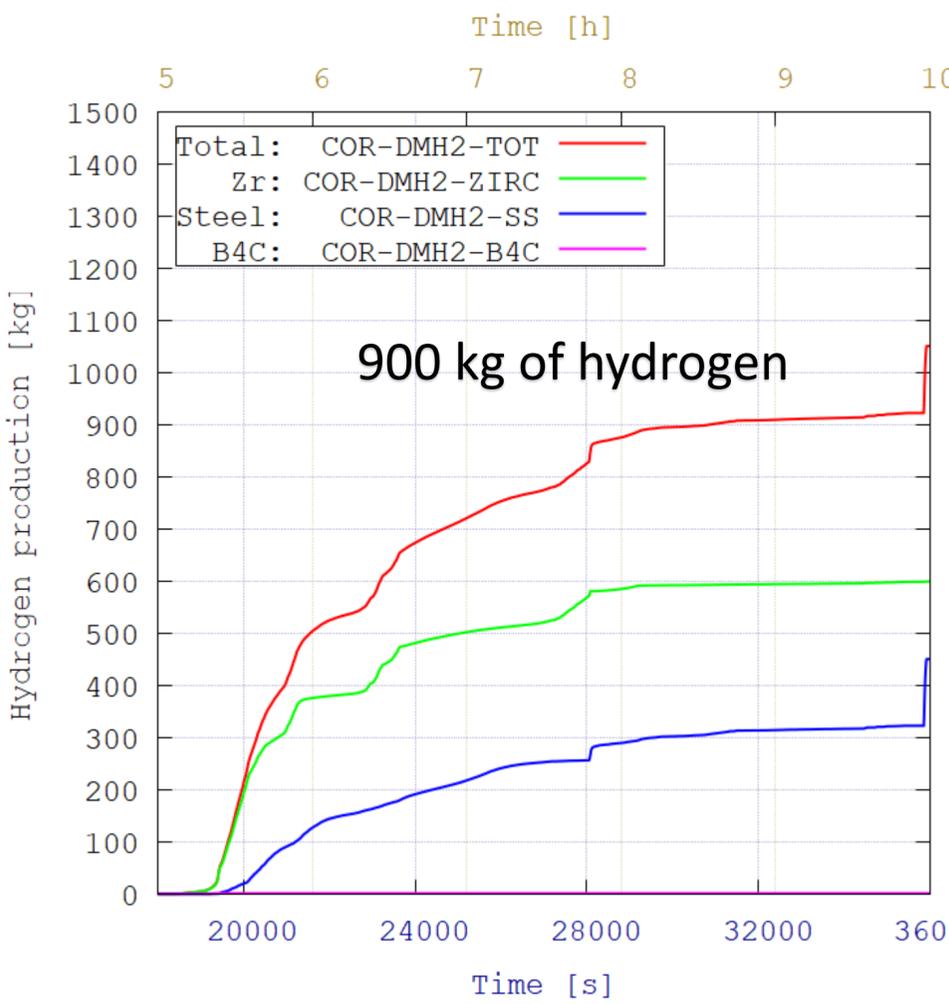
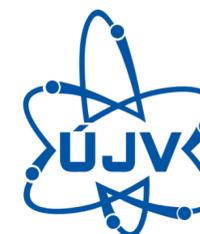
MELCOR: shortest time to failure, largest amount of molten corium & overall debris

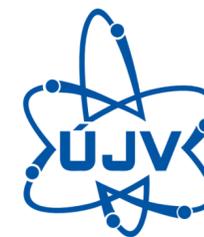
ASTEC: longest time to failure, no solid debris

MAAP: rather long time to failure & large amount of debris, 0.5/0.5 of solid/molten debris

RECENT UPDATE: SBO SCENARIO

- The same input model
- Evaluated until RPV failure (~10 h)





Encountered MELCOR issues (21402)

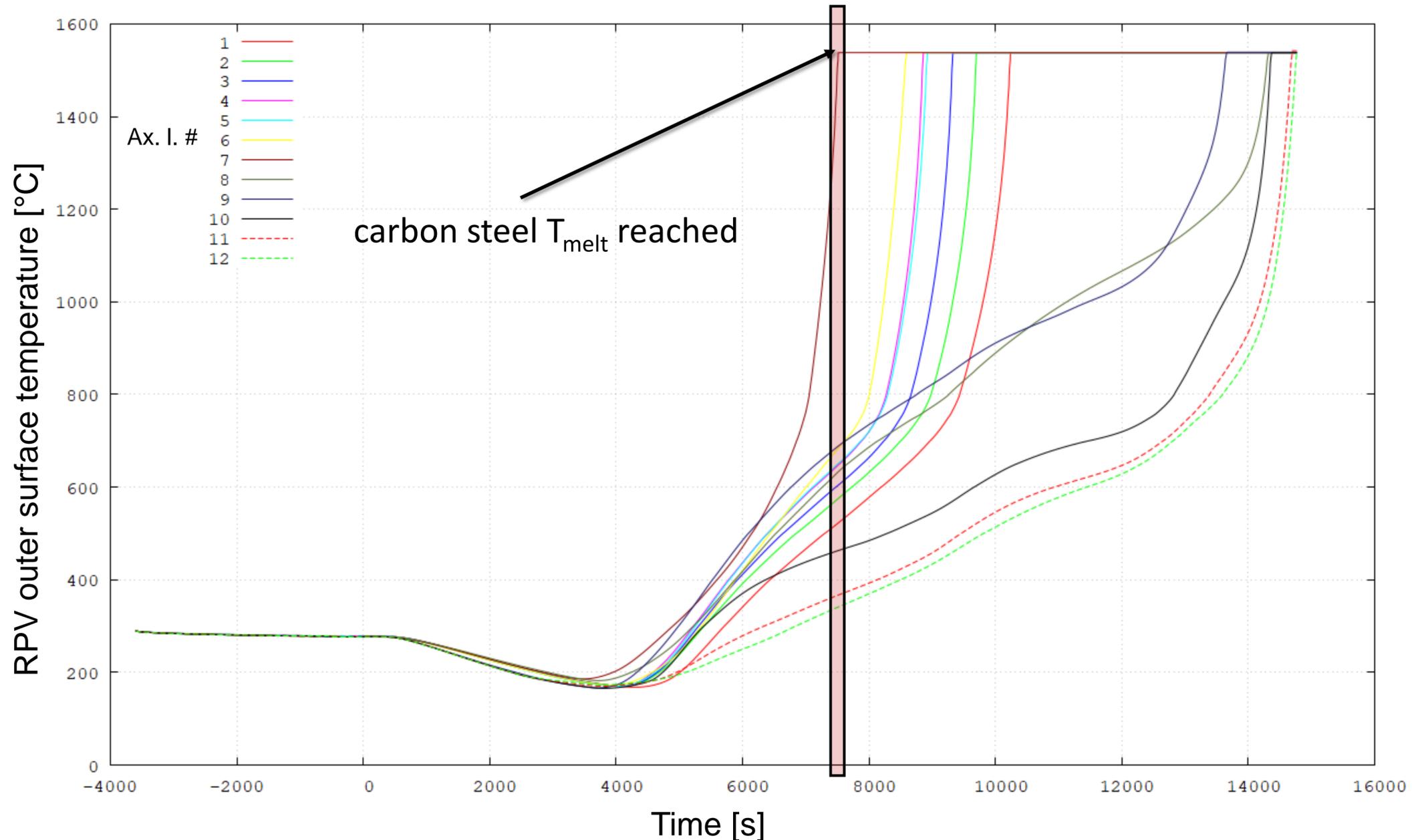
ABSENCE OF LH FAILURE

- Complete RPV wall melt-through, but no LHF or corium ejection!!!

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...
*** LH MELTING HAS STARTED AT MESH 17 OF SEGMENT 3
/SMESSAGE/ TIME= 7.53137E+03 CYCLE= 1001784
*** LH MELTING COMPLETE AT MESH 1 OF SEGMENT 7
/SMESSAGE/ TIME= 7.57136E+03 CYCLE= 1005783
*** LH MELTING HAS STARTED AT MESH 15 OF SEGMENT 5
/SMESSAGE/ TIME= 7.57160E+03 CYCLE= 1005807
*** LH MELTING HAS STARTED AT MESH 21 OF SEGMENT 1
...

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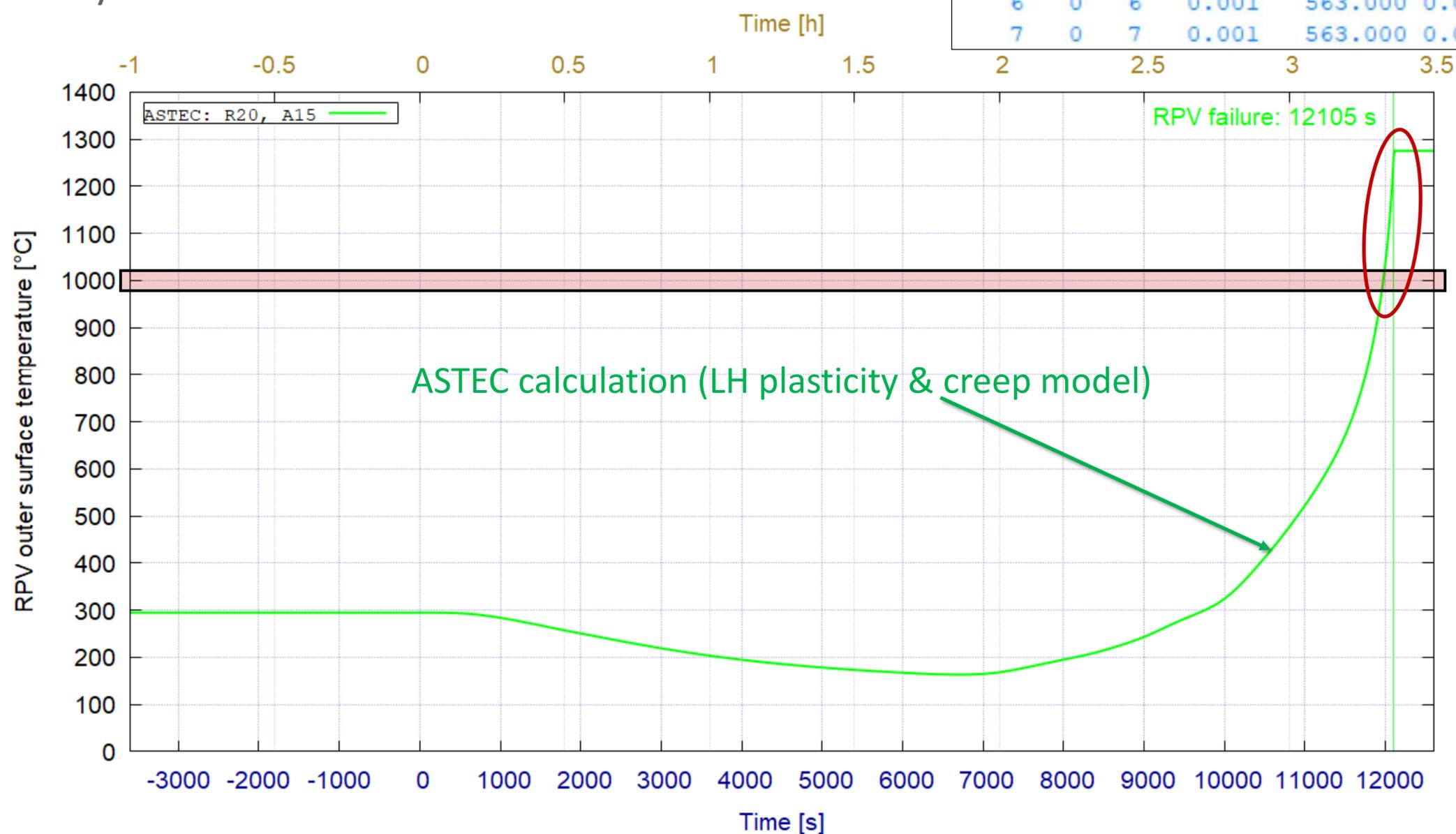


„Tiny“ penetrations defined

ALTERNATIVE LH FAILURE CRITERION

- Virtual „penetrations“ defined
- Failure: $T=1000\text{ °C}$ at outer RPV surface
- „Verified“ by ASTEC simulation

COR_PEN 7									
!	NP	IPNREF	IRP	XMPN	TPN	ASPN	AXPN	DFLPN	ICFLHF
1	0	1	0.001	563.000	0.001	0.001	0.5	'CF_3012'	
2	0	2	0.001	563.000	0.001	0.001	0.5	'CF_3022'	
3	0	3	0.001	563.000	0.001	0.001	0.5	'CF_3032'	
4	0	4	0.001	563.000	0.001	0.001	0.5	'CF_3042'	
5	0	5	0.001	563.000	0.001	0.001	0.5	'CF_3052'	
6	0	6	0.001	563.000	0.001	0.001	0.5	'CF_3062'	
7	0	7	0.001	563.000	0.001	0.001	0.5	'CF_3072'	



SPR PACKAGE 2.2.21402

CONTAINMENT SPRAY SOURCES									
SRC	C.V.	CONTROL C.F.	TEMP C.F.	DROPLET TEMP (K)	FLOW C.F.	FL-RATE (M**3/S)	HS RAIN T.P.	NO. DROP SIZES	STAT
SPR_1	CVH_899	CF_604	CF_699	3.145E+02	CF_607	1.7444E-01	---	1	ON
SPR_2	CVH_899	CF_200604	CF_200699	3.196E+02	CF_200607	0.0000E+00	---	1	OFF

Though spray number 1 is ON and has non zero flow rate, there are zero mass transfer data.

DROPLET DISTRIBUTIONS FOR SOURCE SPR_1				
GROUP NO.	DIAMETER M	REL. FREQ.	FLOW RATE DROPS/SEC	DROPLET MASS KG
1	8.0000E-04	1.0000E+00	6.5070E+08	2.6594E-07

SPRAY JUNCTION DATA FOR SOURCE SPR_1			
JUNCTION NO.	FROM VOLUME	TO VOLUME	TRANSMISSION FACTOR
1	CVH_899	CVH_881	1.00000E+00
2	CVH_881	CVH_861	1.00000E+00
3	CVH_861	CVH_852	5.00000E-02
4	CVH_861	CVH_833	1.50000E-01
5	CVH_861	CVH_832	2.00000E-02
6	CVH_861	CVH_831	2.00000E-02

This anomaly occurs only if spray system is using a junction data SPR_JUN

SPRAY HEAT AND MASS TRANSFER DATA		
CONTROL VOL	HEAT TRAN RATE W	MASS TRAN RATE KG/S
CVH_810	0.00000E+00	0.00000E+00
CVH_824	0.00000E+00	0.00000E+00
CVH_831	0.00000E+00	0.00000E+00
CVH_832	0.00000E+00	0.00000E+00
CVH_833	0.00000E+00	0.00000E+00
CVH_852	0.00000E+00	0.00000E+00
CVH_861	0.00000E+00	0.00000E+00
CVH_881	0.00000E+00	0.00000E+00
CVH_899	0.00000E+00	0.00000E+00



OBSERVATIONS

- Rather pronounced core oxidation
 - Due to:
 - Larger surface of Zr SGs (for new FAs)
 - Earlier supporting structure components slumping?...
 - Water accessibility into in the gap between *barrel LH* \Leftrightarrow *RPV wall*?...
- Large amount of solid debris prior to RPV failure observed
 - Due to higher T_{melt} of oxides (in agreement with large H_2 production)
 - Completely different to ASTEC results (which predicts no solid debris)
- Some bugs/issues encountered
 - r2023 to be tested!

Thank you for the attention!



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