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# Analysis of simultaneous SBO and LBLOCA considering DEC equipment

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# Outline

- Introduction
- Analyzed SA scenarios
- Krško NPP MELCOR model
- Simulation results
- Conclusions



# Krško NPP

2-loop Westinghouse PWR with 1,994 MW<sub>th</sub> and 696 MW<sub>el</sub>





# Analyzed SA scenarios

Initiating external event: Strong earthquake resulting in simultaneous SBO and LBLOCA

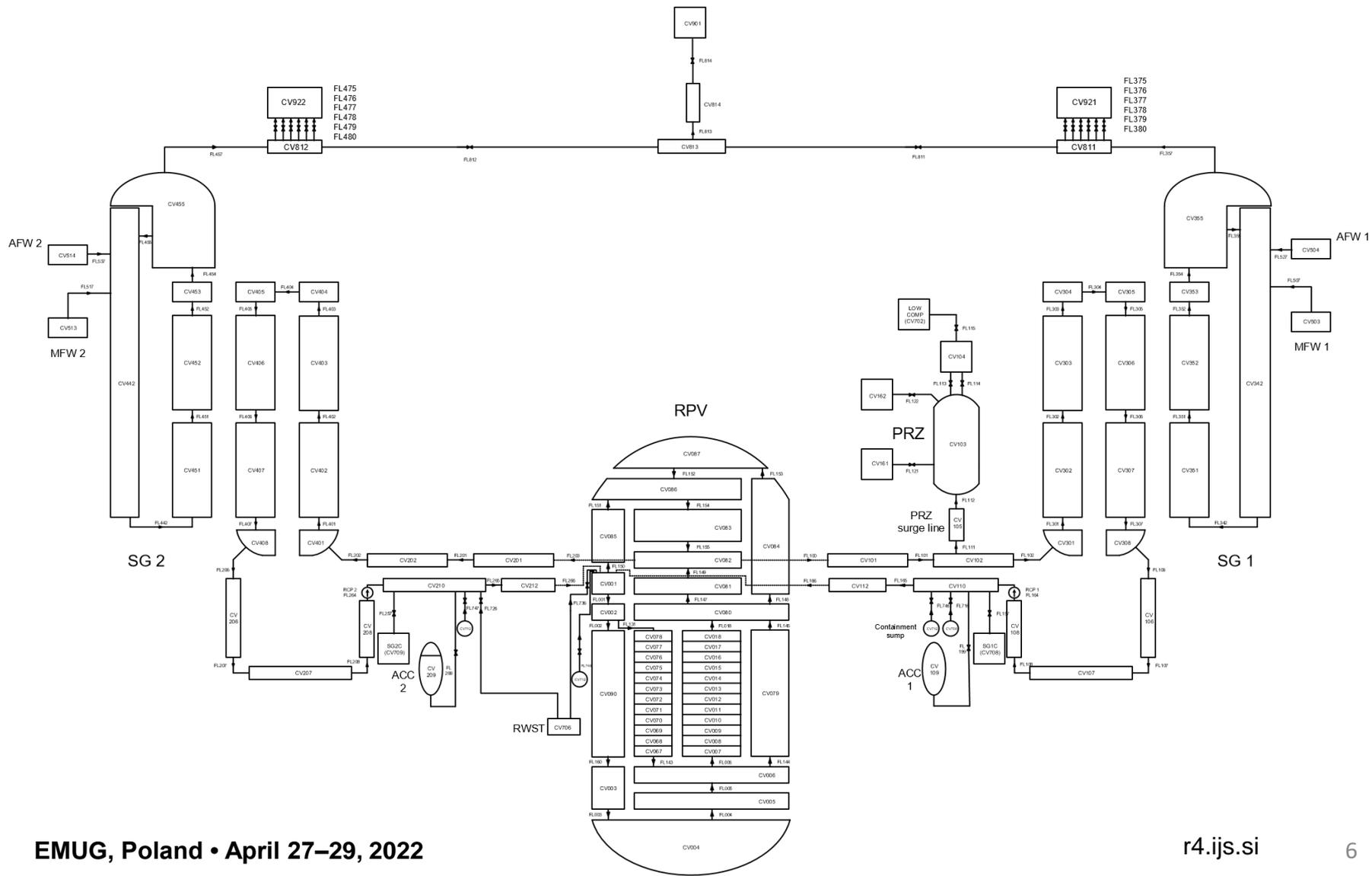
Analyzed five scenarios:

1. No mitigation (noASS)
2. After melt release from RV water injection through cont. sprays (ACI\_RV)
3. After melt release from RV water injection simultaneously through cont. sprays and into RCS RV (ACVI\_RV)
4. After melt release from RV water injection into RCS RV (AVI\_RV)
5. After melt release from RV water injection into RCS RV, without ARHR HEX, with AAF (AVI\_RV\_noHEX\_AAF)

Simulations performed with MELCOR 2.2 revision 15254

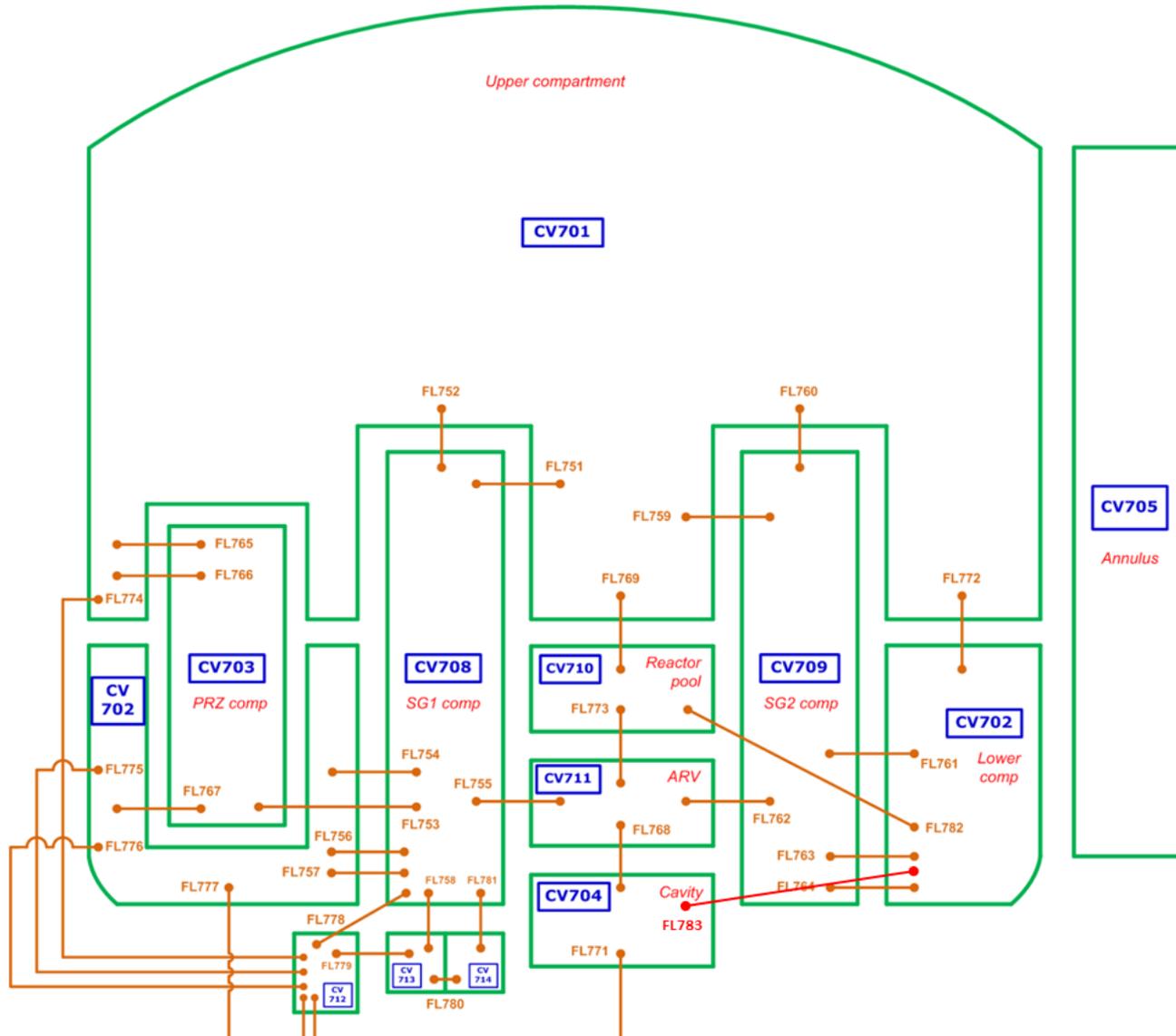


# Krško NPP primary and secondary systems nodalization



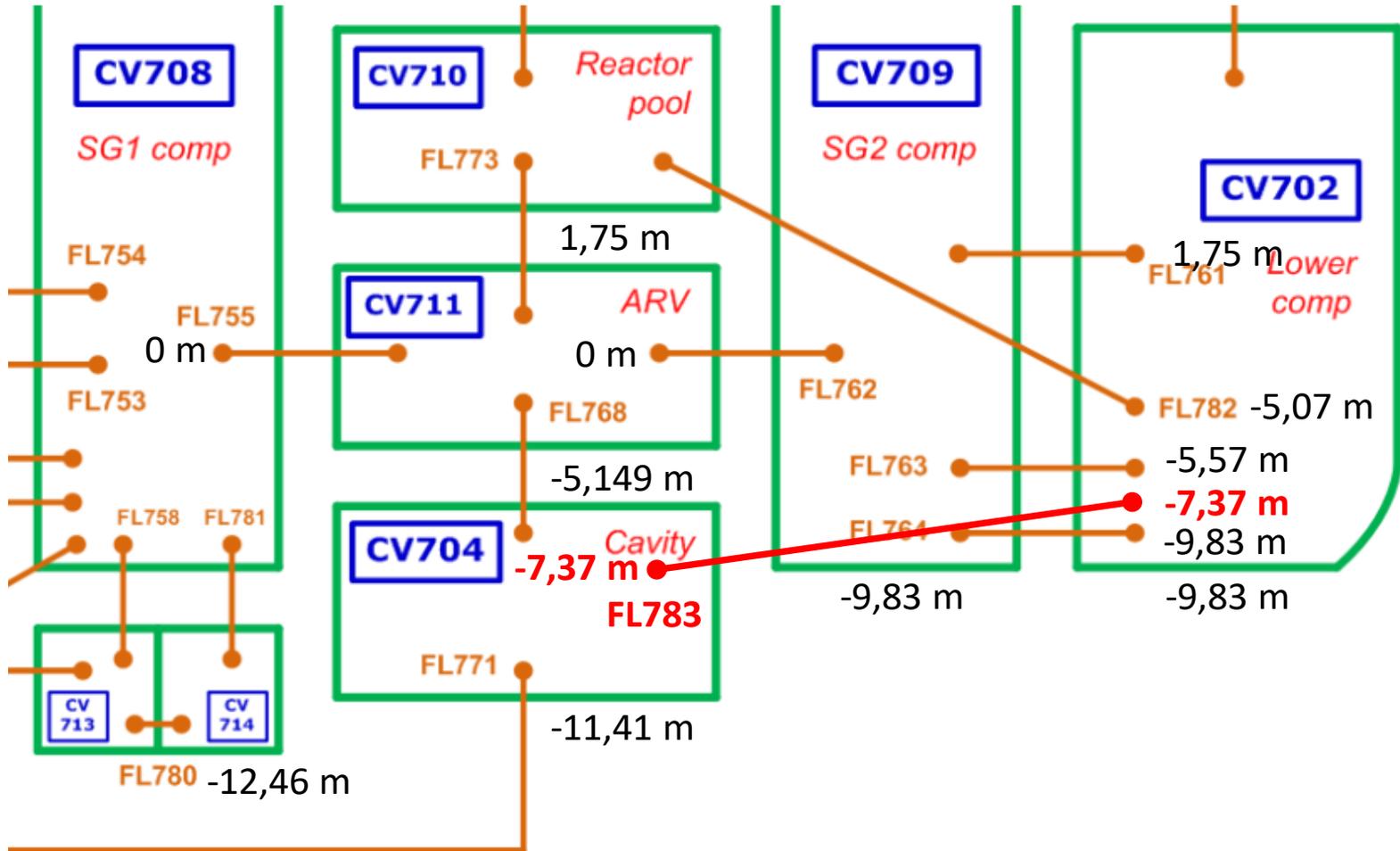


# Krško NPP containment nodalization





# Nodalization around reactor cavity





# Simulation results

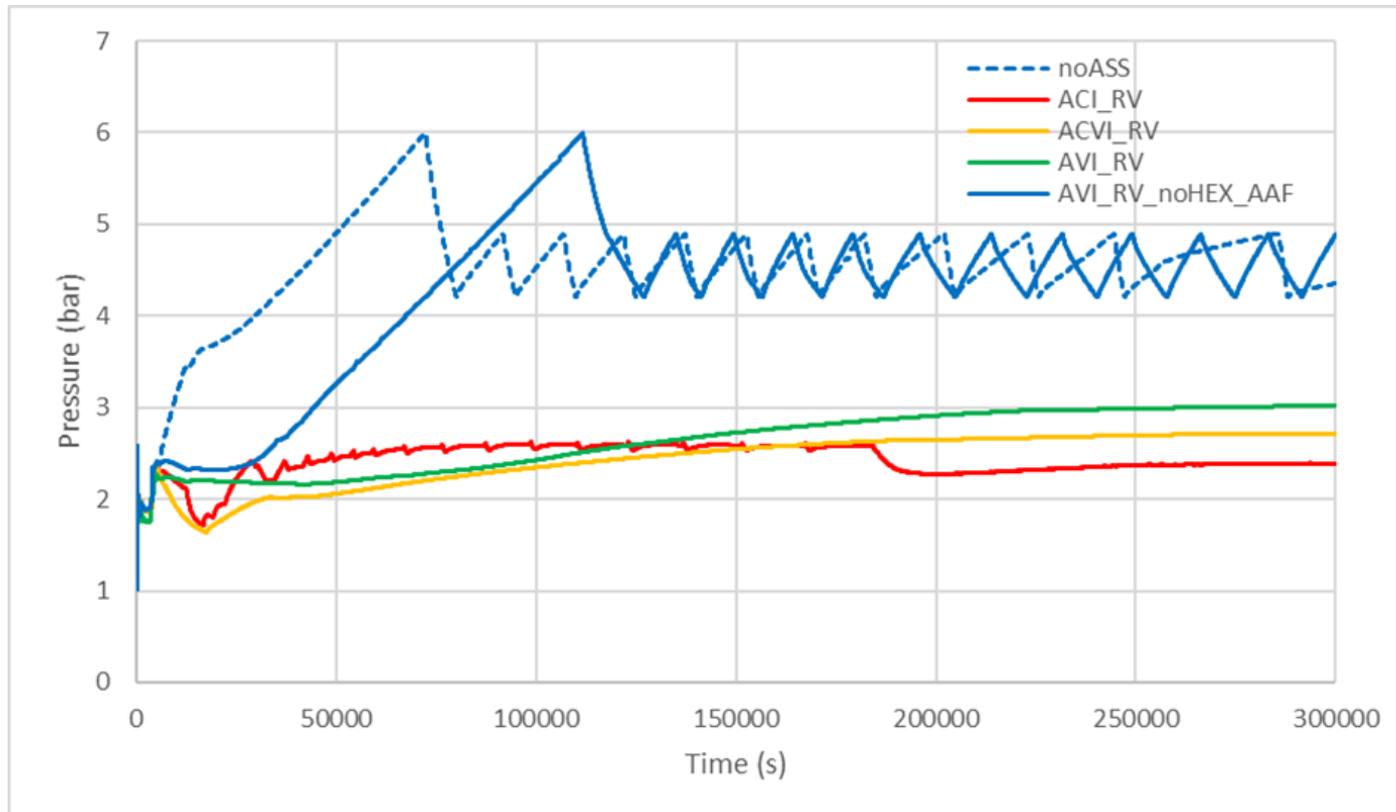
## Chronology of main events

Event \ Scenario	Time (s)				
	noASS	ACI_RV	ACVI_RV	AVI_RV	AVI_RV_noHEX_AAF
<b>Accumulators empty</b>	83	82	82	83	81
<b>Gap release</b>	303	305	305	303	302
<b>Core melting</b>	888	927	927	888	874
<b>RV failure</b>	3467	3734	3734	3467	3614
<b>ASS activated</b>	/	5000	5000	5000	5000
<b>PCFVS open</b>	72263	/	/	/	111702
<b>PCFVS open 2<sup>nd</sup> time</b>	92700	/	/	/	135100

Differences for scenarios in period when they are still identical (first 5000 s) are due to numerical variance



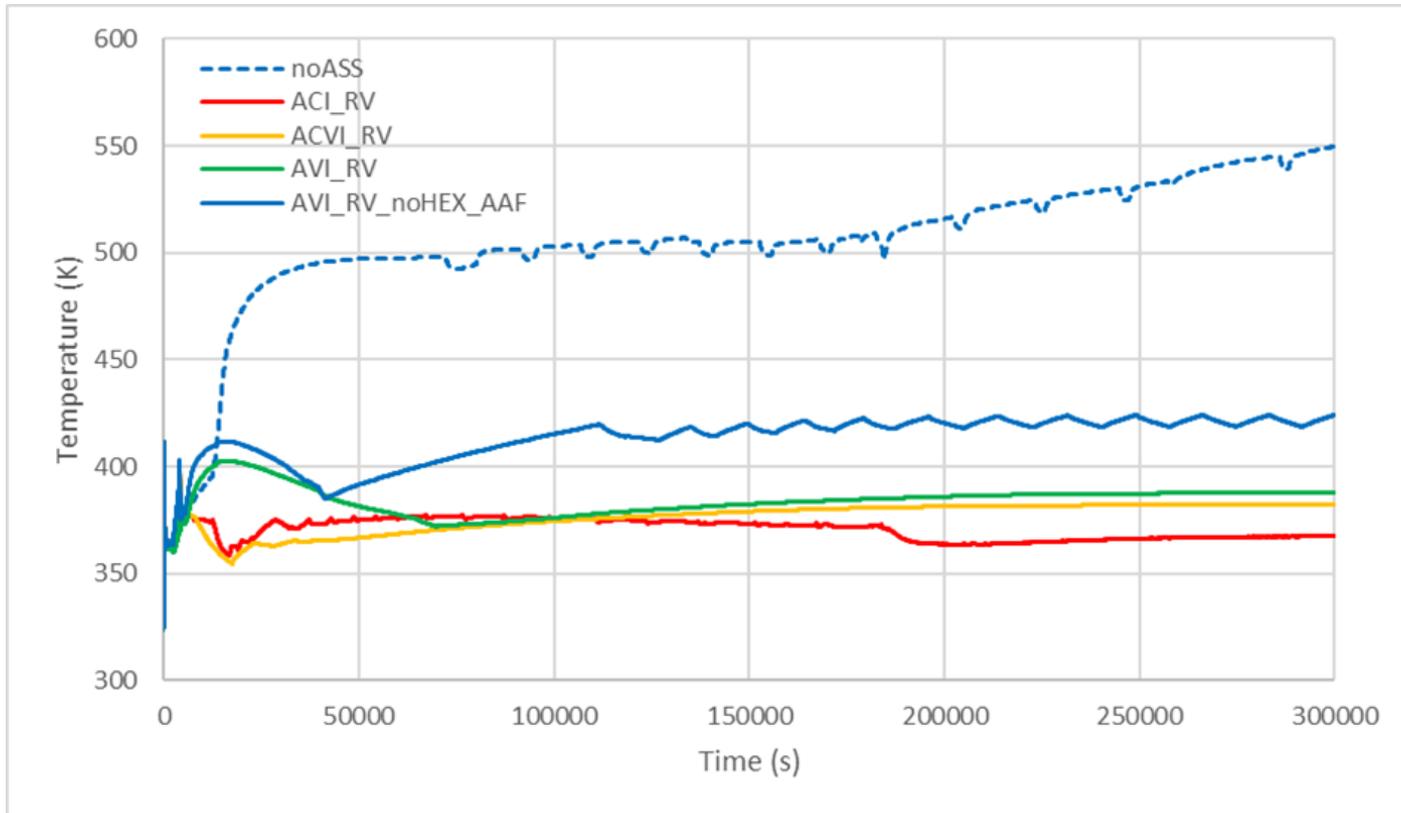
# Containment pressure



Cooling through steam generators by natural circulation of atmosphere in failed RCS is not sufficient to stabilize severe accident (AVI\_RV\_noHEX\_AAF)



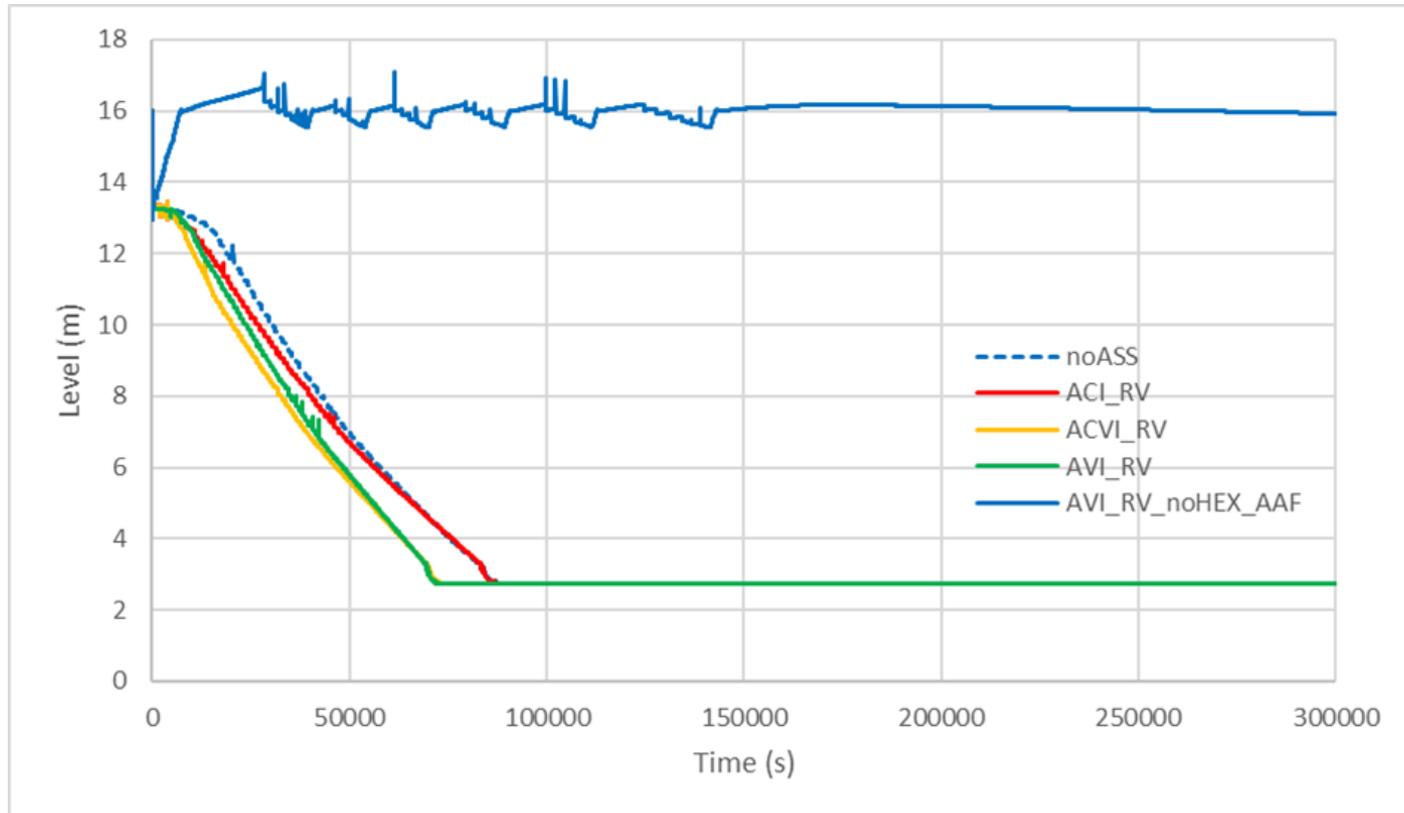
# Containment temperature



Heat transfer through containment walls not sufficient to extract the entire residual heat from the molten core (noASS)



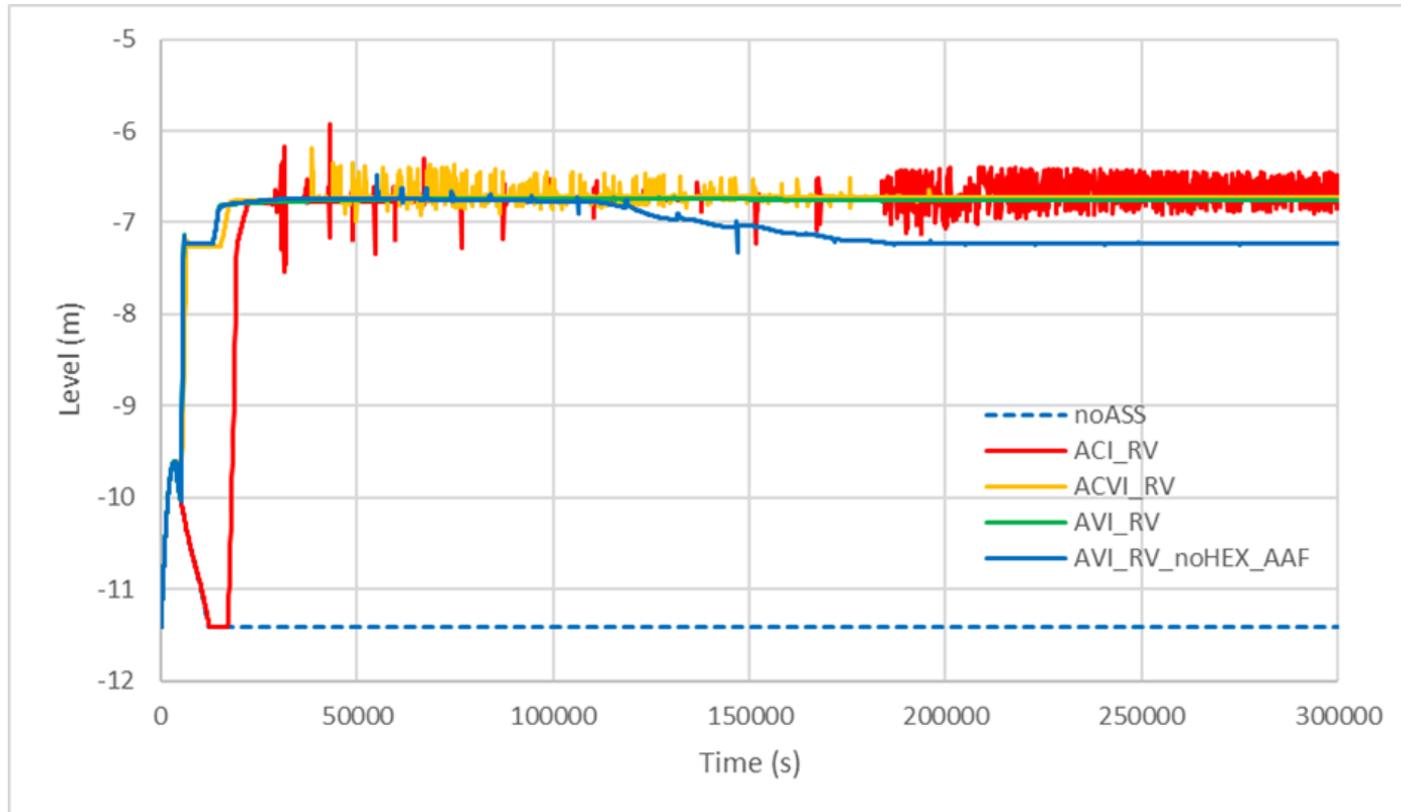
# Water level in steam generator 2



In second loop of RCS with large break natural circulation of atmosphere develops, which transfers heat from containment atmosphere to water in second steam generator



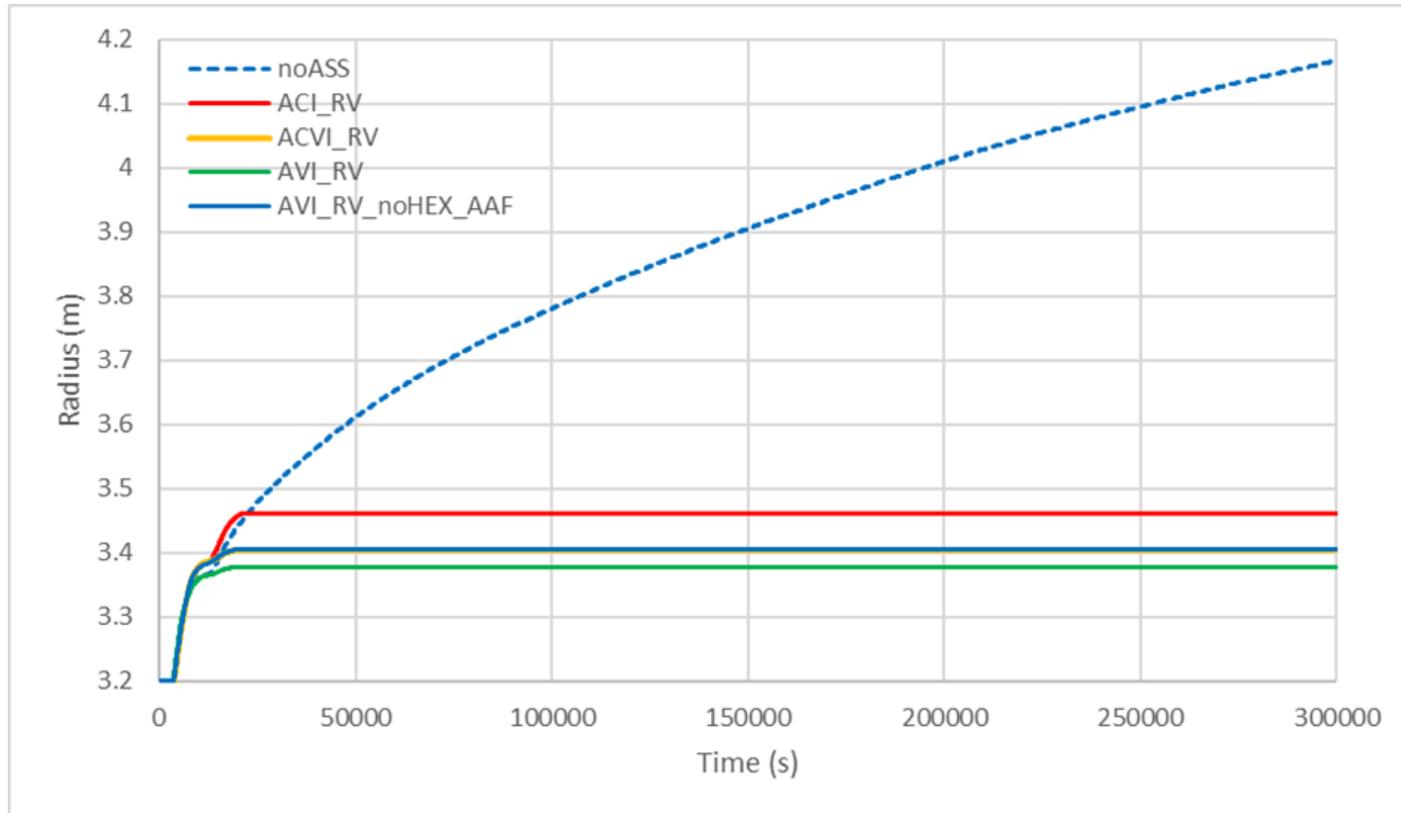
# Water level in reactor cavity



In scenario ACI\_RV reactor cavity dries out for more than one hour before it is flooded again



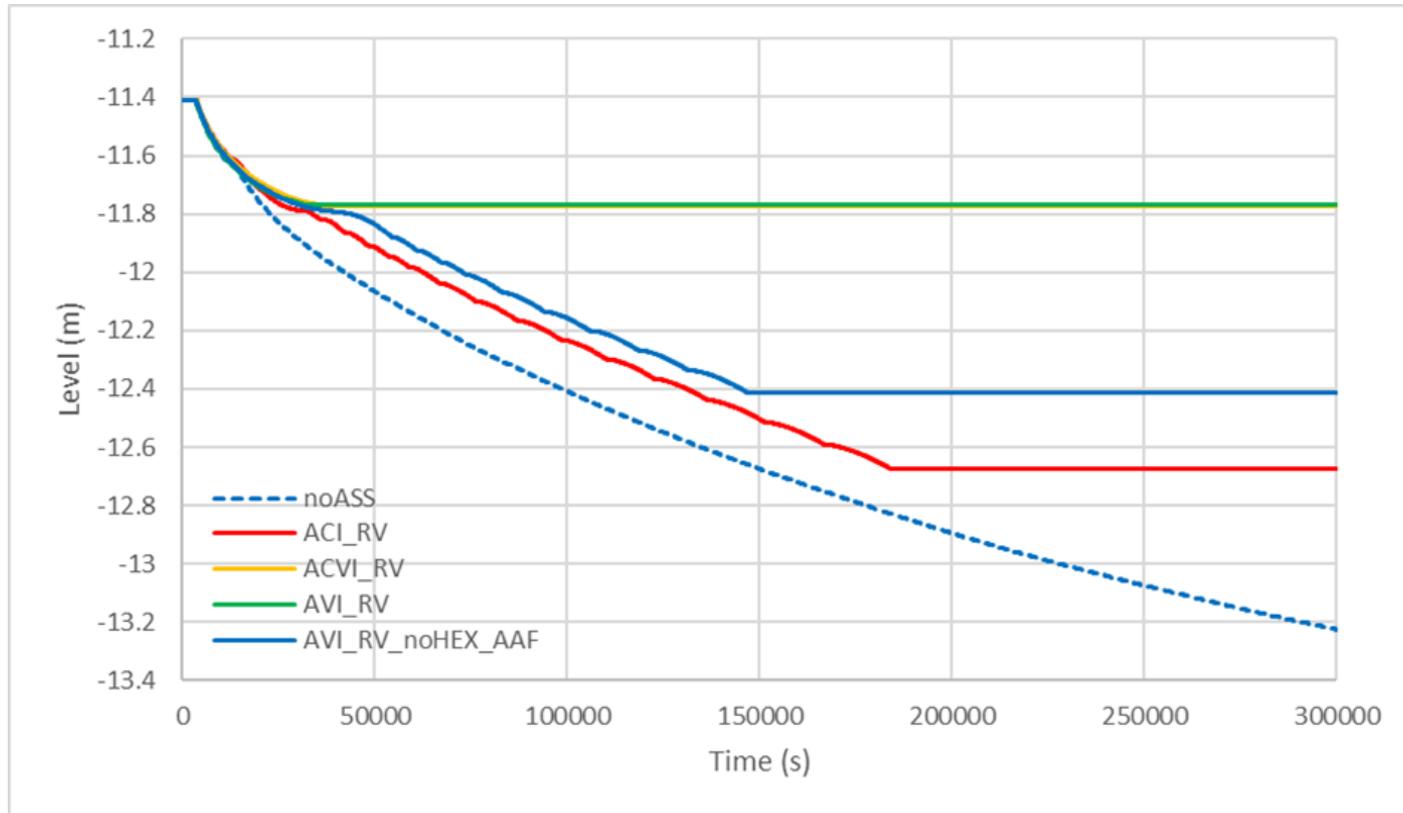
# Radius of eroded reactor cavity



In scenario ACI\_RV, where the molten core dries out for more than one hour before it is flooded again, the extend of the MCCI is significantly larger



# Bottom level of eroded cavity



Small differences in flooding conditions influence characteristics of molten core concrete mixture, which influence the MCCI. Consequently, MCCI is very sensitive on flooding conditions.



# Conclusions

- Analysis of unmitigated and mitigated SBO+LBLOCA scenarios performed with MELCOR 2.2
  - Mitigation measures for heat removal from containment solely by DEC alternative safety systems considered
  - Main focus given to MCCI
- MCCI in reactor cavity can be stopped if molten core is flooded soon after it is released from the failed reactor vessel
- Extend of MCCI sensitive on the flooding time
  - In scenarios, where water is injected into RCS RV, molten corium remains flooded all the time
  - In scenario, where water is injected solely through containment sprays, reactor cavity dries out before molten core is flooded again, resulting in much more extensive MCCI
- In loop of RCS system where large break occurs, natural circulation of atmosphere develops
  - Heat transfer by steam generator not enough to remove all residual heat from molten core and to stabilize SA
- In mitigated scenarios with operable ARHR HEX, SA could be stabilized and no releases into environment occurred
  - For mitigation of SA it is important to activate the available safety systems as soon as possible



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