

# STABILITY ASSESSMENTS

Jeremy Bittan

Electricité de France (EDF)

[jeremy.bittan@edf.fr](mailto:jeremy.bittan@edf.fr)

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# Outline

1. MAAP5/MAAP6 Numerical stability studies
2. Examples of improvements in MAAP6

# 1- MAAP5/MAAP6 Numerical stability studies

## Motivation for the studies

Feedbacks from using SA codes show that when uncertainties are propagated in a transient it is sometimes difficult to explain physically the discrepancies between the runs: small input discrepancies can lead to large discrepancies in the FoM:

- **A pioneer work based on STCP** (Khatib-Rahbar et al., 1989)

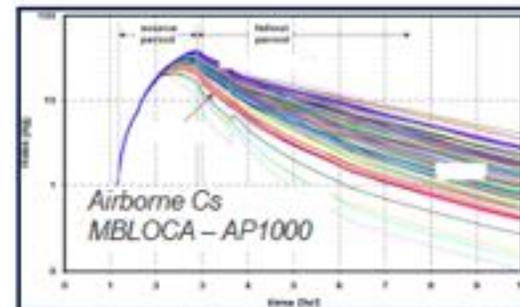
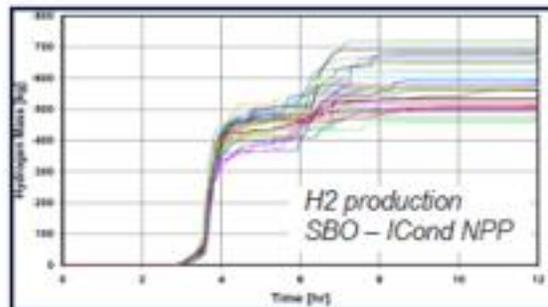
- Identification of input param.
- Determination of pdf's
- Random combination samp.
- Calculation running



**Source Term uncertainties**

- Meltdown parameters
- FP release coefficients
- Chemical activities (MCCI)
- Containment performance

- **Similar methodology based on MELCOR 1.8.5** (Gauntt R.O., 2005)



# 1- MAAP5/MAAP6 Numerical stability studies

## Motivation for the studies

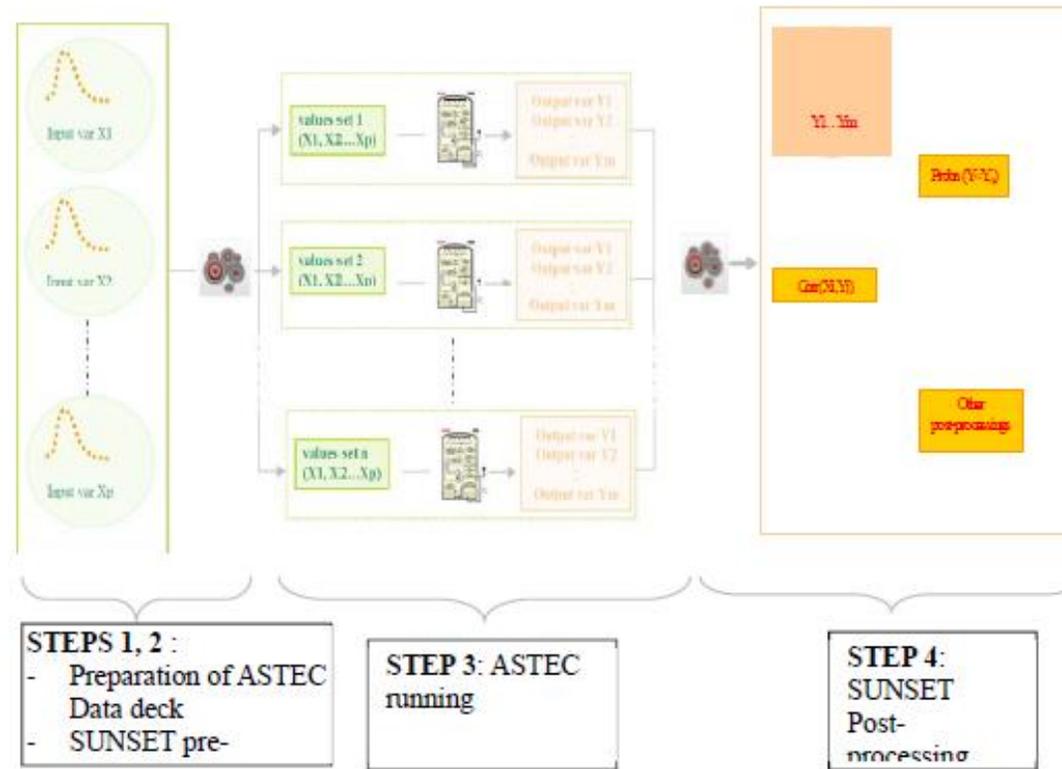


Figure 14: General sketch of uncertainty analysis using SUNSET and ASTEC

# 1- MAAP5/MAAP6 Numerical stability studies

## Motivation for the studies

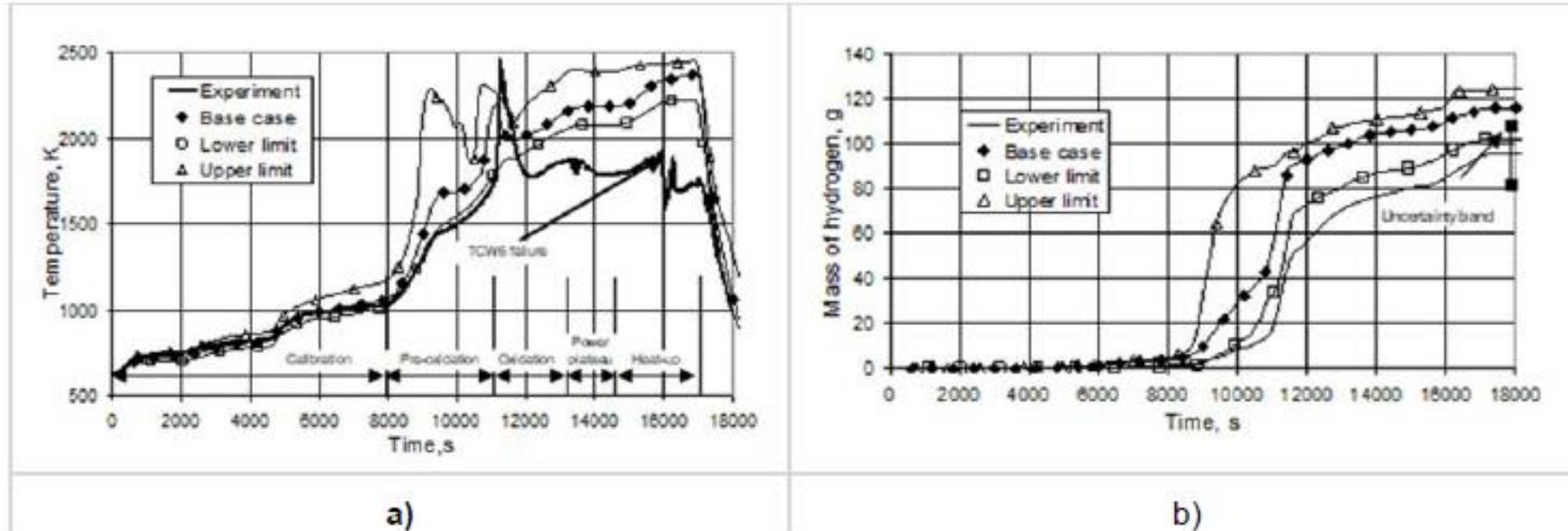


Figure 6: Results of ASTEC calculation of PHEBUS FPT1 experiment: a) fuel cladding temperature at 700 mm elevation; b) total hydrogen generation

[https://musa-h2020.eu/wp-content/uploads/2023/05/D3\\_1\\_review\\_of\\_uncertainty\\_methodologies\\_and\\_tools\\_applicable\\_to\\_SA\\_codes\\_for\\_the\\_prediction\\_of\\_ST\\_V1.pdf](https://musa-h2020.eu/wp-content/uploads/2023/05/D3_1_review_of_uncertainty_methodologies_and_tools_applicable_to_SA_codes_for_the_prediction_of_ST_V1.pdf)

# 1- MAAP5/MAAP6 Numerical stability studies

## Motivation for the studies

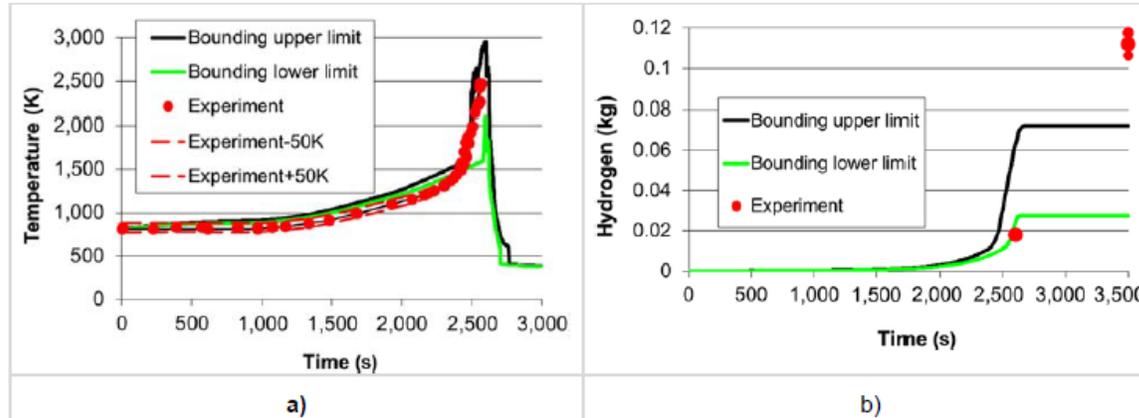


Figure 21: Results of ASTEC calculation of QUENCH-03 experiment: a) cladding temperatures of the fuel rod imitator from the outer ring at 750 mm height; b) amount of generated hydrogen

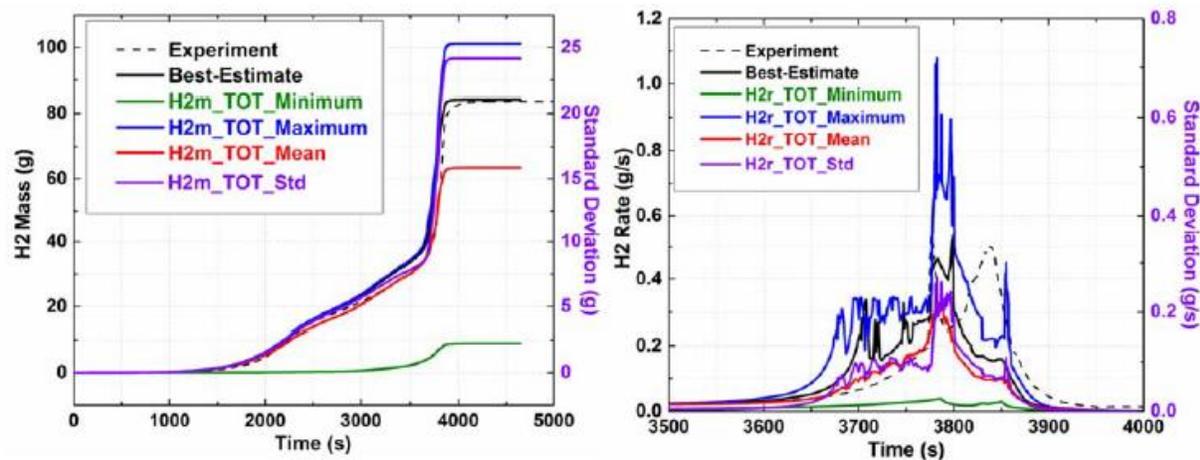


Figure 35: ASTEC/URANIE results: H2 mass and production rate [24]

# 1- MAAP5/MAAP6 Numerical stability studies

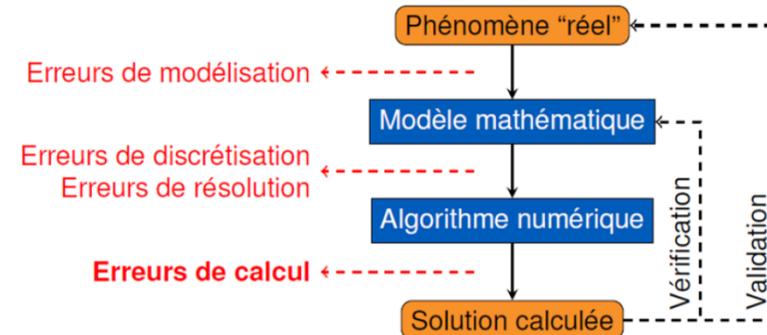
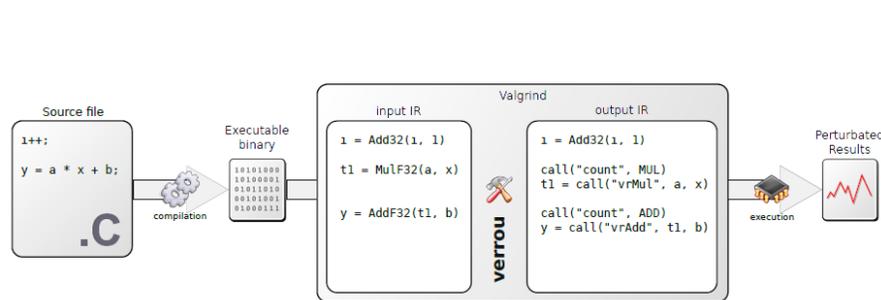
## Introducing VERROU

The physics of the SA are of course nonlinear and could explain some parts of the discrepancies.

EDF has developed a tool – called VERROU – that evaluates the round-off error of a code (SA code or not).

No need to have access to the source code, only an executable is necessary

```
$ valgrind --tool=verrou --rounding-mode=random PROGRAM [ARGS...]
```



# 1- MAAP5/MAAP6 Numerical stability studies

## Introducing VERROU

VERROU modifies each floating-point operation to add a different rounding of the results (random by default).

Original code with two arithmetic operations $MWEXP = MWR + FMWR * DTR$	Result $MWEXP = 593.$
Modified code (rounded upward) by Verrou $MWEXP = (MWR + (FMWR * DTR) + \Delta) + \Delta$	Result $MWEXP = 593.000000000000006$

For types Float64,  $\Delta$  perturbation is  $10^{-16} = \pm 0.0000000000000001$

If the code has low floating-point errors, the significant digits of the results should be robust to a random rounding. If not, the numerical noise increases over time, the code is then unstable which may have impacts on the global results

# 1- MAAP5/MAAP6 Numerical stability studies

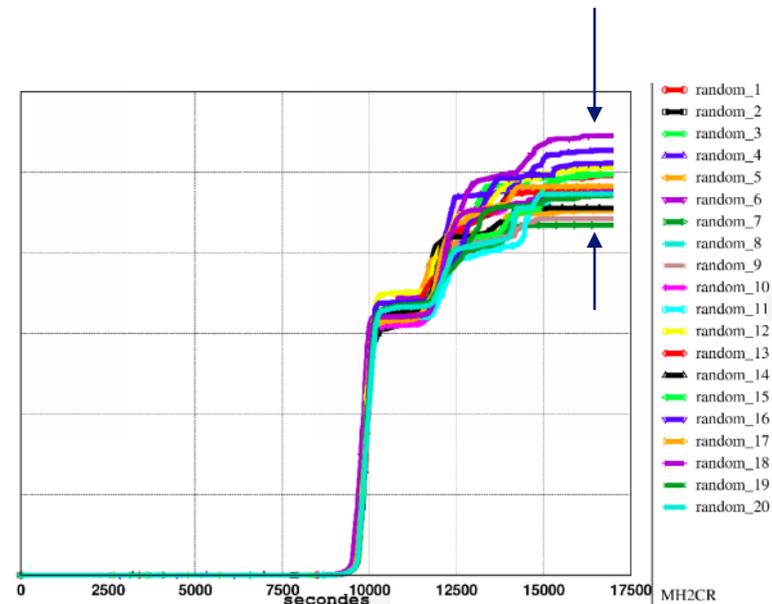
## Introducing VERROU

VERROU can be used as a diagnostic tool to know whether a code is stable or not.

- Running the same calculation of MAAP several times with VERROU (random rounding):

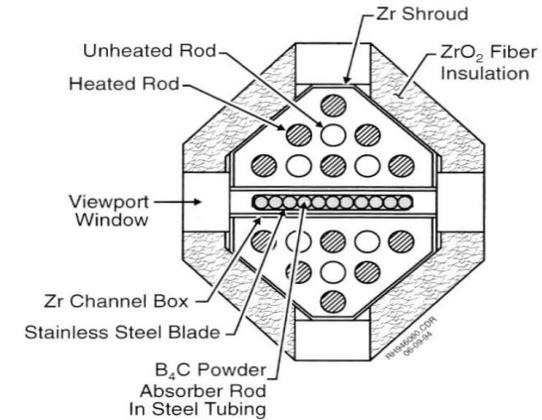
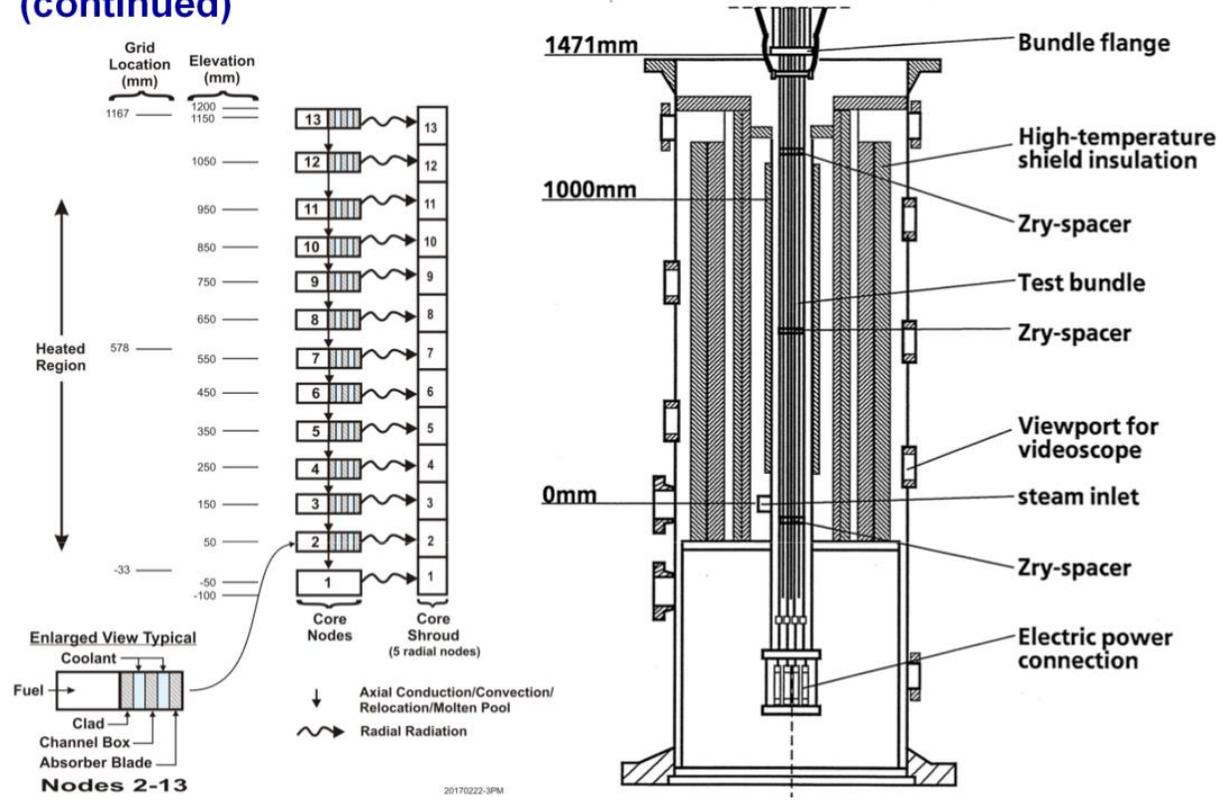
```
valgrind --tool=verrou --rounding-mode=random ${MAAP} ${INP}
```

- Analyzing parameter of interest discrepancy

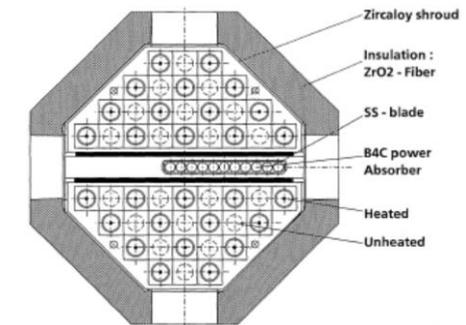


# BENCHMARKS

## CORA-16, CORA-17, and CORA-18 MAAP5 Modeling (continued)



**CORA-16 and CORA-17  
Rod Arrangement**

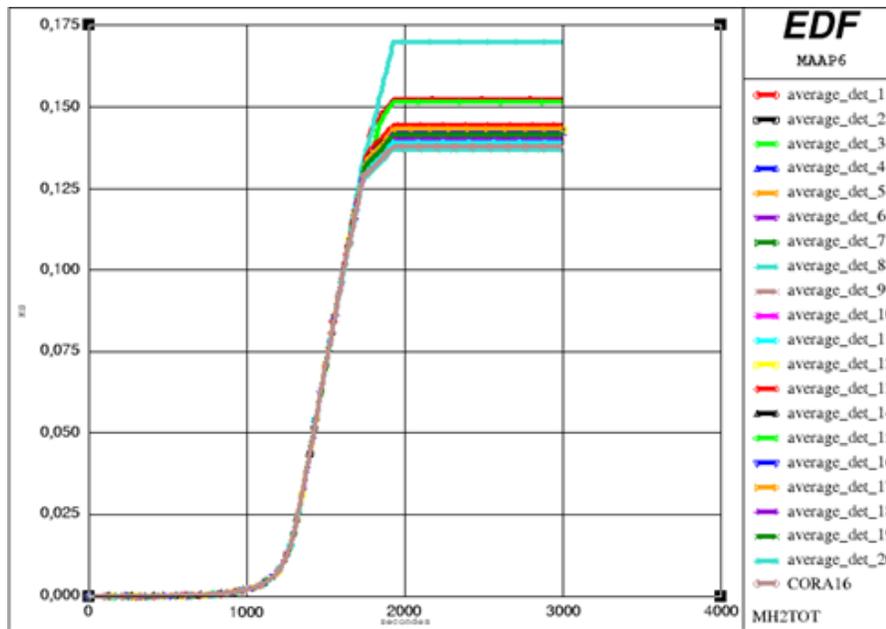


**CORA-18 Rod Arrangement**

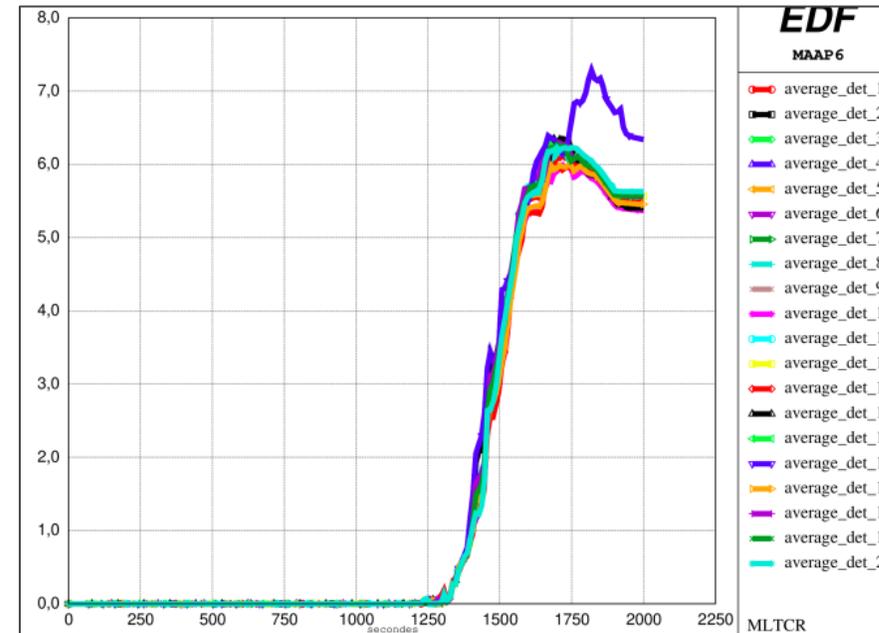
MAAP5 Benchmark of CORA Tests  
 Chan Y. Paik & Paul McMinn, Fauske & Associates, LLC (FAI)  
 2017 EPRI Safety Technology Week, MAAP User Group Meeting  
 Denver, Colorado, June 12-13 2017

# CORA16

## Before update



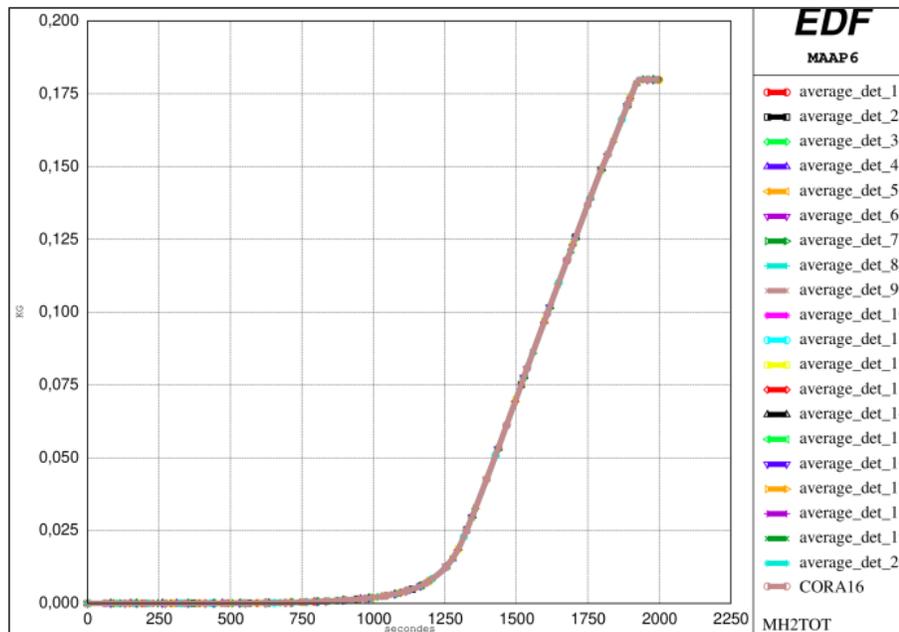
Total hydrogen production in core  
 $0.135 < \text{MH2TOT} < 0.169$



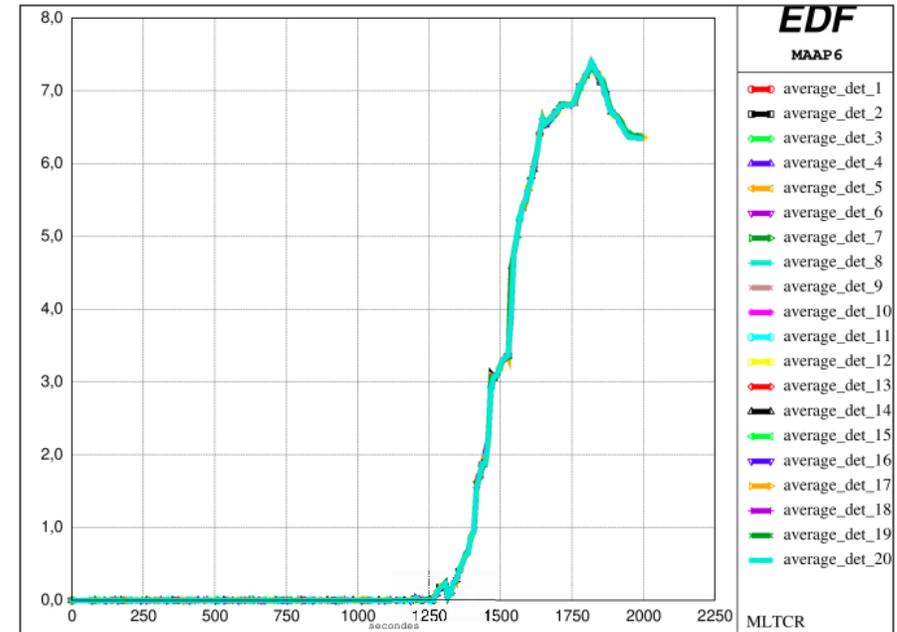
Mass of molten core material  
 $\text{MLTCR}_{\text{max}} < 7.3$

# CORA16

## After update



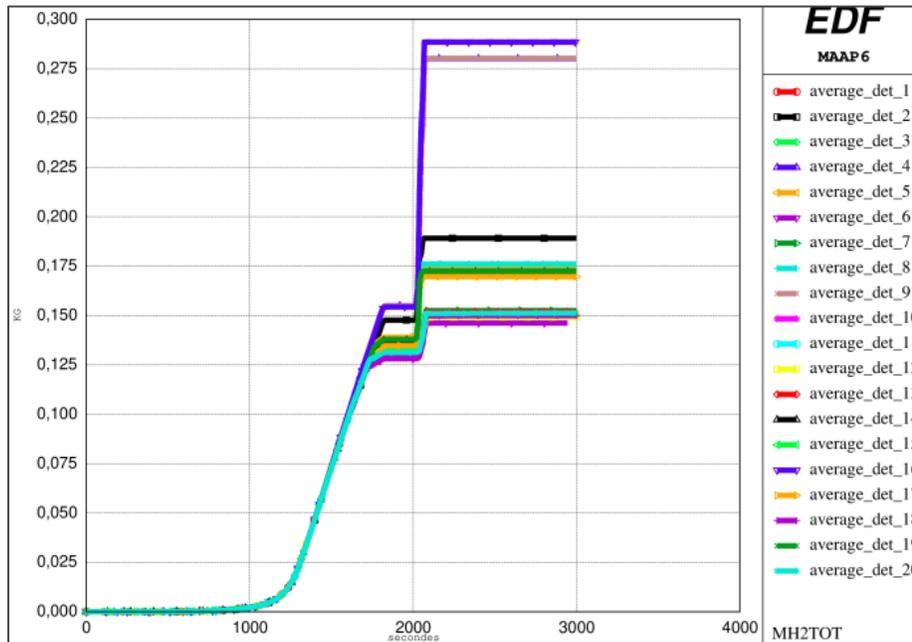
Total hydrogen production in core  
 $MH2TOT = 0.180$



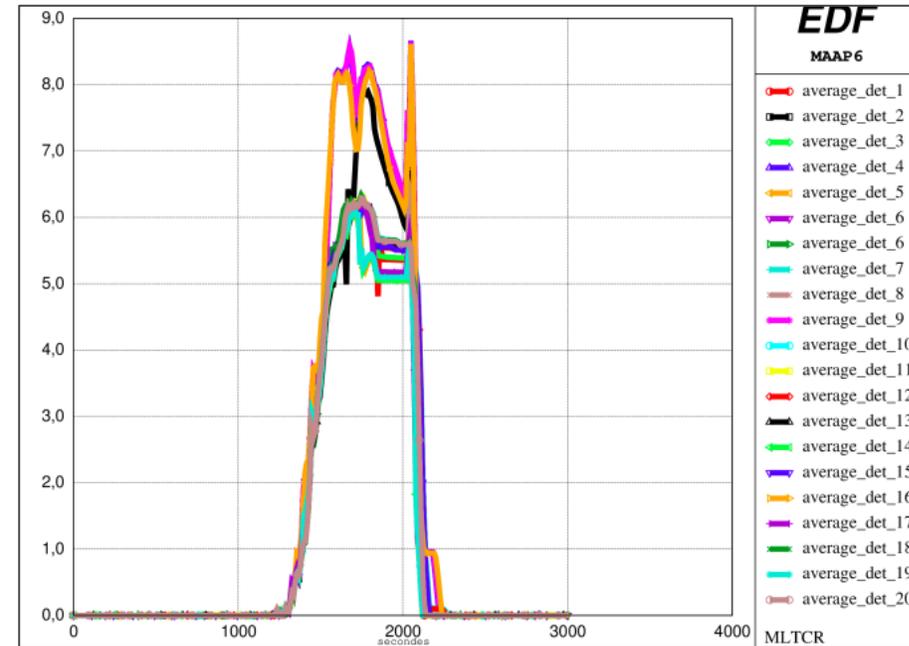
Mass of molten core material  
 $MLTCR_{max} < 7.3$

# CORA17

## Before update



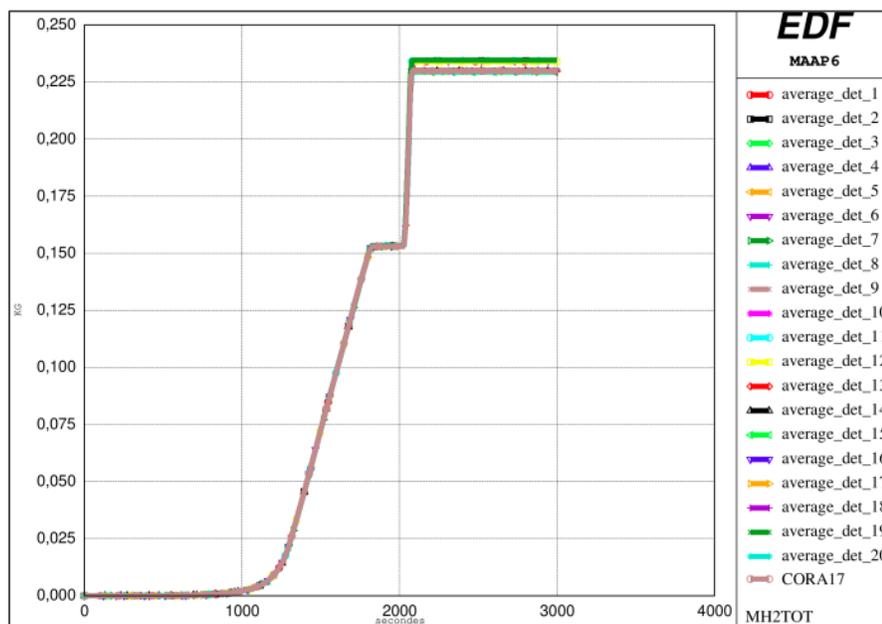
Total hydrogen production in core  
 $0.145 < \text{MH2TOT} < 0.285$



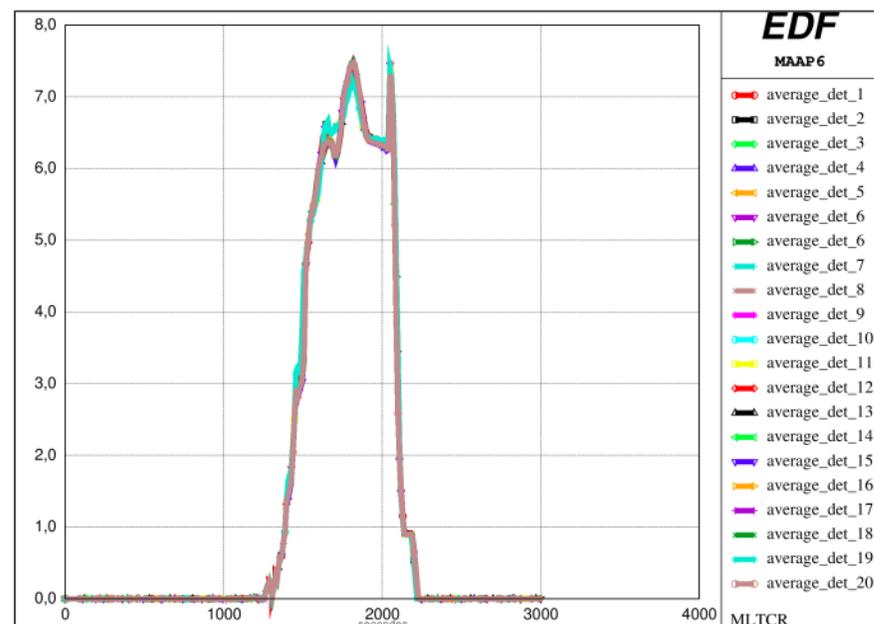
Mass of molten core material  
 $\text{MLTCR}_{\text{max}} < 8.5$

# CORA17

## After update



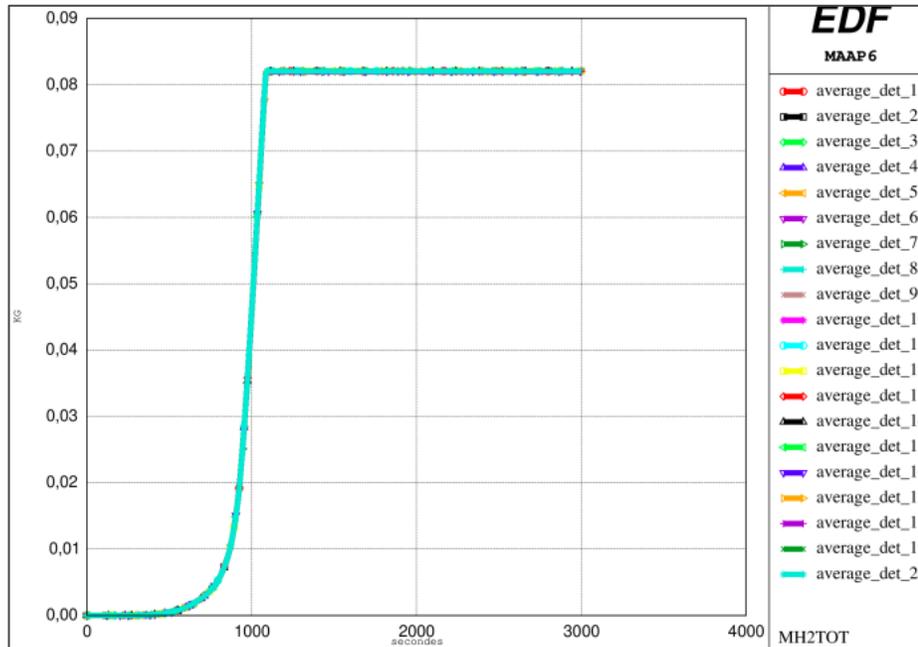
Total hydrogen production in core  
 $MH2TOT = 0.235$



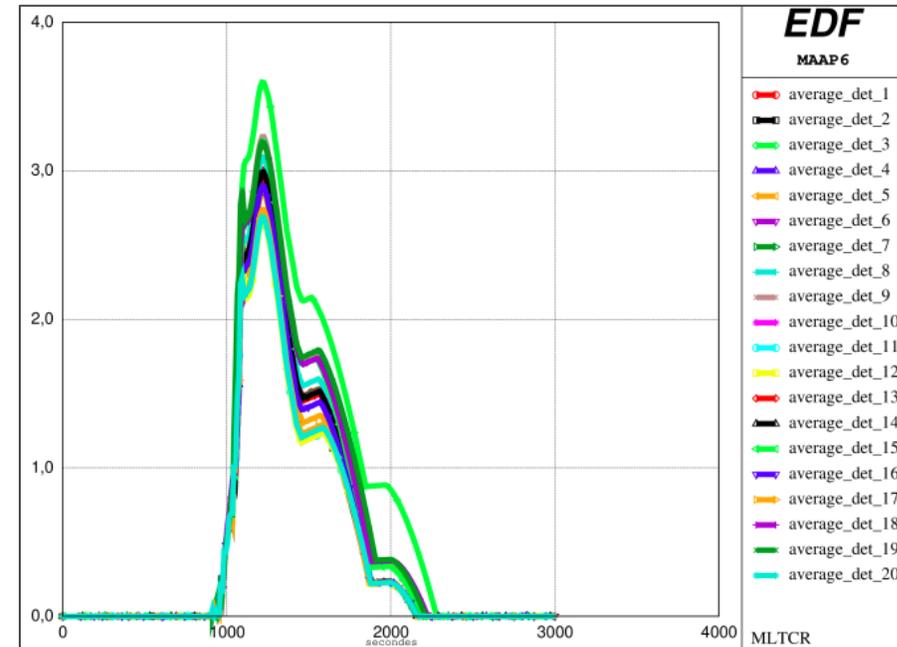
Mass of molten core material  
 $MLTCR_{max} < 7.5$

# CORA18

## Before update



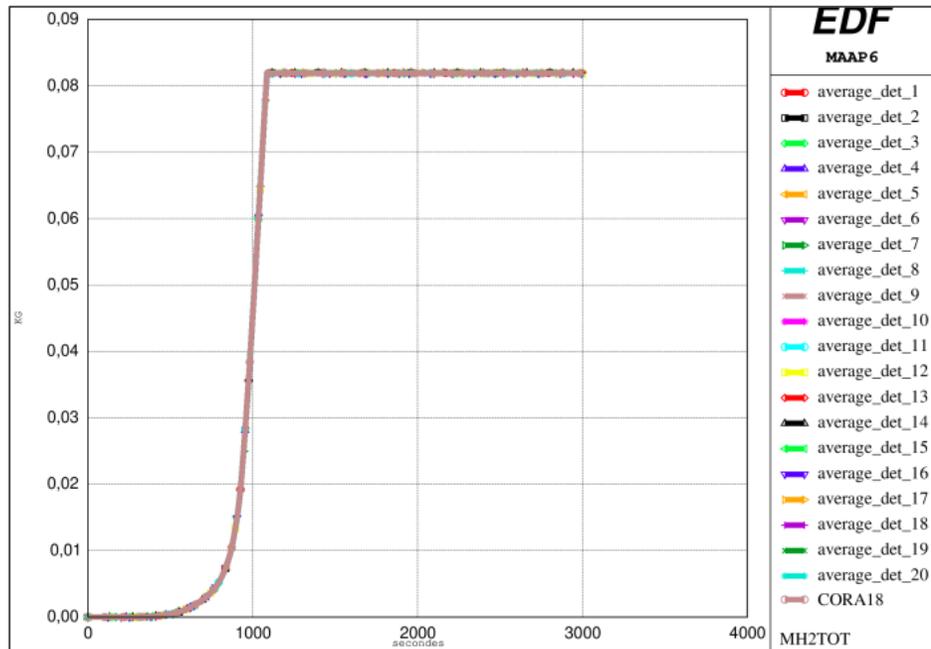
Total hydrogen production in core  
 $MH2TOT = 0.085$



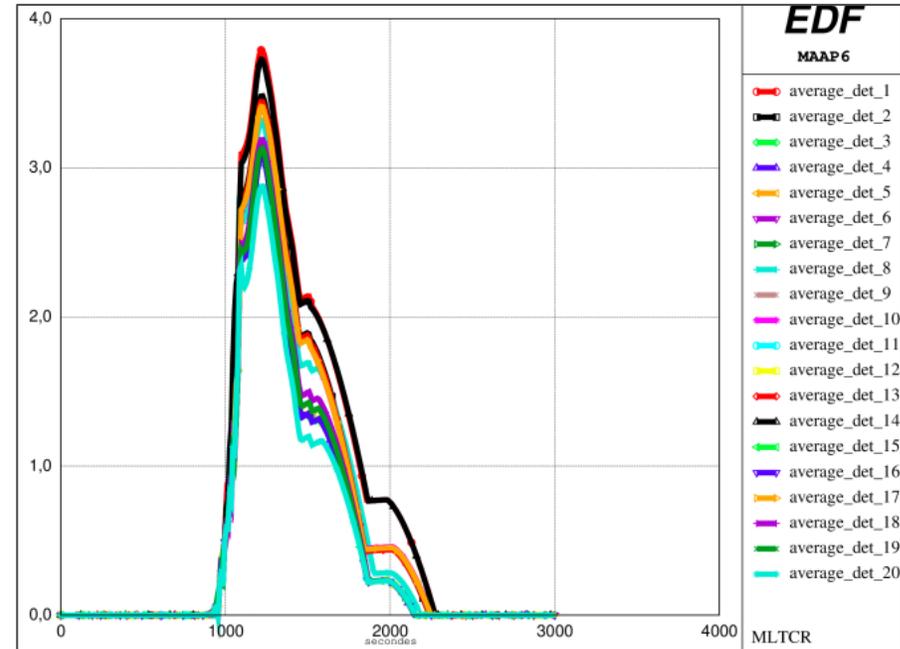
Mass of molten core material  
 $MLTCR_{max} < 3.5$

# CORA18

## After update



Total hydrogen production in core  
 $MH2TOT = 0.085$

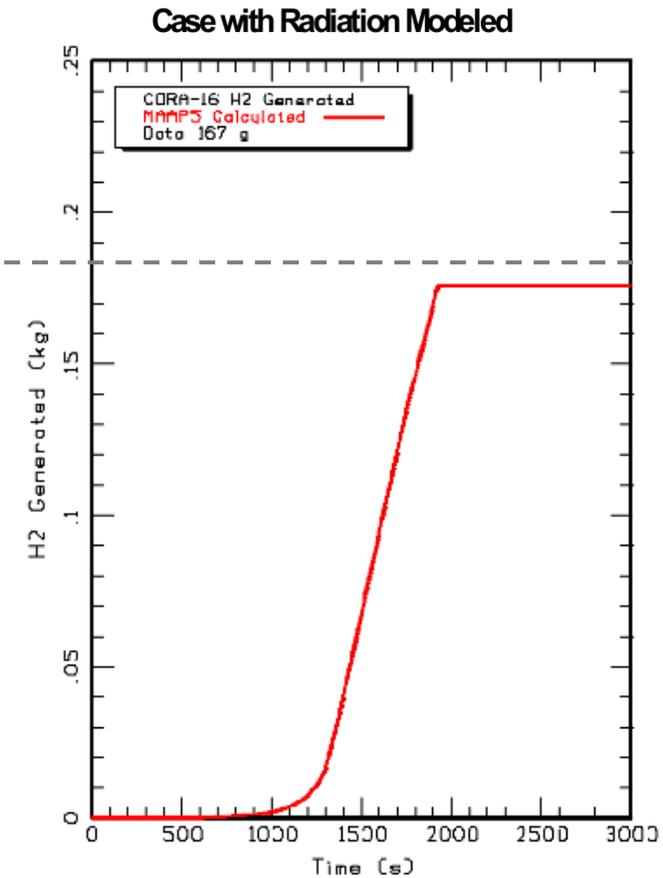
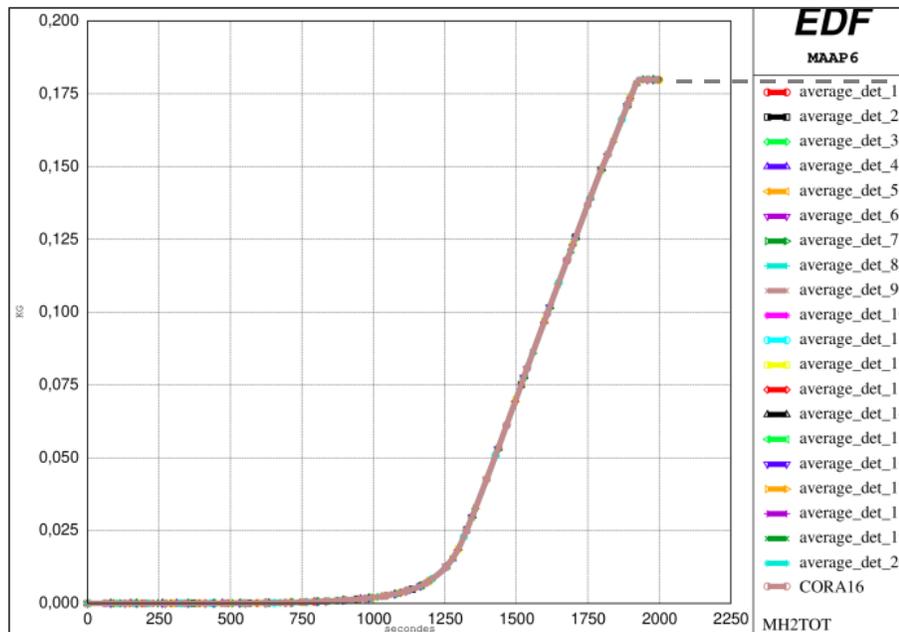


Mass of molten core material  
 $MLTCR_{max} < 3.8$

# Comparison with CORA experiments

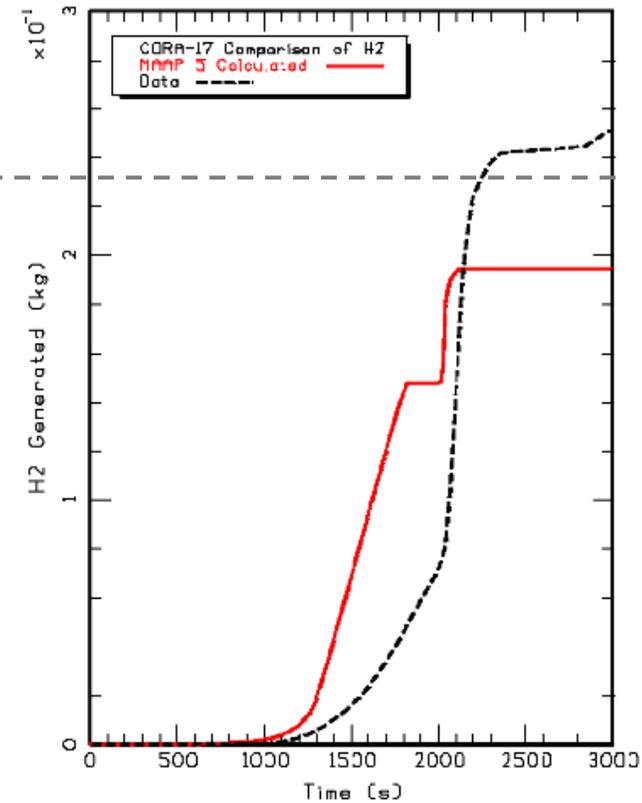
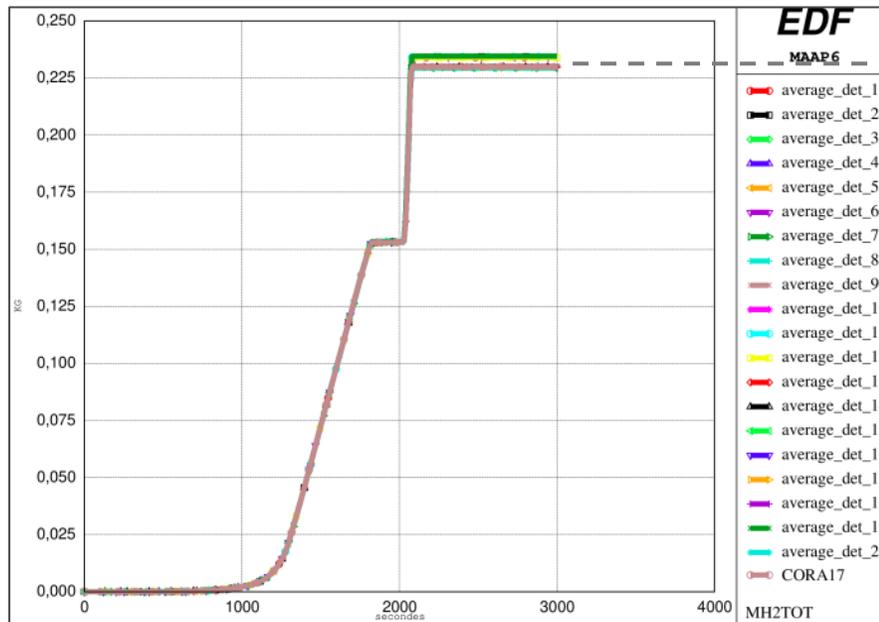
Presented at 2023 EPRI Safety Technology Week, MAAP User Group Meeting  
Manchester, UK, 2023, June

# CORA16



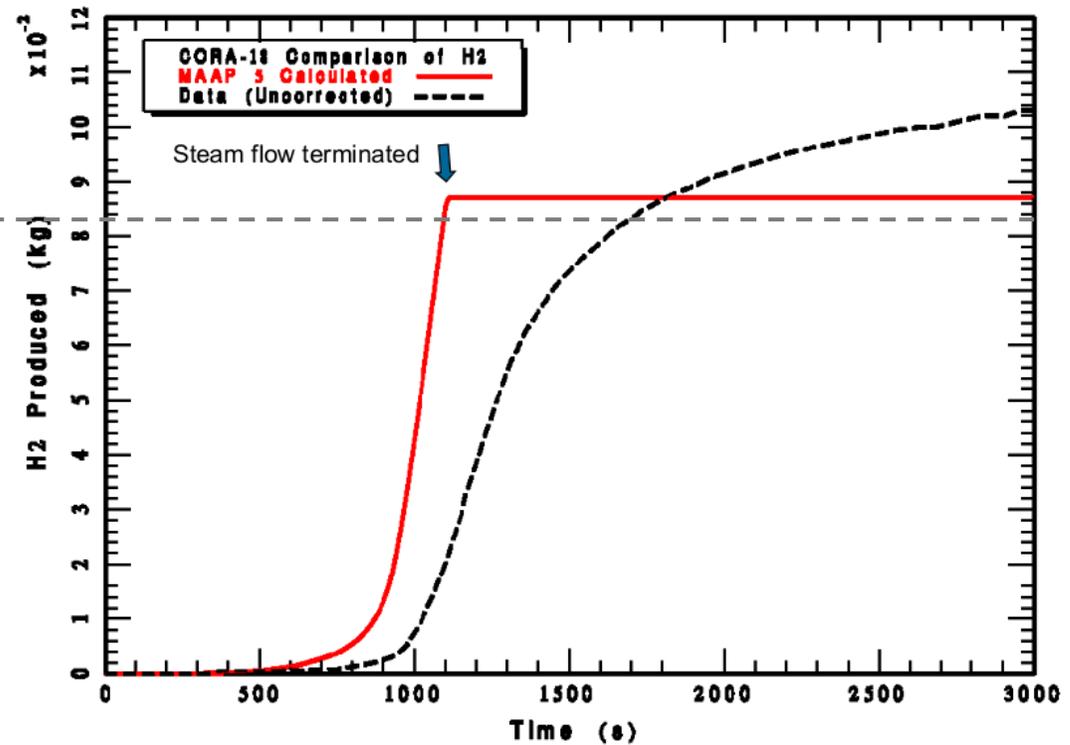
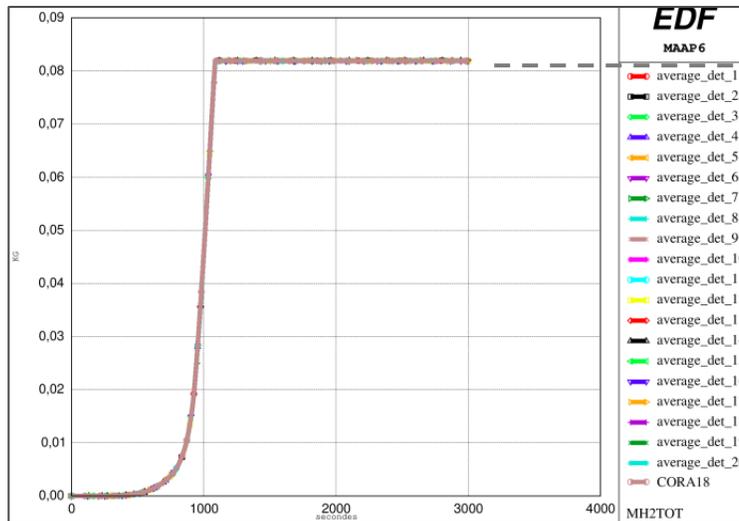
Total hydrogen production in core is slightly overestimated :  
180 g (calculation) versus 167 g (experiment)

# CORA17



Total hydrogen production in core is slightly underestimated :  
235 g (calculation) versus 250 g (experiment)

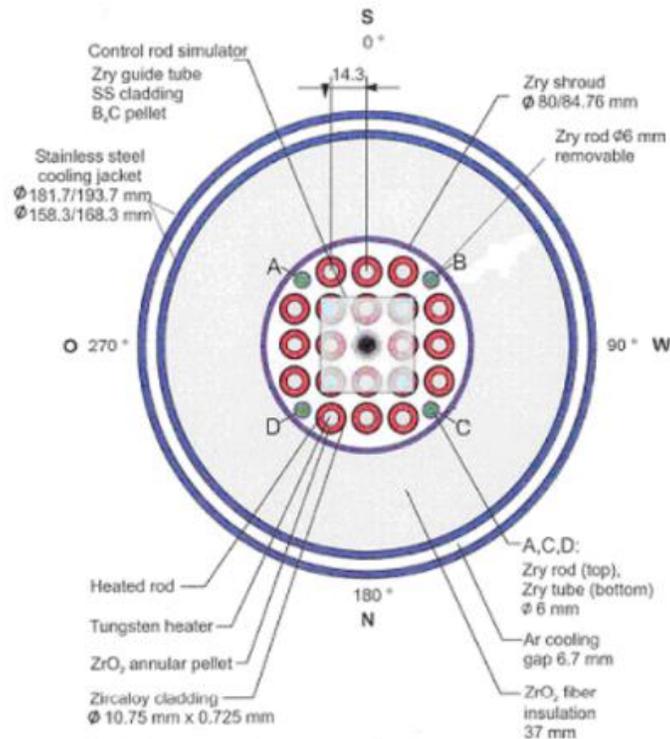
# CORA18



Data uncorrected, inlet steam flow was terminated at 1080 s

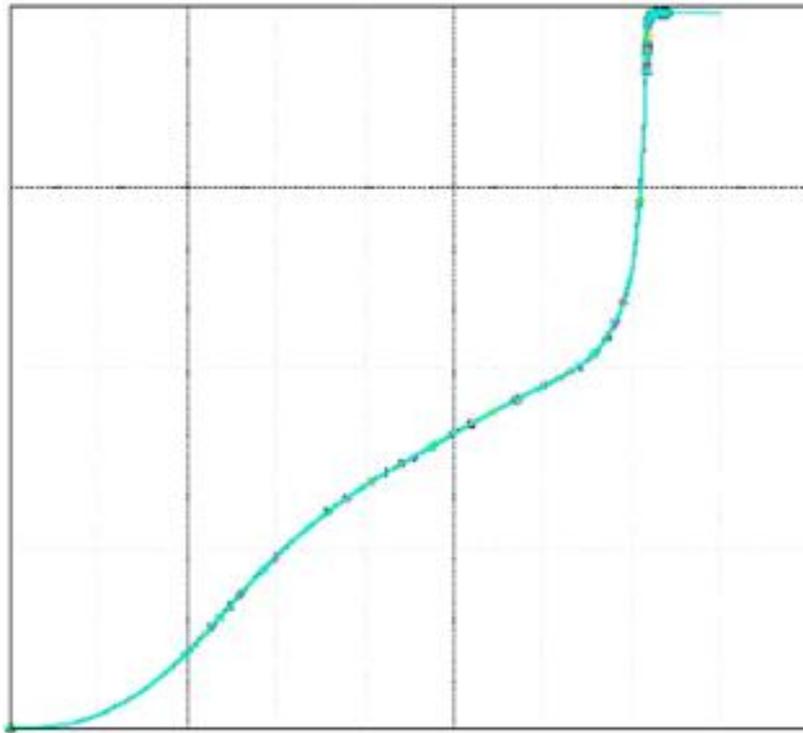
# QUENCH TESTS

The QUENCH tests were a follow-up of the CORA program. The main goal of QUENCH tests was to improve the modeling associated with reflooding of degraded core: quenching, oxidizing of cladding, hydrogen production, etc. The experimental set-up QUENCH includes a bundle of non-prototypic ( $ZrO_2$ ) electrically heated rods having Zircaloy cladding along with other components inside of a Zr shroud. Reflooding of the bundle is ensured with injection of water or steam.

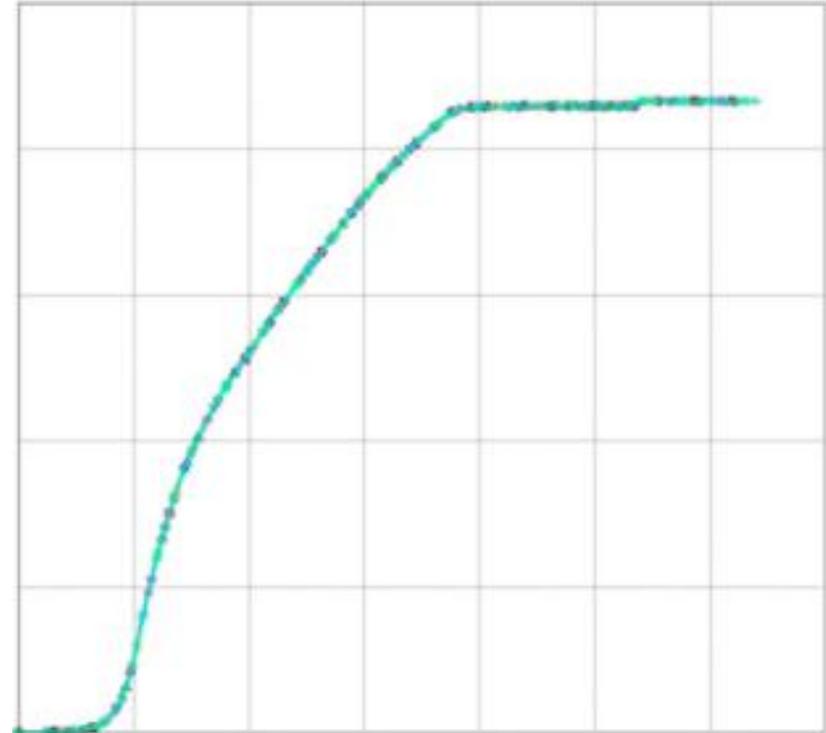


# QUENCH TESTS

The investigated QUENCH tests are perfectly stable



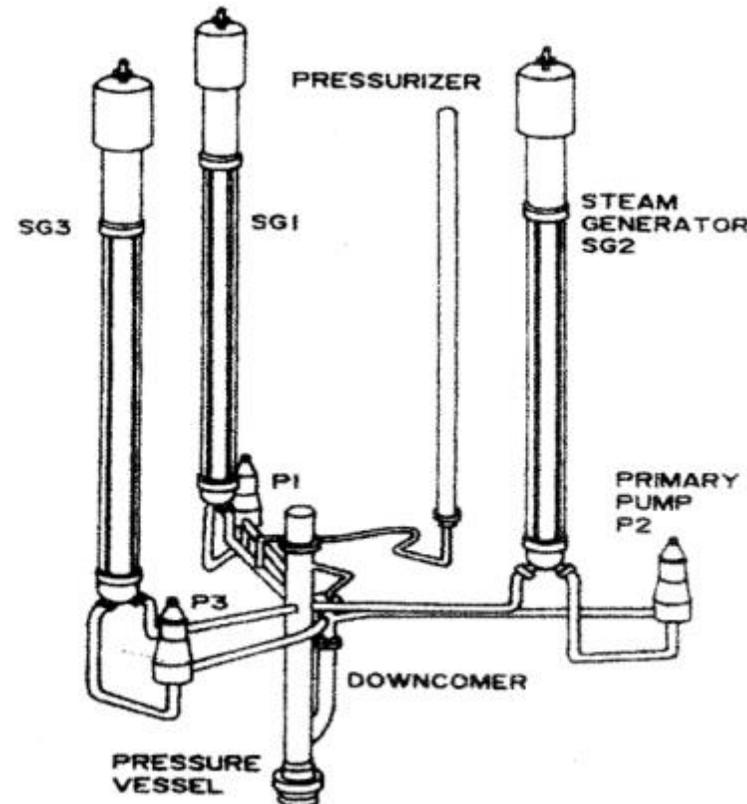
QUENCH 6



QUENCH 10

# BETHSY – TEST 91B

The BETHSY test program was part of a French strategy for PWR severe accident management performed during late 1980s for validation of the CATHARE code. The BETHSY facility shown below represents a scaled down model of a 3-loop 900 MWe EDF (1:99) PWR – Heights keep the real dimensions (for gravity head).

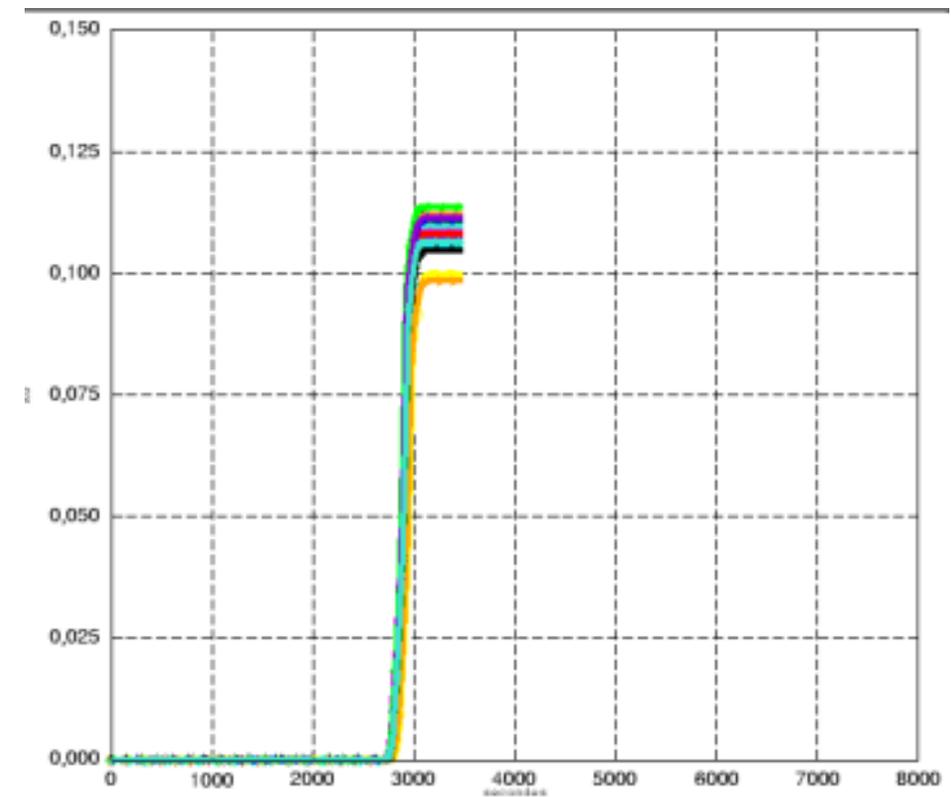
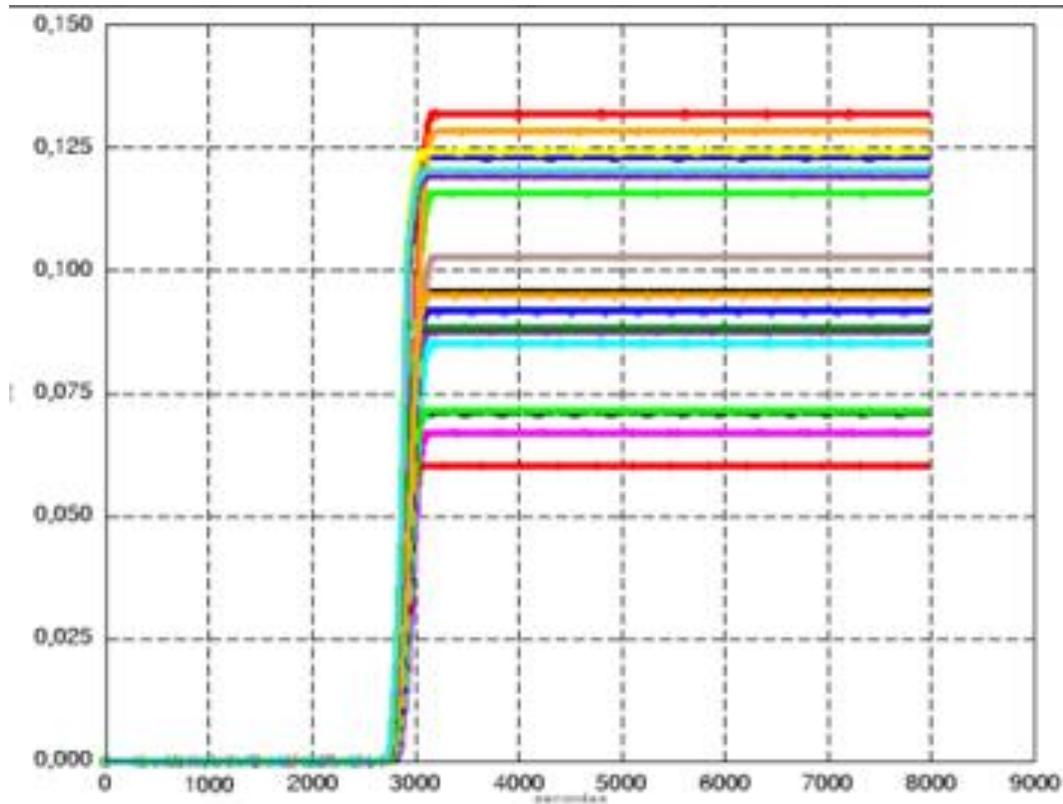


# BETHSY – TEST 91B

Before update

After update

Mass of H<sub>2</sub> generated



# Conclusion

VERROU is a powerful tool enabling to diagnose instabilities in SA codes.

Finding the origin of the instabilities is often a complicated task (use of debugger) but worth in order to improve the SA evaluations (TH, FP releases...)