# PAUL SCHERRER INSTITUT

## ALLGEMEINE ENERGIE

LEM - Laboratory for Energy and **Materials Cycles** 

Results

Reactor Modeling



# Optically accessible channel reactor for kinetic investigations of autothermal reforming

M. Bosco, T.-B. Truong, E. De Boni, F. Vogel

Temperature (K), Velocity Profile

reactor x-axis Reactor inlet section (1 quartz window, 2 channel, 3 catalytic plate, 4 heating block) with parabolic velocity profile. The arrows show the velocity distribution in the gas channel. Temperature distribution (side view)

→ Buovancy force has no significant influence on flow behavior in reactor channel for pure nitrogen

## Introduction

- Autothermal reforming of gasoline provides an efficient method to produce hydrogen for fuel cell applications.
- · To control a fuel processor a simple yet accurate kinetic model is necessary.
- · A new experimental reactor concept was developed, which allows surface temperature measurements through a guartz window and gas sampling through a capillary to measure the concentration profile in the reactor.
- · The measurements will be used to develop a kinetic model which takes into account the complex reaction network of autothermal gasoline reforming in a monolithic reactor.

Complex reaction network

$$\begin{split} \text{TOX:} & \text{C}_{n}\text{H}_{m} + \left(n + \frac{m}{4}\right)\text{O}_{2} \rightarrow n \,\text{CO}_{2} + \frac{m}{2}\text{H}_{2}\text{O} \qquad & \text{SR:} \,\text{C}_{n}\text{H}_{m} + n \,\text{H}_{2}\text{O} \leftrightarrow n \,\text{CO} + \left(n + \frac{m}{2}\right)\text{O}_{2} \rightarrow n \,\text{CO} + \frac{m}{2}\text{H}_{2} \qquad & \text{WGS:} \,\text{CO} + \text{H}_{2}\text{O} \leftrightarrow \text{CO}_{2} + \text{H}_{2} \\ \text{POX:} \, \text{C}_{n}\text{H}_{m} + \left(\frac{n}{2}\right)\text{O}_{2} \rightarrow n \,\text{CO} + \frac{m}{2}\text{H}_{2} \qquad & \text{MET:} \,\text{CO} + 3\,\text{H}_{2} \leftrightarrow \text{CH}_{4} + \text{H}_{2}\text{O} \end{split}$$

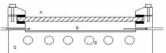
## Experimental

> Reactor

POX:

Idea: Design an optically accessible reactor with a flow field similar to a single monolith channe

Schematic side view of the channel reactor



A: quartz window, B: catalytic plate, C: reactor housing. D: heating cartridge



the feed system (left side of setup channel reactor picture), channel reactor (in the middle of the picture). heating box for sampling capillary (right side of picture) and the infrared camera (top section of the picture)

Setup Control LabVIEW™ program to control

the step motor, the mass flow

meters and the controllers of

the different heaters

- Infrared Camera Spectral range: 900 1700 nm
- Detector: Indium Gallium Arsenide
- Array format: 320 x 256 Pixel: 30 x 30 microns
- Frame rate: 30 Hz
- Temperature range: 20 1200°C



reactor with catalytic plate (insulation Channel removed). The white arrows visualize the flow through the reactor. On the right side of the reactor the septum port with the movable sampling capillary (black arrow) is

## > Experimental Setup

#### Feed System

- Water and Gasoline are fed using pressurised containers and
- LiquiFLOW™ controllers Oxygen and nitrogen are fed through flow controllers
- 2 Separate evaporators for water and
- gasoline Superheater up to 750°C

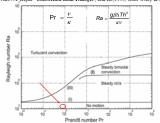
### Reactor

Stainless steel, channel height = 4 mm Maximum heating temperature = 750°C

#### Gas Sampling

- Movable stainless steel sampling capillary, internal diameter = 0.05 mm, external diameter = 0.8 mm
- Capillary enters reactor through high temperature septum port
- Capillary is placed directly above catalyst plate
- Electrical step motor is coupled to a linear positioning system (accuracy <
- 0.1 mm)
- Heated transfer line to GC and MS

## Assumptions: • Flow velocity: 0.14 m/s • Pure Nitrogen • Incompressible flow (Mach number << 1) • Laminar flow (Re < 30) avier-Stokes (incompressible flow) $\rho \frac{\partial u}{\partial t} + \rho (u \cdot \nabla) u = -\nabla \rho + \eta \nabla^2 u + F$ $\nabla \cdot u = 0$ $F_y = g\rho\beta(T-T_\infty)$ Convection and conduction: $\rho c_{\rho} \frac{\partial T}{\partial t} + \nabla \cdot \left(-k\nabla T + \rho c_{\rho} T u\right) = Q$ $Q = \alpha (T - T_{amb.})$ (Convective heat flux)



### First Experiments

- Measured concentration profiles (MS) along the catalyst plate during dry partial oxidation of methane at 575°C (O/C = 0.85, GHSV = 94500 h<sup>-1</sup>, atmospheric pressure)
- The oxygen is consumed completely after 8% of reactor <sup>5</sup> length by total oxidation and partial oxidation, producing water, carbon monoxide, carbon dioxide and hydrogen
- After 3% of reactor length the water concentration decreases due to the seam reforming and water gas shift reactions
- . The thermodynamic equilibrium is reached at 50% of the reactor length
- After 90% of the reactor length changes in concentration profiles are due to the not optimal capillary positioning over the catalytic plate

 Measured (yellow = hot (> 575°C), red = 575°C, blue = cold) temperature distribution on the catalyst plate during the experiment. The gas flow is from left to right vs). The sampling capillary is visible in centre of the reactor (top view)

. Three hot spots are visible at the gas inlets, they correspond to the regions where oxygen leads to strongly exothermic reactions (TOX and POX)

## Conclusions

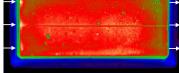
- The reactor modeling showed that the parabolic flow in the channel is maintained.
- · First experiments showed that the gas sampling and the surface temperature measurements can be carried out with a high local resolution.
- The measured concentration profiles indicate that CO<sub>2</sub>, CO, H<sub>2</sub>, and H<sub>2</sub>O are primary products in the early stage of reaction.
- · The measured concentration profiles and surface temperatures will allow to parameterise a kinetic model based on a large number of experimental data.

Contact: Frédéric Vogel, Paul Scherrer Institute, OVGA/104 5232 Villigen-PSI, Switzerland - phone: +41-(0)56-310-2135 fax: +41-(0)56-310-2199 / email: frederic.vogel@psi.ch

Ref.: A.,Bejan - Convection Heat Transfer, 2nd ed., 1995, John Wiley & So

Rayleigh-Bénard convection does not occur in reactor channel: Ra is far into the no-motion area

- →The parabolic velocity profile is maintained along the reactor 35 30 20
  - 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9



0.1 0.2 0.3 0.4 0.5 0.6 0.7 0.8 0.9 Distance from inlet

